



Environmental Protection and Compliance Division Environmental Compliance Programs (EPC-CP) PO Box 1663, K490 Los Alamos, New Mexico 87545 (505) 667-0666 National Nuclear Security Administration Los Alamos Field Office, A316 3747 West Jemez Road Los Alamos, New Mexico, 87544 (505) 665-7314

Date: JAN 1 3 2017 Symbol: EPC-DO-16-361 LA-UR: 16-29607 Locates Action No.: N/A

Mr. John E. Kieling Hazardous Waste Bureau New Mexico Environment Department 2905 Rodeo Park Drive East, Building 1 Santa Fe, NM 87505

Dear Mr. Kieling:

Subject: Technical Area 63 Transuranic Waste Facility Container Storage Unit Construction Notice, Los Alamos National Laboratory, Hazardous Waste Facility Permit, EPA ID #NM0890010515

The purpose of this letter is to provide notification of the construction of the Technical Area 63 Transuranic Waste Facility (TWF) Container Storage Unit to the New Mexico Environment Department Hazardous Waste Bureau (NMED-HWB). This notice is submitted pursuant to the requirements of the New Mexico Administrative Code (NMAC 20.4.1.900) incorporating the Code of Federal Regulations, Title 40 (40 CFR) provisions at 40 CFR §270.30(l)(2). The TWF has been constructed in compliance with the requirements contained in the Los Alamos National Laboratory (LANL) Hazardous Waste Facility Permit (the Permit) issued to the Department of Energy (DOE) and Los Alamos National Security, LLC (LANS), collectively the Permittees, in November 2010.

The Permittees originally submitted a permit modification request seeking approval for the TWF on August 18, 2011 and this was approved by NMED-HWB on December 23, 2013. The permit modification request contained facility design drawings that illustrated construction details used for the development of the TWF related conditions contained in the Permit. Some minor changes that developed later during the project were subsequently submitted through permit modifications. These included design changes submitted by the Permittees on July 28, 2014 and permit modifications to incorporate changes made during construction of the facility that were originally submitted on March 11, 2016 and supplemented on September 1, 2016.

Enclosure 1 of this submittal includes a comparison of construction related TWF conditions from the Permit referencing the associated drawings or descriptions contained in the original permit modifications



Mr. John E. Kieling EPC-DO-16-361

with the construction drawings, material information, or reports for the final project. This is used to demonstrate meeting the requirement in 40 CFR 270.30(1)(2)(i) that the facility has been constructed in compliance with the Permit. Enclosure 2 of this submittal includes the new construction drawings and information listed in the comparison.

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Enclosure 3 of this submittal includes a list of operational equipment or items in the Permit that will also be available for review and inspection by NMED-HWB prior to the hazardous waste management operations start date for the TWF. With this submittal, the Permittees are requesting the coordination of this inspection in order to meet the start schedule for the project and provide timely corrections or replacement of equipment if needed.

Enclosure 4 of this submittal includes signed certification pages for this report by facility representatives and a registered professional engineer as required by 40 CFR §§270.11 and 270.30(l)(2)(i). Three hard copies and one electronic copy of this submittal are being delivered to the NMED-HWB. The electronic copy, provided only to the NMED-HWB, contains a reproduction of the hardcopy in portable document format (pdf). If you have comments or questions regarding this report, please contact Karen E. Armijo (DOE) at (505) 665-7314 or Mark Haagenstad (LANS) at (505) 665-2014.

Sincerely,

John C. Bretzke Division Leader Environmental Protection and Compliance Division Los Alamos National Security, LLC

Sincerely,

Karen E. Armijo Permitting and Compliance Program Manag-National Nuclear Security Administration Los Alamos Field Office U.S. Department of Energy

JPM:KEA:MPH:/gb

Enclosure: 1) TA-63 TWF Permit Construction Requirements

- 2) TA-63 TWF Construction Drawings and Information
- 3) TA-63 TWF Permit Equipment and Operational Requirements
- 4) Facility Certification
- Cy: Laurie King, USEPA/Region 6, Dallas, TX (E-File) Kathryn M. Roberts, NMED-HWB, Santa Fe, NM, (E-File) Dave Cobrain, NMED/HWB, Santa Fe, NM, (E-File) Neelam Dhawan, NMED-HWB, Santa Fe, NM, (E-File) Siona Briley, NMED-HWB, Santa Fe, NM (E-File) Kimberly Davis Lebak, NA-LA, (E-File) Peter Maggiore, NA-LA, (E-File) Jody Pugh, NA-LA, (E-File)

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Karen E. Armijo, NA-LA, (E-File) Janelle Armijo, APM/NA-LA, (E-File) Paul Holland, LASO-NS-LP, (E-File) Sophia Calabaza, NA-LA, (E-File) Craig S. Leasure, PADOPS, (E-File) William R. Mairson, PADOPS, (E-File) Michael T. Brandt, ADESH, (E-File) Raeanna Sharp-Geiger, ADESH, (E-File) Brett A. Cederdahl, PM1, (E-File) Denise C. Gelston, EWMO-DO, (E-File) Jerry Bonn, MOF-CM, (E-File) John P. McCann, EPC-DO, (E-File) Victoria R. Baca, DESHS-EWMS (E-File) Mark P. Haagenstad, EPC-CP, (E-File) Gian A. Bacigalupa, EPC-CP, (E-File) Ellena I. Martinez, EPC-CP, (E-File) lasomailbox@nnsa.doe.gov, (E-File) locatesteam@lanl.gov, (E-File) emla.docs@em.doe, (E-File) epc-correspondence@lanl.gov, (E-File) rcra-prr@lanl.gov, (E-File) epcat@lanl.gov, (E-File)







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Date: JAN 1 Symbol: EPC-DO-LA-UR: 16-29607 Locates Action No.: N/A

JAN 1 3 2017 EPC-DO-16-361 16-29607 N/A

Dear Mr. Kieling:

Santa Fe, NM 87505

Mr. John E. Kieling Hazardous Waste Bureau

New Mexico Environment Department 2905 Rodeo Park Drive East, Building 1

Subject: Technical Area 63 Transuranic Waste Facility Container Storage Unit Construction Notice, Los Alamos National Laboratory, Hazardous Waste Facility Permit, EPA ID #NM0890010515

The purpose of this letter is to provide notification of the construction of the Technical Area 63 Transuranic Waste Facility (TWF) Container Storage Unit to the New Mexico Environment Department Hazardous Waste Bureau (NMED-HWB). This notice is submitted pursuant to the requirements of the New Mexico Administrative Code (NMAC 20.4.1.900) incorporating the Code of Federal Regulations, Title 40 (40 CFR) provisions at 40 CFR §270.30(1)(2). The TWF has been constructed in compliance with the requirements contained in the Los Alamos National Laboratory (LANL) Hazardous Waste Facility Permit (the Permit) issued to the Department of Energy (DOE) and Los Alamos National Security, LLC (LANS), collectively the Permittees, in November 2010.

The Permittees originally submitted a permit modification request seeking approval for the TWF on August 18, 2011 and this was approved by NMED-HWB on December 23, 2013. The permit modification request contained facility design drawings that illustrated construction details used for the development of the TWF related conditions contained in the Permit. Some minor changes that developed later during the project were subsequently submitted through permit modifications. These included design changes submitted by the Permittees on July 28, 2014 and permit modifications to incorporate changes made during construction of the facility that were originally submitted on March 11, 2016 and supplemented on September 1, 2016.

Enclosure 1 of this submittal includes a comparison of construction related TWF conditions from the Permit referencing the associated drawings or descriptions contained in the original permit modifications

ENCLOSURE 1

Technical Area 63 Transuranic Waste Facility Container Storage Unit Permit Construction Requirements

EPC-DO-16-361

LA-UR-16-29607

Date:

JAN 1 3 2017

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Item No.	Permit Section	Requirement	Permit Modification Request Documentation (TWF PMR, August 18, 2011)	Construction Documentation	Notes
1	A.6	General. The unit is built at the intersection of Pajarito Road and Puye Road, within the triangle formed by Building 63-111 to the east, Puye Road to the north, and Pajarito Road to the southwest.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in location.
2	A.6	The main structure for the unit is a concrete pad providing a physical base for six waste storage buildings, three waste characterization trailers, and outside storage of waste containers that are too large for placement in the buildings.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change to general plan.
3	A.6	The TWF is constructed on 1.82 acres (79,239 square feet).	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	Slight revision in area calculation included in TWF Construction Upgrades Permit Modification Supplement of September 1, 2016.
4	A.6	The pad is surrounded by a security barrier system.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	Revision to replace security fence with security barrier included in TWF Construction Upgrades Permit Modification of March 11, 2016. Revised Fig. 55, Attachment N, Permit.
5	A.6	The boundary of the hazardous waste management unit is limited to the northern portion of the concrete pad defined by those areas that drain to a retention basin.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in boundary of permitted unit.
6	A.6	Along the northern and western sides of the unit, this is the edge of the concrete pad along the bottom of the retaining walls.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in boundary of permitted unit.
7	A.6	On the east side, the edge of the curbing for the concrete pad is the boundary.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in boundary of permitted unit.
8	A.6	The southern side of the boundary is defined by a painted line in compliance with Permit Section 3.5(2), <i>Management of Containers</i> . The line is situated approximately between the south east corner of the retention basin and the curb and gutter at the opposite corner of the fence line along the eastern side of the unit. This is defined by the limits of the catchment that drains to the retention basin.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000; DWG-102355-C55443-C-3001; DWG-102355-C55443-C-1004B	No change in boundary of permitted unit.
9	A.6	The unit also includes a small storage building for calibration sources used for waste characterization activities.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in location or use for Building TA-16-0159
10	A.6.1	Concrete Pad. The TWF pad consists of 8-inch thick reinforced concrete to provide support for the site structures and vehicle movement. The pad rests on leveled gravel base course and is nominally 8 inches thick.	TWF PMR, Figure 2-7, C55443, C-5000	DWG-102355-C55443-C-5000	No change in thickness of concrete pad
11	A.6.1	Given the elevation difference on the site, retaining walls were constructed along the northwest portion of the site.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in location of retaining walls

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12	A.6.1	The pad is sloped in a range from 1.1 to 2.5% to promote drainage of storm water and potential fire suppression water to the retention pond.	TWF PMR, Figure 2-6, C55443, C-1003	DWG-102355-C55443-C-1003; DWG-102355-C55443-C-1004B	Only minor differences in slope gradient lines. Range of pad slopes revised by TWF Construction Upgrades Permit Modification Supplement of September 1, 2016.
13	A.6.1	The perimeter of the pad has a 15" to 18" gutter and 6" high curb to provide run-off control.	TWF PMR, Figure 2-7, C55443, C-5000	DWG-102355-C55443-C-5000; DWG-102355-C55443-C-1000	No change in gutter and curb locations and function. Size of gutter revised by TWF Construction Upgrades Permit Modification Supplement of September 1, 2016.
14	A.6.1	A valley gutter isolates the northern portion of the pad.	TWF PMR, Figure 2-5, C55443, C-1000; TWF PMR, Figure 2-7, C55443, C-5000		No change in location or design of valley gutter.
15	A.6.1	Storm water and potentially contaminated fire suppression water flow from the northern portion of the pad flows to the valley gutter that drains to the retention basin.	TWF PMR, Figure 2-6, C55443, C-1003	DWG-102355-C55443-C-1003; DWG-102355-C55443-C-1004B	Only minor differences in slope gradient lines. No change in function of concrete pad slope.
16	A.6.2	Storage Buildings . The five buildings measure 33 x 64 ft or approximately 2112 square feet, and are 15 ft high.	TWF PMR, Figure 2-9, C55444, A-1050	DWG-102355-C55444-A-1050; DWG-102355-C55444-A-3002	No change in building dimensions; actual dimensions are 33'4" x 64'4."
17	A.6.2	These five storage buildings are designated 63-0149, 63-0150, 63-0151, 63-0152, and 63-0153.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in building numbers
18	A.6.2	The storage buildings are constructed as covered single-story structural steel frames. Each of the storage buildings and its structural members are designed to exceed the snow load for roof design, the design wind force for buildings, and the seismic loading for structural components, as described in American Society of Civil Engineers specification ASCE 7-05, Minimum Design Loads for Buildings and Other Structures. The steel frame is an ordinary moment frame with joists to attach roof panels and girts to attach wall panels. The walls of the facility are rigid to provide protection from the elements and external forces. Gypsum board on light gauge metal studs with industrial coating finish the interior walls. The roof is a high quality metal standing seam. Batt insulation in the ceiling and on the inside of the walls	TWF PMR, Figure 2-13, C55444, S- 3000	DWG-102355-C55444-S-3000; DWG-102355-C55444-A-1051; DWG-102355-C55444-A-3002; DWG-102355-C55444-S-0002	No change in building structural details.

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19	A.6.2	Electric heaters heat the interior to prevent fire suppression systems and eyewash stations from freezing.	NA	DWG-102355-C55444-M-1000; DWG-102355-C55445-M-1000; DWG-102355-C55444-M-6000; DWG-102355-C55445-M-6000	Heater and eyewashes present.
20	A.6.2	Cooling is provided by venting fans.	NA	DWG-10235-C55444-M-1000; DWG-10235-C55445-M-1000; DWG-10235-C55444-M-6000; DWG-10235-C55445-M-6000	Venting fans present.
21	A.6.2	In order to drain the building in the event of a fire, the floors are constructed to provide a shallow slope (1/8 inch to 1 foot) from the back end of the building towards the front, and then out the roll-up door opening and a loading ramp to the concrete pad outside the building.	TWF PMR, Figure 2-10, C55444, S- 1000	DWG-10235-C55444-S-1000; DWG-10235-C55445-S-1000	No change in floor slope and floor configuration.
22	A.6.2	The building floors (i.e., mat slabs) are six inches higher than the outside surface of the concrete pad to prevent run-on, and are sloped toward the roll-up door at the building entrances for drainage, in accordance with 40 CFR §264.175(b)(2) and (c).	TWF PMR, Figure 2-14, C55444, S- 5010; Figure 2-10, C55444, S-1000	DWG-10235-C55444-S-1000, DWG-10235-C55444-S-5010; DWG-10235-C55445-S-1000; DWG-10235-C55445-S-5010	No change in curb or floor slope.
23	A.6.2	The concrete floors are coated to provide a sealed surface and chemical resistance, although secondary containment pallets are used to meet the containment requirements of the Permit for potential liquid containing waste containers in the storage buildings and in compliance with 40 CFR §264.175(b)(1). The floor coating standards include: • Minimum Class B per National Fire Protection Association (NFPA); • Radiation resistant as determined by American Society for Testing and Materials, International specification ASTM D 4082; and • Decontaminable to at least 95 percent of total activity removed and certified for Nuclear Coating Service level II.	NA	TA-63 TWF Storage Building Floor Coating Information	No change in floor coating specification. Condition of the structure (e.g., floor cracking or deterioration) will be addressed by the facility program for equipment and structure repair (Permit Section 2.6.2 and Attachment E, Inspection Plan; see Enclosure 4 of this document).
24	A.6.3	Storage and Characterization Building. The sixth storage building is divided into a storage area, a staging room used for the thermal equilibrium of containers to prepare for head space gas sampling, and additional support and analytical equipment rooms.	TWF PMR, Figure 2-19, C55445, A- 1050	DWG-102355-C55445-A-1050	No change in building layout as constructed.
25	A.6.3	The building dimensions are 80 x 33 ft (approximately 2640 square feet) and 15 feet high. The building is constructed to the same standards as the other storage buildings. The building is numbered 63-0154.	TWF PMR, Figure 2-19, C55445, A- 1050; Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000; DWG-102355-C55445-A-1050; DWG-102355-C55445-A-3002	No change in building dimensions and numbering; actual building size is 33'4"x79'11."

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26	A.6.4	Characterization Trailers . The TWF facility includes pads with utility hook-ups for the characterization trailers used to certify containers as meeting DOE WIPP waste acceptance criteria (WAC).	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in locations for characterization trailers.
27	A.6.4	The trailers are numbered 63-0155, 63-0156, and 63-0157 at TA-63.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in characterization trailer numbering.
28	A.6.5	Retention Basin . The retention basin is designed to collect surface storm water or melt water run-off from the concrete pavement via the slope (ranging from 1.1% to 2.5%) of the concrete pad, and in the event of a fire at the unit, fire suppression water that could flow out of the storage buildings or from other unit structures to the concrete pad.		DWG-102355-C55443-C-1003; DWG-102355-C55443-C-1004B	No change in site grading of permitted unit that would affect purpose of the retention basin. Range of pad slopes revised by TWF Construction Upgrades Permit Modification Supplement of September 1, 2016
29	A.6.5	The designed total retention basin volume also includes a minimum of 1.0 ft of freeboard, resulting in a total capacity of 137,450 gallons (18,375 cubic ft.).	TWF PMR, Figure 2-6, C55443, C-1003	DWG-102355-C55443-C-1003; DWG-102355-C55443-C-1017	No change in design volume of the retention basin. The freeboard information was revised in the TWF Construction Upgrades Permit Modification of March 11, 2016. However, subsequent review for this report has determined the freeboard value should remain the same (0.5 ft) as included in the original PMR and this will be resolved with a future permit modification description change to Permit Attachment A.6.5 for clarification.
30	A.6.5	The dimensions of the basin are 125 ft by 42 ft by 3.5 ft deep.	TWF PMR, Figure 2-29, C55443, C- 1017	DWG-102355-C55443-C-1017	No change in retention basin plan.
31	A.6.5	The retention basin is equipped with a manual release valve that may be used to discharge collected water that meets appropriate surface water discharge standards, as required by Permit Section 3.14.2.	TWF PMR, Figure 2-29, C55443, C- 1017	DWG-102355-C55443-C-1017	No change in retention basin plan.

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32	A.6.5 A.6.5 The concrete mixture used for construction of the retention basin is supplemented with an additive to improve the concrete's water resistance.		NA	TA-63 TWF Retention Basin Sealant Information	No change in presence or purpose of concrete enhancement. Final product used is a penetrating sealant (Xypex) rather than a concrete admixture type of additive (see Enclosure 2 of this document). A text revision to correct this will be made with a future permit modification description change to Permit Attachment A.6.5 for clarification.
33	A.6.6	Other Project Structures. However, it (<i>Note: the Operations Support Building</i>) provides storage of waste container data and monitoring of key operational parameters (e.g., fire alarm systems, safety equipment status indicators, and communication systems including the public address system) and specific safety structure, system, and component status.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in site layout of structures outside of permitted unit.
34	A.6.6	Vehicle access to the hazardous waste management unit is through a gated driveway located east of the concrete pad. Gates are kept closed and vehicle access to the controlled area within the unit fence line requires check-in at the Operations Support Building. Pedestrian access to the controlled area also requires check-in through the Operations Support Building.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in site layout of structures outside of permitted unit.
35	A.6.6	A fire water supply tank and a utility building that houses two fire water pumps and instrumentation needed to ensure operation of the fire suppression system are located to the north of the Operations Support Building outside the controlled area fence.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in site layout of structures outside of permitted unit.
36	A.6.6		TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in site layout.

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37	A.6.7			DWG-102355-C55443-C-1000; DWG-102355-C55443-C-1021	Revision to replace security fence with security barrier included in TWF Construction Upgrades Permit Modification of March 11, 2016. Revised Fig. 55, Attachment N, Permit. Three pedestrian emergency egress gates (crash gates) have been added to the fence line for emergency exit only from the permitted unit area and this will be resolved with a future permit modification description change to Permit Attachment A.6.7 and Figure 55 for clarification (See Item 67).
38	A.6.7	Two vehicle access gates are integrated into the fence line.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change in site layout.
39	A.6.8	Required Equipment. The TWF is equipped with safety-alarm systems to alert personnel in the event of an emergency and to evacuate the area. The facility monitor/control system is located in the access control station at the TWF; the system is also connected to the Los Alamos County Consolidated Dispatch Center.	NA	DWG-102355-C57217-F-1002; DWG-102355-C57217-F-6000	Schematic of safety alarms in Operations Building
40	A.6.8	Fire-alarm pull boxes and/or drop box push-button alarms are located pursuant to NFPA standards in the TWF where waste management activities are conducted.	NA	DWG-102355-C57217-F-1003; DWG-102355-C57217-F-6001	Storage building layouts for fire alarm manual pull stations.
41	A.6.8	Once manually activated, an alarm will sound in the TWF access control station and at the LAFD through Los Alamos County Consolidated Dispatch Center.	NA	DWG-102355-C57217-F-6002	Schematic of safety alarms in Operations Building
42	A.6.8			DWG-102355-C57217-F-6002	Schematic of safety alarms in storage buildings and Operations Building.
43	A.6.8		NA	DWG-102355-C57217-F-6002	Schematic of safety alarms in storage buildings and Operations Building.

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44	A.6.8	In addition to the alarms described above, a public address (PA) system is available to announce emergency conditions or to initiate an evacuation at the TWF. The PA system is audible throughout the TWF and is activated from the access control station in the Operations Support Building.	NA	DWG-102355-C55443-E-6003	Paging system block diagram.
45	A.6.8	Fire hydrants are located in accordance with NFPA standards on the west and east sides of the TWF pad and near the Operations Building. Water is supplied to the fire hydrants by a municipal water system which can provide adequate volume and pressure (i.e., greater than 1,000 gal per minute and 90 pounds per square inch static pressure) to multiple water hoses in the event of a fire.	NA	DWG-102355-C55443-C-1007; Hydraulic Calculation 14055020 FP-CAL-001	Fire hydrant locations (Note 10). Testing showed that a supplemental 200,000 gallon water tank and fire water pumps were needed to meet the flow and pressure requirements of the fire hydrants.
46	A.6.8	Fire protection systems for the TWF storage buildings, including the Storage and Characterization Building 63-0154, include a wet-pipe sprinkler system for fire suppression.	TWF PMR, Figure 2-16, C55444, F- 1000; TWF PMR, Figure 2-27, C55445, F-1000	DWG-102355-C57218-F-1003; DWG-102355-C57218-F-1008	Revision from wet-pipe sprinkler system to dry-pipe sprinklers system included in TWF Design Updates Permit Modification, July 28, 2014.
47	A.6.8	Water will be supplied via the 196,000 gallon tank north of the Operations Support Building with a combination of electric fire water pumps backed up with a diesel generator to distribute water to automatic sprinkler systems in the buildings.	TWF PMR, Figure 2-5, C55443, C-1000	DWG-102355-C55443-C-1000	No change to location of fire suppression water storage tank (63-0148) or fire water pump station (63-0147). Revision to fire water storage tank volume, fire pump description, and generator location (Note 18) included in TWF Construction Upgrades Permit Modification Request (PMR) Supplement of September 1, 2016.
48	A.6.8	Personnel decontamination equipment at the TWF includes safety showers and eye wash stations located inside each of the storage buildings. These are situated in all waste storage buildings in accordance with OSHA requirements.	TWF PMR, Figure 2-18, C55444, P- 5000	DWG-102355-C55444-P-5000; DWG-102355-C55445-P-5000; DWG-102355-C55444-P-1000; DWG-102355-C55445-P-1000	No change in safety shower and eyewash stations specifications or locations.

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49	A.6.9	Control of Run-on/Run-off. Controlling run-on and run-off at the TWF locations where waste management operations occur is accomplished by the design of the buildings and the use of control structures with appropriate contouring of surface areas. Run-on of storm water into the storage buildings is prevented by walls that enclose raised floors and surface contouring that slopes away from the building to prevent storm water from pooling against the foundations, doors, and loading areas. The internal floors of the buildings are sloped toward the front doors to prevent flooding by precipitation or storm water in addition to providing internal drainage to the outside.	TWF PMR, Figure 2-10, C55444, S-	DWG-102355-C55443-C-1003; DWG-102355-C55444-S-1000; DWG-102355-C55445-S-1000	No change in concrete pad slope function or internal slope of storage building floors.
50	A.6.9	The concrete pad within the permitted unit at the TWF site is sloped in a range from 1.1% to 2.5% to promote drainage to the retention pond.	TWF PMR, Figure 2-6, C55443, C-1003	DWG-102355-C55443-C-1003; DWG-102355-C55443-C-1004B	No change in site grading of permitted unit that would affect purpose of the retention basin. Range of pad slopes revised by TWF Construction Upgrades Permit Modification Request (PMR) Supplement of September 1, 2016.
51	A.6.9	A retention wall prevents slope failure between the surrounding roads and the site.	TWF PMR, Figure 2-6, C55443, C-1003	DWG-102355-C55443-C-1003	No change in location of retaining wall (Note 2).
52	A.6.10	Subsurface Vapor Monitoring. The Permittees shall install a subsurface vapor monitoring network consisting of a minimum of five vapor monitoring wells in the vicinity of the buildings located within the TWF facility to evaluate for vapor-phase contaminants that may migrate from MDA C.	included in the TWF PMR. Added to	TA-63 TWF Soil Vapor Monitoring System Report, October 29, 2015	No change in well number or purpose for monitoring system
53	A.6.10	Two of the monitoring wells must be located as close as possible to the building foundations that are adjacent to the unit boundary facing MDA C and the utility corridor on Puye Road as depicted by locations VMW-1 and VMW-2 on Figure 56 in Attachment N (Figures).	included in the TWF PMR. Added to	TA-63 TWF Soil Vapor Monitoring System Report, October 29, 2015	No change in location of monitoring wells VMW-1 and VMW-2.
54	A.6.10	A third monitoring well must be located at a point on the western edge of the permitted unit as close as possible to the utility corridor on Pajarito Road as depicted by location VMW-3 on Figure 56.	included in the TWF PMR. Added to	TA-63 TWF Soil Vapor Monitoring System Report, October 29, 2015	No change in location of monitoring well VMW-3

Item No.	Permit Section	Requirement	Permit Modification Request Documentation (TWF PMR, August 18, 2011)	Construction Documentation	Notes
55	A.6.10	Two monitoring wells must be located between MDA C and Puye Rd as depicted by locations VMW-4 and VMW-5 on Figure 56.	Soil Vapor Monitoring System was not included in the TWF PMR. Added to LANL Hazardous Waste Facility Permit with approval December 19, 2013.	TA-63 TWF Soil Vapor Monitoring System Report, October 29, 2015	Location of VMW-4 revised by October 29, 2015 Report and Permit Figure 56 revised by TWF Construction Upgrades Permit Modification of March 11, 2016
56	A.6.10	Vapor monitoring wells VMW-1, VMW-2, and VMW-3 shall be constructed with a single vapor monitoring port located in the center of a sampling interval between 5 ft and 10 ft below ground surface (bgs). Vapor monitoring wells VMW-4 and VMW-5 shall be constructed with two vapor monitoring ports located at 25 ft and 60 ft below ground surface (bgs). Boreholes will be advanced using hollow stem auger drilling methods. The vapor monitoring wells shall be constructed utilizing the same type of stainless steel (SS) tubing sampling system used at Vapor Monitoring Well 50-613183 at MDA C.	Soil Vapor Monitoring System was not included in the TWF PMR. Added to LANL Hazardous Waste Facility Permit with approval December 19, 2013.	TA-63 TWF Soil Vapor Monitoring System Report, October 29, 2015	No change in construction of monitoring wells VMW-1, VMW- 2, or VMW-3.
57	A.6.10	Well boreholes for VMW-1, VMW-2, and VMW-3 must be advanced to the design depth of 10 ft bgs. A continuous 0.25 inch stainless steel sampling tube with a screened end opening must then be placed in the borehole centered in the sampling interval (5 ft to 10 ft bgs) depth and clean sand filter pack added as the auger(s) are withdrawn to create a vapor permeable medium in the interval 5 ft to 10 ft bgs. The vapor monitoring wells must then be sealed with 2.5 ft of hydrated bentonite clay overlain by 2 ft of bentonite-cement grout.		TA-63 TWF Soil Vapor Monitoring System Report, October 29, 2015	No change in sampling interval for monitoring wells VMW-1, VMW-2, or VMW-3.
58	A.6.10	Well boreholes for VMW-4 and VMW-5 must be advanced to the design depth of 67.5 ft bgs. A minimum 5 ft hydrated bentonite clay plug must be placed above and below each sampling interval. A continuous 0.25 inch stainless steel sampling tube with a screened end opening must be placed in the borehole centered in the 5-foot sampling intervals and clean sand filter pack added as the auger(s) are withdrawn to create a vapor permeable medium in the intervals from 62.5 ft to 57.5 ft bgs and 22.5 ft to 27.5 ft bgs. Bentonite chips shall fill the borehole between sampling interval hydrated bentonite plugs and from the top of the 25 ft sampling interval to 5.5 ft bgs and overlain by a 5 ft bentonite cement grout surface seal.	Soil Vapor Monitoring System was not included in the TWF PMR. Added to LANL Hazardous Waste Facility Permit with approval December 19, 2013.	TA-63 TWF Soil Vapor Monitoring System Report, October 29, 2015	No change in sampling interval for monitoring wells VMW-4 or VMW-5.
59	A.6.10	Final construction of the vapor monitoring wells requires the installation of surface completions consisting of traffic-rated, flush-mount steel surface monuments. The Permittees shall take measures to ensure that the surface monuments will not be damaged by snow removal or other maintenance equipment.	Soil Vapor Monitoring System was not included in the TWF PMR. Added to LANL Hazardous Waste Facility Permit with approval December 19, 2013.	TA-63 TWF Soil Vapor Monitoring System Report, October 29, 2015	Change to flush mount well completions included in TWF Design Updates Permit Modification, July 28, 2014. Well casings are above ground and protected by bollards.

Item No.	Permit Section	Requirement	Permit Modification Request Documentation (TWF PMR, August 18, 2011)	Construction Documentation	Notes
60		Fire Control Equipment. Flame or smoke detection equipment and fire alarm pull stations are located within structures at TA-63-0149, TA-63-0150, TA-63-0151, TA-63-0152, TA-63-0153, and TA-63-0154.	NA	DWG-102355-C55443-F-0001; DWG-102355-C55444-F-1001; DWG-102355-C55445-F-1001	Location of fire alarm pull stations and smoke detectors in storage buildings
61	Table D-4	Dry-pipe fire suppression systems are available at TA-63-0149, TA-63-0150, TA-63-0151, TA-63-0152, TA-63-0153, and TA-63-0154.	TWF PMR, Figure 2-16, C55444, F- 1000; TWF PMR, Figure 2-27, C55445, F-1000	DWG-102355-C55444-F-1000; DWG-102355-C55445-F-1000	Revision from wet-pipe sprinkler system to dry-pipe sprinklers system included in TWF Design Updates Permit Modification, July 28, 2014.
62	Table D-4	Fire alarm pull stations are available at TA-63-0145, TA-63-0149, TA-63-0150, TA-63-0151, TA-63-0152, TA-63-0153, TA-63-0154, TA-63-0155, TA-63-0156, and TA-63-0157.	NA	DWG-102355-C55443-F-0001; DWG-102355-C55444-F-1001; DWG-102355-C55445-F-1001	Location of fire alarm pull stations in storage buildings.
63	Table D-4	Two fire hydrants are located in TWF. These fire hydrants supply water at an adequate volume and pressure to satisfy the requirements of 40 CFR 264.32(d).	NA	DWG-102355-C55443-C-1007	Location of fire hydrants in TWF.
64	Table D-4	Communication Equipment. Telephones and the public address system are located inside the Operations Support Building.	NA	DWG-102355-C55443-E-6003	No change in location of telephones or public address system.
65	Table D-4	Employees can be notified of an emergency situation and appropriate response action through the public address system.	NA	DWG-102355-C55443-E-6003	No change in purpose of the public address system.
66	Table D-4	Fire alarm pull stations are located in the storage buildings, the receiving canopy, and at operations support building.	NA	DWG-102355-C57217-F-1002; DWG-102355-C57217-F-1005; DWG-102355-C57217-F-1010; DWG-102355-C57217-F-5002	Receiving canopy structure (TA- 63-0145) removed by the Construction Updates Permit Modification of March 11, 2016.
67	Figure 55	Technical Area (TA) 63 Transuranic Waste Facility Site	NA	DWG-10235-C55443-C-1000; DWG-10235-C55443-C-5006	Three pedestrian emergency egress gates (crash gates) have been added to the fence line for emergency exit only from the permitted unit area and this will be resolved with a future permit modification description change to Figure 55 for clarification.

ENCLOSURE 2

Technical Area 63 Transuranic Waste Facility Container Storage Unit Construction Drawings and Information

EPC-DO-16-361

LA-UR-16-29607

Date: JAN 1 3 2017

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Contents:

A. Figures

- B. Hydraulic Calculation 14055020-FP-C-001
- C. TA 63 TWF Retention Basin Sealant Information
- D. TA63 TWF Storage Building Floor Coating

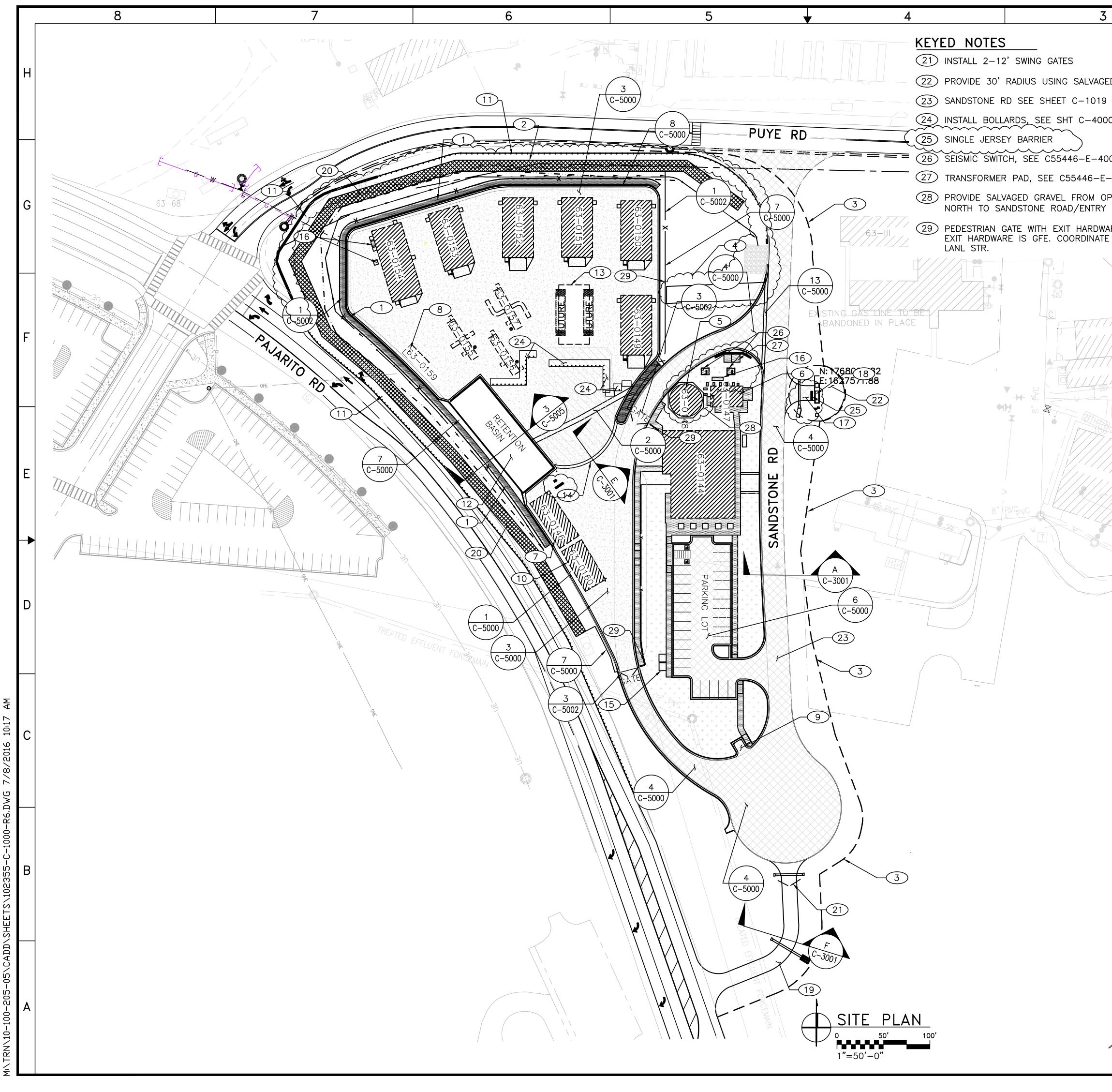
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Figures

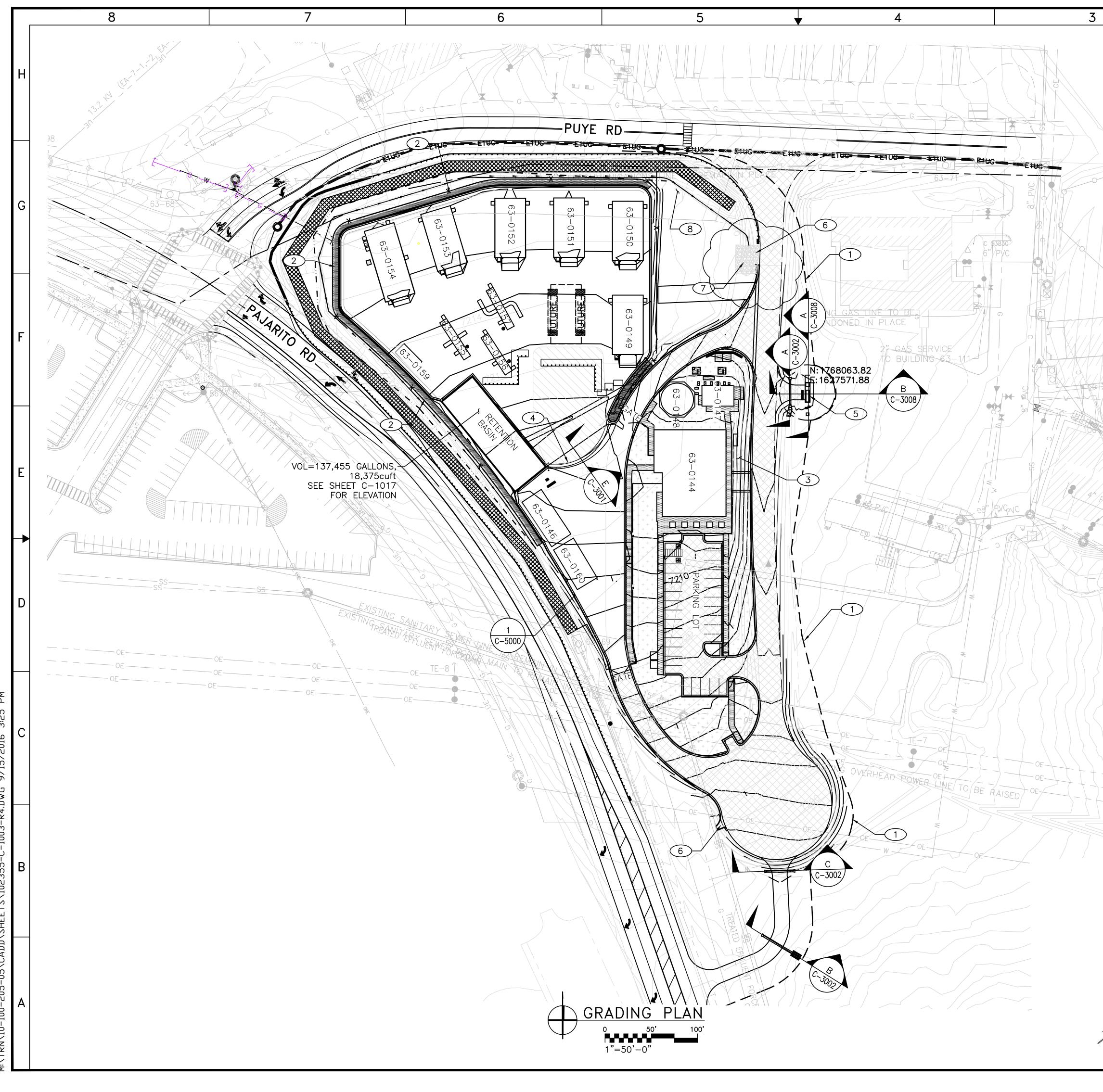
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No.	Drawing Identification	Description
1	DWG-102355-55443-C-1000	Overall Site Plan
2	DWG-102355-55443-C-1003	Overall Grading Plan
3	DWG-102355-55443-C-1004B	LIDAR Image Grading Plan
4	DWG-102355-55443-C-1007	Fire Protection Site Plan
5	DWG-102355-55443-C-1017	Retention Basin Foundation Plan
6	DWG-102355-55443-C-1021	Overall Metalith Barrier Plan
7	DWG-102355-55443-C-3001	Sandstone Road Typical Section
8	DWG-102355-55443-C-5000	Miscellaneous Details
9	DWG-102355-55443-C-5006	Miscellaneous Details
10	DWG-102355-55443-E-6003	Operations Support Building – Electrical Diagrams
11	DWG-102355-55443-F-1001	Operations Support Building – Symbol Legend and General Notes
12	DWG-102355-55444-A-1050	Storage Building – Floor Plan
13	DWG-102355-55444-A-1051	Storage Building – Roof Plan
14	DWG-102355-55444-A-3002	Storage Building – Wall Section
15	DWG-102355-55444-F-1000	Storage Building – Fire Protection Plan
16	DWG-102355-55444-F-1001	Storage Building – Fire Detection and Alarm Plan
17	DWG-102355-55444-M-1000	Storage Building – HVAC Plan
18	DWG-102355-55444-M-6000	Storage Building – HVAC Flow Diagram
19	DWG-102355-55444-P-1000	Storage Building – Plumbing Plan
20	DWG-102355-55444-P-5000	Storage Building - Details
21	DWG-102355-55444-S-0002	Storage Building – General Structural Notes
22	DWG-102355-55444-S-1000	Storage Building – Foundation Plan
23	DWG-102355-55444-S-3000	Storage Building – Structural Sections
24	DWG-102355-55444-S-5010	Storage Building – Foundation Details
25	DWG-102355-55445-A-1050	Storage and Characterization Building – Floor Plan
26	DWG-102355-55445-A-3002	Storage and Characterization Building – Wall Section
27	DWG-102355-55445-F-1000	Storage and Characterization Building – Fire Protection Plan
28	DWG-102355-55445-F-1001	Storage and Characterization Building – Fire Detection and Alarm Plan

29	DWG-102355-55445-M-1000	Storage and Characterization Building – HVAC Plan
30	DWG-102355-55445-M-6000	Storage and Characterization Building – HVAC Flow Diagram
31	DWG-102355-55445-P-1000	Storage and Characterization Building – Plumbing Plan
32	DWG-102355-55445-P-5000	Storage and Characterization Building - Details
33	DWG-102355-55445-S-1000	Storage and Characterization Building – Foundation Plan
34	DWG-102355-55445-S-5010	Storage and Characterization Building – Foundation Details
35	DWG-102355-C57217-F-1002	Floor Plan Building 144
36	DWG-102355-C57217-F-1003	Floor Plan Building 146
37	DWG-102355-C57217-F-1005	Floor Plan Building 149
38	DWG-102355-C57217-F-1010	Floor Plan Building 154
39	DWG-102355-C57217-F-5002	Details
40	DWG-102355-C57217-F-6000	FCP-1 Functional Matrix
41	DWG-102355-C57217-F-6001	FCP-2 (FAP) Functional Matrix
42	DWG-102355-C57217-F-6002	SLC Riser Diagram
43	DWG-102355-C57218-F-1003	Fire Sprinkler Floor Plan Storage Building 149
44	DWG-102355-C57218-F-1008	Fire Sprinkler Floor Plan Storage Building 154
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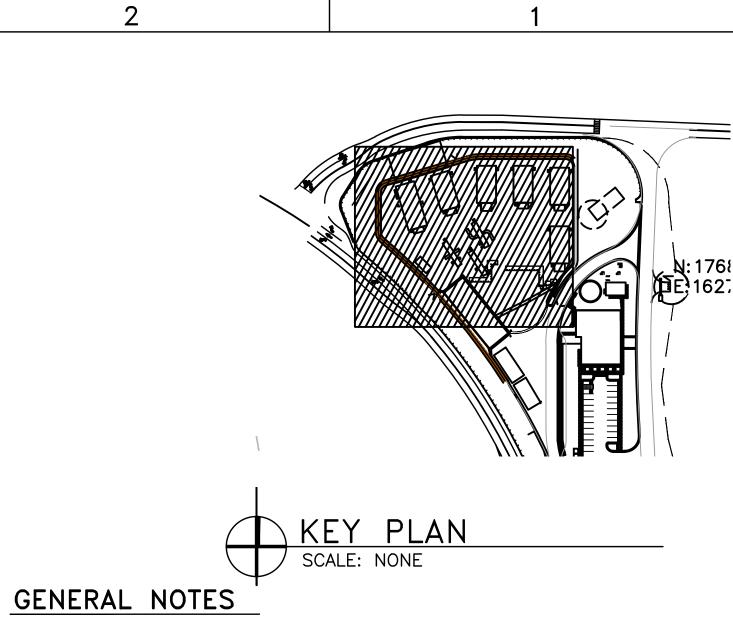


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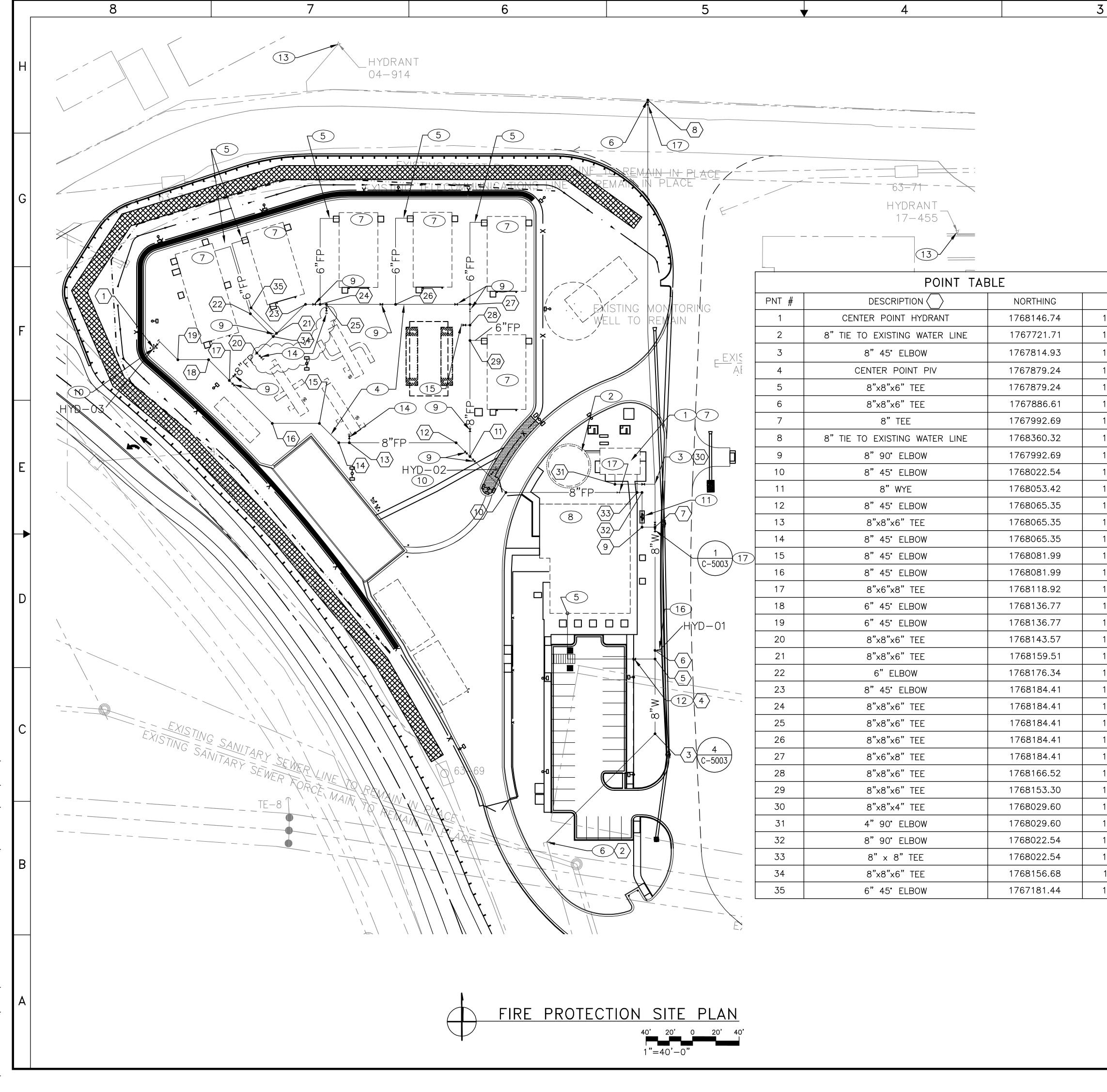
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- 3. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
- 4. STORAGE BUILDINGS, OPERATIONS SUPPORT BUILDING, UTILITY BUILDING, TRAILER COMPLEX AND YARD ARE SEPARATE FIRE AREAS.
- 5. ALL FIRE WATER PIPE SHALL HAVE A MINIMUM COVER DEPTH OF 4 FEET.
- 6. REFER TO SHEET C-1006 FOR SITE UTILITY COORDINATION AND SHEET C-3001 FOR UTILITY SECTIONS.
- 7. A STABLE PIPE BED SUCH AS BACKFILLING AROUND FIRE PROTECTION PIPING TO A HEIGHT OF 18 INCHES OF SAND BEDDING (FROM OUTSIDE OF PIPING) SHALL BE PROVIDED.

KEYED NOTES

- (1) UTILITY BUILDING WITH ELECTRIC FIRE PUMPS.
- (2)SAFETY SIGNIFICANT FIRE WATER STORAGE TANK (200,000 GALLON).
- (3)CONNECTION TO WATER MAIN FOR 4" FIRE WATER STORAGE TANK FILL LINE WITH ALTITUDE VALVE LOCATED IN UTILITY BUILDING.
- SAFETY SIGNIFICANT FIRE PROTECTION MAIN LINE. (4)
- 5 CONNECTION TO FIRE PROTECTION RISER.
- 6 CONNECTION TO WATER MAIN. SUBCONTRACTOR TO BRING PIPE TO WITHIN APPROXIMATELY 3 FEET OF CONNECTION AND PROVIDE ALL MATERIALS AND COORDINATE WITH LANL UTILITIES TO MAKE FINAL TIE-IN.
- (7)SAFETY SIGNIFICANT AUTOMATIC WET PIPE SPRINKLER SYSTEM FEEDING DRY PIPE SYSTEM IN STORAGE BUILDING.
- 8 AUTOMATIC WET PIPE SPRINKLER SYSTEM FEEDING DRY PIPE SYSTEM IN STORAGE BUILDING.
- 9 PROVIDE LOCKABLE DEBRIS CAP (DC 825) BY SW SERVICES, LLC. OR APPROVED EQUAL.
- (10)SAFETY SIGNIFICANT FIRE HYDRANT, SEE DETAIL 2/C-5006.
- $\checkmark \checkmark \checkmark \checkmark \checkmark \checkmark \checkmark$ BACKFLOW PREVENTER ASSEMBLY AND HOT BOX. SEE DETAIL (11)
- 1/C-5019.
- (12)POST INDICATOR VALVE, SEE DETAIL 4/C-5006.
- (13)GENERAL LOCATION OF EXISTING FIRE HYDRANT USED FOR FIRE HYDRANT FLOW TEST. (14)
- -6."FIRE PROTECTION LINE TO CHARACTERIZATION TRAILERS WITH LOCKABLE DEBRIS CAP. TERMINATE VALVE AND BLIND PLANGE AS CLOSE AS POSSIBLE TO MAIN.
- (15) ~6"~FIRE~PROTECTION~STUB-OUT TO FUTURE BUILDING OR TRAILER WITH LOCKABLE DEBRIS CAP. TERMINATE VALVE-AND-BLIND FLANGE-AS-CLOSE-AS-POSSIBLE FO-MAIN.~ 16
- FIRE HYDRANT, SEE DETAIL 2/C-5006. (17)

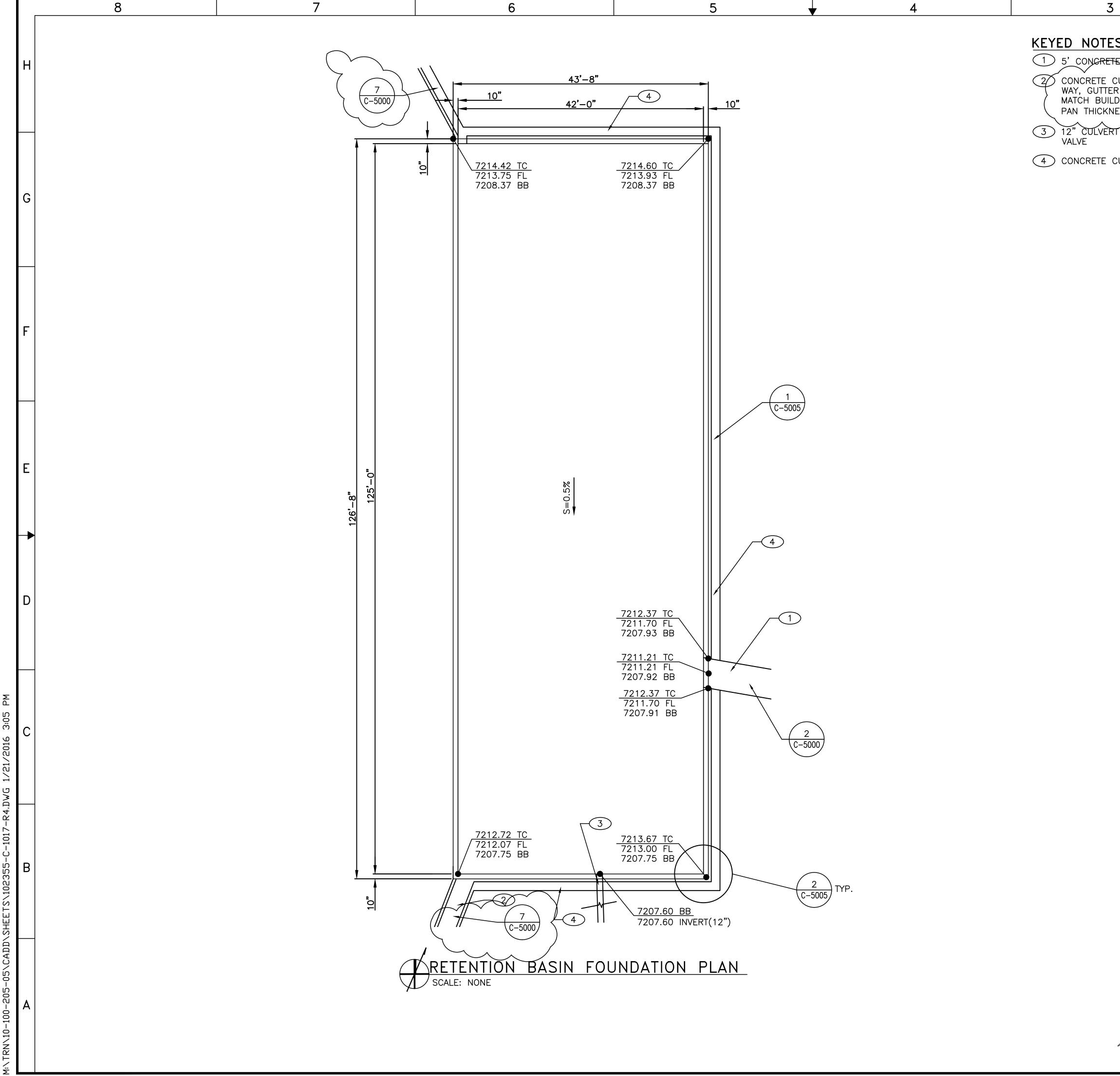
GATE VALVE WITH VALVE BOX, SEE DETAILS ON C-5003.

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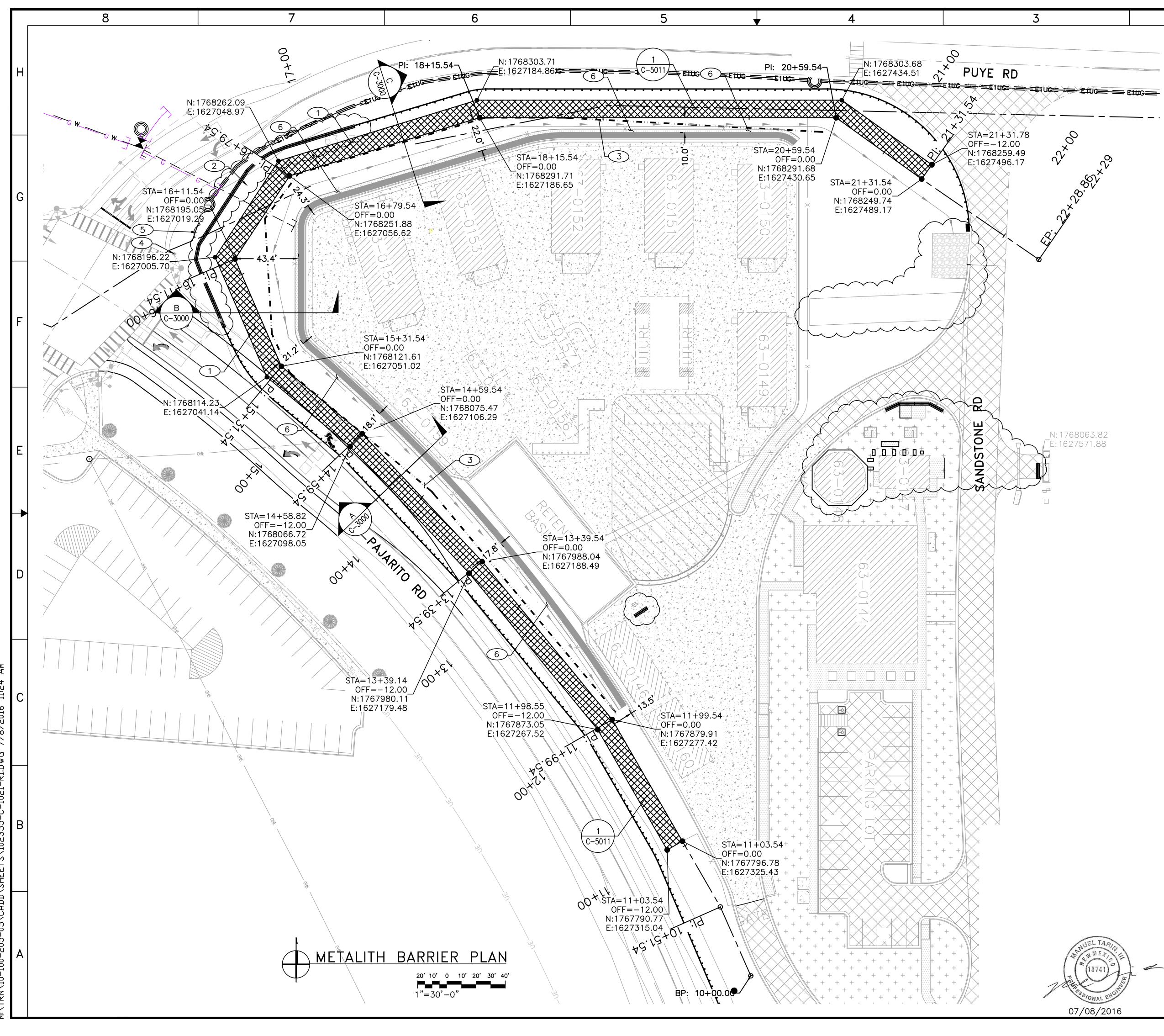


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ES	GENERAL STRUCTURAL NOTES 1. CODES AND STANDARDS:									
TE VALLEY GUTTER	LANL ENGINEERING STANDARDS MANUAL (ESM)—ISD 341—2, CHAPTER 5									
CURB AND GUTTER ŠP ER PAN CAN VARY TO LDING CONTOUR. MAX NESS TO BE 8".	DOE-STD-1020 "NATURAL PHENOMENA HAZARDS DESIGN AND EVALUATION CRITERIA FOR DEPARTMENT OF ENERGY FACILITIES"									
RT PIPE WITH GATE	DOE-STD-1201-93 "NATURAL PHENOMENA HAZARDS PERFORMANCE CATEGORIZATION CRITERIA FOR STRUCTURES, SYSTEMS AND COMPONENTS"									
CURB & GUTTER	DOE-STD-1189-2008, "INTEGRATION OF SAFETY INTO THE DESIGN PROCES	ss"								
	ASCE-7-05 MINIMUM DESIGN LOADS FOR BUILDINGS AND OTHER STRUCTUR	RES								
	INTERNATIONAL BUILDING CODE IBC-2006									
	ACI 318–08 "BUILDING CODE REQUIREMENTS FOR STRUCTURE CONCRETE" CODE AND COMMENTARY									
	ASCE 4–98 SEISMIC ANALYSIS OF SAFETY–RELATED NUCLEAR STRUCTURES AND COMMENTARY									
	ACI 349–01 CODE REQUIREMENTS FOR NUCLEAR SAFETY RELATED CONCRE STRUCTURES	TE								
	BROOKHAVEN NATIONAL LABORATORY, BNL-BNL-52361, SEISMIC DESIGN AN EVALUATION GUIDELINES FOR THE DOE HIGH-LEVEL WASTE STORAGE TANKS AND APPURTENANCES									
	GEOTECHNICAL REPORT WNNNM JV NO.: 11-002-GRPT-002									
	ACI 350.2R—04 CONCRETE STRUCTURES FOR CONTAINMENT OF HAZARDOUS MATERIALS									
	2. DESIGN DATA:									
	REINFORCED CONCRETE FOUNDATIONS – NOMINAL WEIGHT (150 pcf) REINFORCED CONCRETE COMPRESSIVE STRENGTH f'c = 4.0 ksi AT 28 DAYS									
	GRADE 60 REINFORCING STEEL-DEFORMED BARS AND STIRRUPS, ASTM A615, fy = 60 ksi									
	MINIMUM SPLICE LENGTH FOR CONTINUOUS #5 REINFORCING = $2'-2"$ AND FOR #6 REINFORCING = $2'-7"$.									
	RETENTION BASIN SLAB & WALLS SHALL BE WATER CURED PER SPECIFICATIONS.									
	DO NOT BACKFILL WALLS UNTIL CONCRETE HAS OBTAINED FULL 28 DAY STRENGTH. BACKFILL EVENLY AROUND BASIN.									
	SEISMIC LOADS (ESM CHAPTER 5 – STRUCTURE, ASCE 7–05, SECTION 12 REFER TO PROJECT DESIGN CALCULATIONS.	2								
	SEE SHEET C-1000 FOR LOCATION AND LAYOUT OF RETENTION BASIN.									
	3. RETENTION BASIN SHALL BE SEALED WITH XYPEX CONCRETE SEALANT OR APPROVED EQUAL IN ACCORDANCE WITH SPECIFICATION 09 9201.									
	4 01-22-16 U INCORP. FCN-057 ME MT Tun B& DRN-14-63-0144-0043									
	3 03-27-14 U UPDATE BASIN FOUNDATION ELEVATIONS CH KC TM BS 2 03-20-14 U UPDATE BASIN FOUNDATION ELEVATIONS CH KC TM BS									
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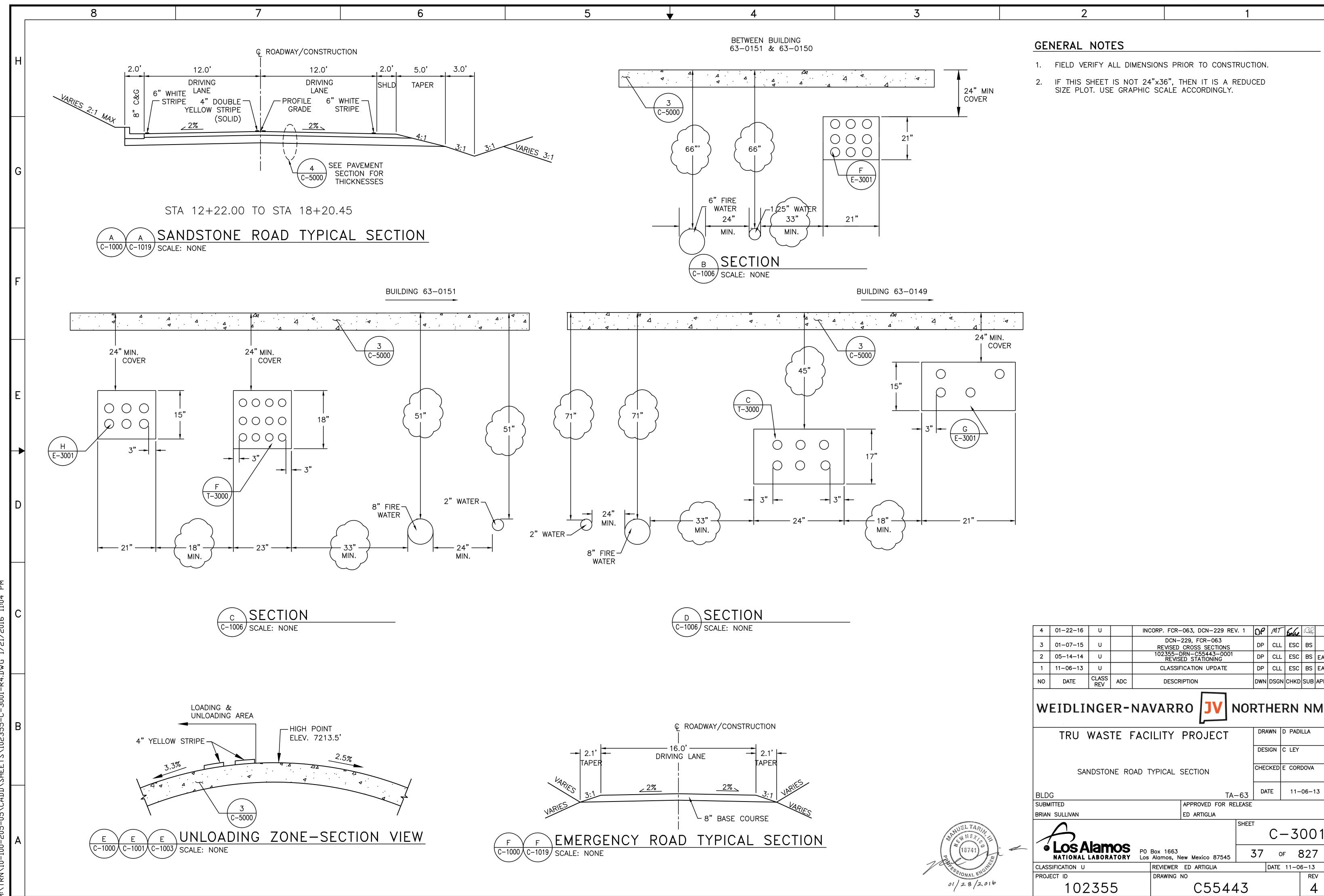
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- . FIELD VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION.
- 2. IF THIS SHEET IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.
- 3. EXISTING UTILITY LOCATIONS ARE APPROXIMATE ONLY AND SHALL BE FIELD LOCATED PRIOR TO CONSTRUCTION.
- 4. THE INTENT OF THIS SHEET IS TO GIVE AN OVERALL METALITH BARRIER PLAN VIEW. SEE SHEETS C-1022 & C-1023 FOR MORE DETAIL.
- 5. SEE TRU-WASTE FACILITY PHASE "A" SITE DESIGN AS-BUILTS FOR RETAINING WALL HEIGHT SHEETS S-1000, S-3000 AND S-3001

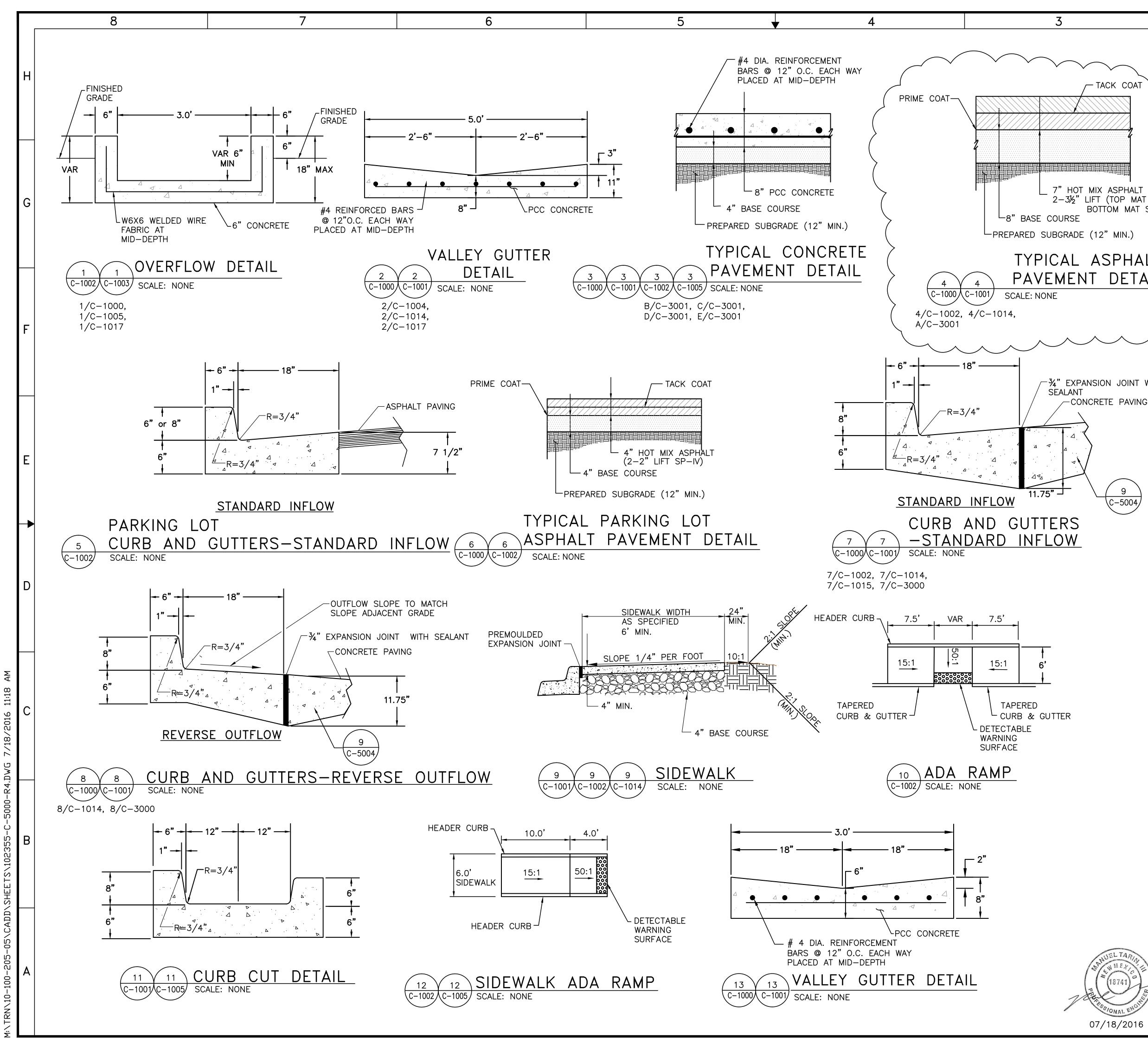
KEYED NOTES

- 1) METALITH BARRIER (INFRASTRUCTURE DEFENSE TECHNOLOGIES, LLC 3575 MORREIM DRIVE, BELVIDERE, IL 61008).
- (2) THRIE BEAM METAL BARRIER, SEE SHEET C-1025 & C-1026.
- (3) 2:1 MINIMUM OFFSET LINE FROM EXISTING RETAINING WALL.
- (4) ADJUST PULL BOX TO GRADE.
- 5 CAP AND BURY EXISTING CULVERT PIPE.
- (6) INSTALL SMOOTH 3-STRAND WIRE FENCE. SEE DETAILS ON SHEET C-5020

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3	04–19–16	U			-373 DCN 513 WALL FENCE		DP	CLL	ESC	BS	
2	12-31-14	U		FCR-	-060 DCN 221 CING AROUND META	лтн	DP	CLL	ESC	BS	EA
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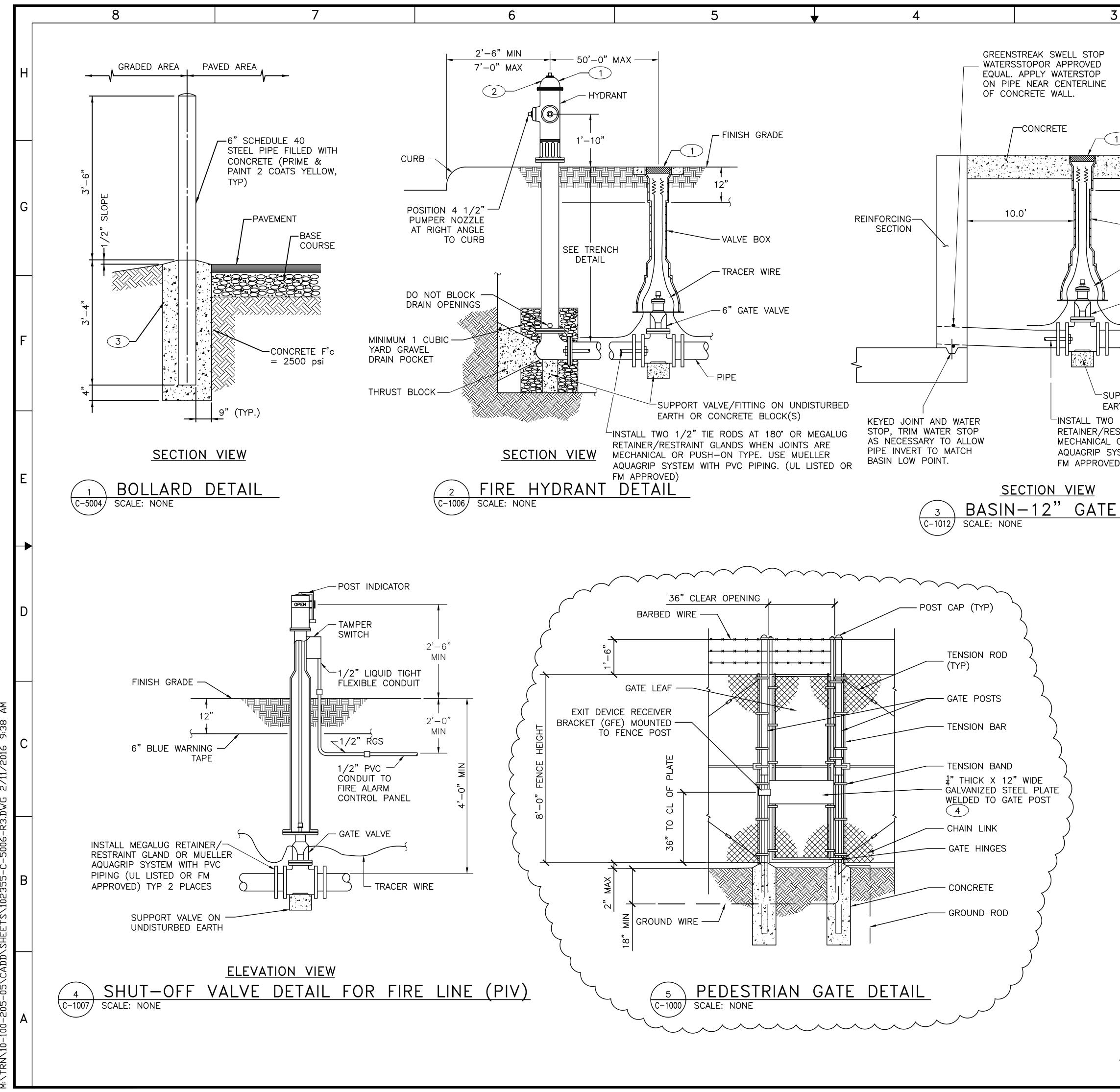
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	G	ENERAL NOTES	
	1.	REFER TO GEOTECHNICAL REF NO:11-002-GRPT-002.	PORT & WNNNM JV
	2.		S QUALITY CONSTRUCTION FORM TO SECTIONS 416, 417, 423 OF TICATIONS FOR HIGHWAY AND BRIDGE
<	3.	CONCRETE SHOULD BE PER CONCRETE OR 03 3053 MISC CONCRETE.	SPECIFICATION 03 3001 REINFORCED CELLANEOUS CAST-IN-PLACE
	4.	DETECTABLE WARNING SURFAC RECESSED INTO CONCRETE	CE (TRUNCATED DOMES) SHALL BE
7"HOT MIX ASPHALT 2—3½"LIFT (TOP MAT S BOTTOM MAT SF OURSE			CE SHALL COMPLY WITH THE LATEST HIGHWAY & BRIDGE CONSTRUCTION
BGRADE (12" MIN.)	6.		EXPANSION JOINT FILTER MATERIAL AT 5 CONTROL JOINTS. (20' MINIMUM)
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E) J		
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4" EXPANSION JOINT WI EALANT	ТН		
CONCRETE PAVING			

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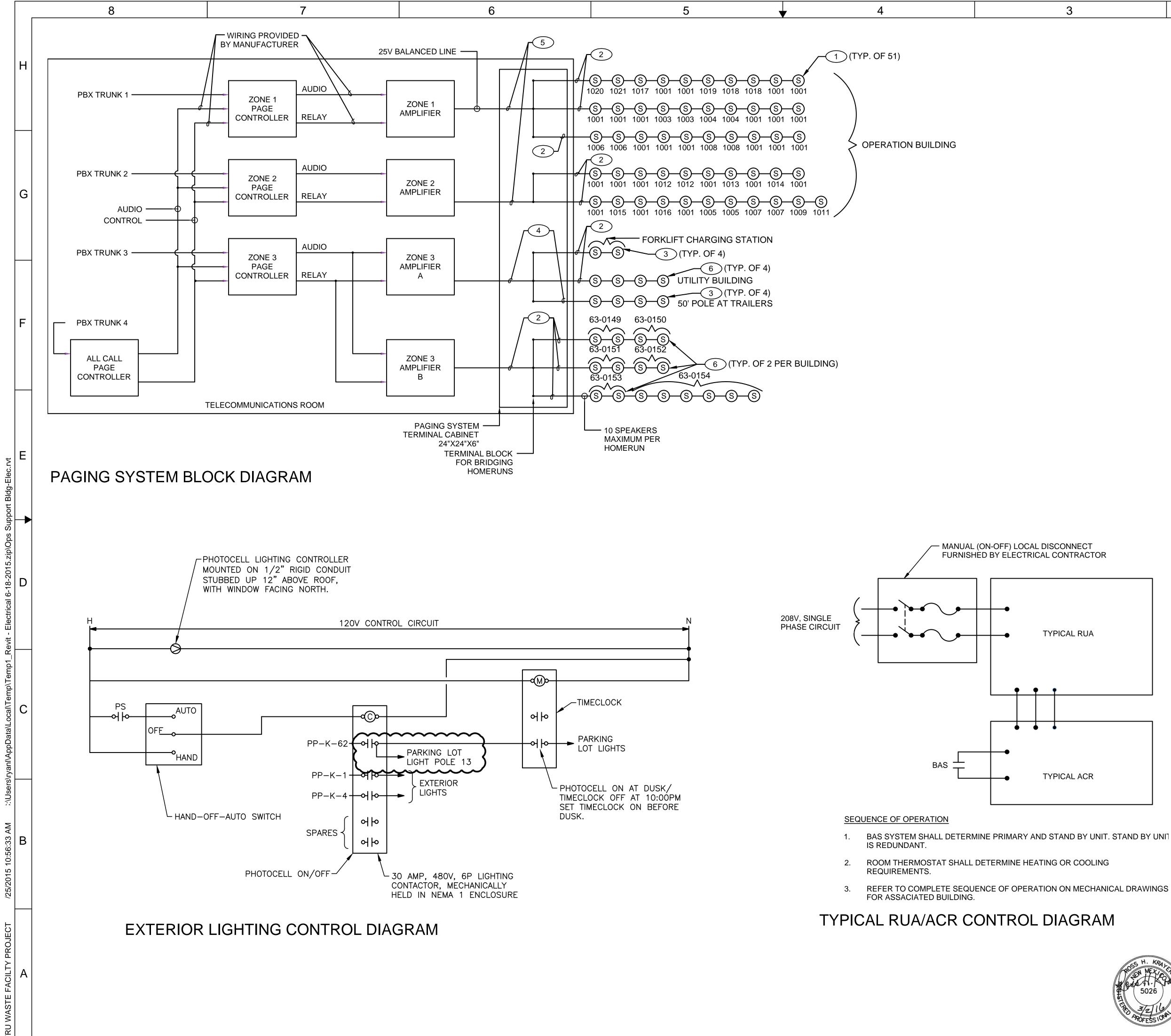
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	(1) LANL W BOX LIE		(METAL STAMP) TH	HE FIRE HYDR	ANT AND/OR VALVE
	\frown		NET BLACK AND A	ΑΤΤΛΟΗ ΙΔRFI	
FINISH GRADE			R, DO NOT DRINK		- CAUTION.
> /	(3) CONSUL	STRUCTURA	L ENGINEER OF R	FCORD BEFOR	F POURING
	CONCRE	FE FOUNDATIO	ON FOR BOLLARD	IF SIDE OF FO	OUNDATION WILL
12"			ELOW—GRADE OBJ WITHIN <u>T</u> HE HEIGH	•	
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{			ARDWARE INSTALL		
VALVE BOX	\sum	\sim	\sim	\sim	
TRACER WIRE					
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L					
PIPE TO MANHOLE					
PORT VALVE/FITTING ON U	NDISTURBED				
TH OR CONCRETE BLOCK(S					
1/2" TIE RODS AT 180° O STRAINT GLANDS WHEN JOIN					
OR PUSH-ON TYPE. USE M	IUELLER				
STEM WITH PVC PIPING. (UI))	L LISTED OR				
VALVE					
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- ROOM THERMOSTAT SHALL DETERMINE HEATING OR COOLING
- REFER TO COMPLETE SEQUENCE OF OPERATION ON MECHANICAL DRAWINGS

TYPICAL RUA/ACR CONTROL DIAGRAM



2 #16 CU TWISTED PAIR

KEYED NOTES

- 3 OUT DOOR WEATHER PROOF SPEAKERS TAPPED AT 15 WATTS

- 4 #12 CU TWISTED PAIR
- (6) OUTDOOR WEATHER PROOF SPEAKERS MOUNTED ON STRUCTURE BELOW ROOF AIMED 45 DEGREES BELOW HORIZONTAL TAPPED AT 1 WATT.
- 5 #14 CU TWISTED PAIR

(1) CEILING MOUNTED SPEAKERS TAPPED AT .5 WATTS.

DCN-493/FCR-354; UPDATED EXTERIOR LIGHTING CONTROL DIAGRAM

FCN-063; UPDATED EXTERIOR LIGHTING CONTROL DIAGRAM

DCN-395/FCR-254: UPDATED EXTERIOR LIGHTING CONTROL DIAGRAM

CLASSIFICATION UPDATE

DESCRIPTION

FCR-178/DCN-336 (RFI #335) UPDATED RL

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NATIONAL LABORATORY

TRU WASTE FACILTY PROJECT

OPERATIONS SUPPORT BUILDING

ELECTRICAL DIAGRAMS

P0 Box 1663

Los Alamos, New Mexico 87545

DRAWING NO

REVIEWER ED ARTIGLIA

USE 25 WATT CONSTANT WATTAGE BALLANCED SYSTEMS.

1) ANY TELEPHONE HANDSET CAN ACCESS THE PUBLIC ADDRESS

1) ANY TELEPHONE HANDSET CAN ACCESS THE PUBLIC ADDRESS SYSTEM BY ENTERING CODE # AND "ALL CALL" CODE #.

SYSTEM BY ENTERING CODE # AND ZONE #.

SEQUENCE OF OPERATION:

A. TO PAGE ANY ZONE -

TO PAGE ALL ZONES -

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ACV ACACAHU ANN BAS BDD BFP BOD BOP BHP BP CA CAV CONT CIE CFM CV DX DACP DV DEMO DFACF DV DEMO DFACF DV EPPENT EOLD ESS EXH • FACP FLEX FMS FPM FT. GPH	ALARM CHECK VALVE AIR CONDITIONING AIR HANDLING UNIT ANNUNCIATOR BUILDING AUTOMATION SYSTEM BACK DRAFT DAMPER BACK DRAFT DAMPER BACKFLOW PREVENTER BOTTOM OF DUCT BOTTOM OF PIPE BRAKE HORSEPOWER BTU PER HOUR BUILDING PRESSURE COMPRESSED AIR CONSTANT AIR VOLUME CONTINUATION CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	MA MIXED AIR MIN MINIMUM NA NOT APPLICABLE NAC NOTIFICATION ALARM CIRCUIT NC NORMALLY CLOSED NFPA NATIONAL FIRE PROTECTION ASSOCIATION NIC NOT IN CONTRACT NO NORMALLY OPEN NO. NUMBER (QUANTITY) OBD OPPOSED BLADE DAMPER OA OUTSIDE AIR PCM PROGRAMMABLE CONTROL MODULE P&ID PIPING & INSTRUMENTATION DIAGRAM PI PRESSURE INDICATOR PNL PANEL		FIRE DEPARTMENT CONNECTION FREE STANDING FIRE DEPARTMENT CONNECTION FIRE HYDRANT – TWO HOSE OUTLET FIRE HYDRANT – ONE HOSE OUTLET FIRE HYDRANT – TWO HOSE OUTLET & PUMPER CONN. WALL HYDRANT – TWO HOSE OUTLET WATER SYSTEM BLOCK VALVE	 ⊕ ⊕ ⊕ ⊕ CA □ D − F − 	HEAT DETECTOR HORN FIRE ALARM HORN STROBE COMPRESSED AIR DRAIN FIRE PROTECTION WATER
AHU ANN BAS BDD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BFP BOD BOP BTUH BP CA CAV CIE CFM CV DX DACP DPV DEMO DFACF DV EP ENT EOLD ESS EXH • FACP FDC FDC FDC FDC FDC FDC FDC FDC FDC FDC	AIR CONDITIONING AIR HANDLING UNIT ANNUNCIATOR BUILDING AUTOMATION SYSTEM BACK DRAFT DAMPER BACKFLOW PREVENTER BOTTOM OF DUCT BOTTOM OF PIPE BRAKE HORSEPOWER BTU PER HOUR BUILDING PRESSURE COMPRESSED AIR CONSTANT AIR VOLUME CONTINUATION CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	MA MIXED AIR MIN MINIMUM NA NOT APPLICABLE NAC NOTIFICATION ALARM CIRCUIT NC NORMALLY CLOSED NFPA NATIONAL FIRE PROTECTION ASSOCIATION NIC NOT IN CONTRACT NO NORMALLY OPEN NO. NUMBER (QUANTITY) OBD OPPOSED BLADE DAMPER OA OUTSIDE AIR PCM PROGRAMMABLE CONTROL MODULE P&ID PIPING & INSTRUMENTATION DIAGRAM PI PRESSURE INDICATOR PNL PANEL	-0- ▶ ▼ ▼	CONNECTION FREE STANDING FIRE DEPARTMENT CONNECTION FIRE HYDRANT – TWO HOSE OUTLET FIRE HYDRANT – ONE HOSE OUTLET FIRE HYDRANT – TWO HOSE OUTLET & PUMPER CONN. WALL HYDRANT – TWO HOSE OUTLET WATER SYSTEM BLOCK VALVE	H E − CA − − D − − F −	HORN FIRE ALARM HORN STROBE COMPRESSED AIR DRAIN FIRE PROTECTION WATER
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 BAS BDD BFP BOD BOP BHP BP CA CAV CONT CIE CFM CV DX DACP DPV DACP DPV DACP DPV DACP DPV DEMO DFACE DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDM FT. GPH 	SYSTEM BACK DRAFT DAMPER BACKFLOW PREVENTER BOTTOM OF DUCT BOTTOM OF PIPE BRAKE HORSEPOWER BTU PER HOUR BUILDING PRESSURE COMPRESSED AIR CONSTANT AIR VOLUME CONTINUATION CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	NACNOTIFICATION ALARM CIRCUITNACNOTIFICATION ALARM CIRCUITNCNORMALLY CLOSEDNFPANATIONAL FIRE PROTECTION ASSOCIATIONNICNOT IN CONTRACTNONORMALLY OPENNO.NUMBER (QUANTITY)OBDOPPOSED BLADE DAMPER OAOAOUTSIDE AIRPCMPROGRAMMABLE CONTROL MODULEP&IDPIPING & INSTRUMENTATION DIAGRAMPIPRESSURE INDICATOR PNLPNLPANEL	-0- ▶ ▼ ▼	FIRE HYDRANT – TWO HOSE OUTLET FIRE HYDRANT – ONE HOSE OUTLET FIRE HYDRANT – TWO HOSE OUTLET & PUMPER CONN. WALL HYDRANT – TWO HOSE OUTLET WATER SYSTEM BLOCK VALVE	— CA — — D — — F —	COMPRESSED AIR DRAIN FIRE PROTECTION WATER
 BFP BOD BOP BHP BTUH BP CA CAV CONT CIE DX DACP DV DPV DEMO DFACF DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDMP F.G. FLEX FM FMS FPM FT. GPH GPM 	BACK DRAFT DAMPER BACKFLOW PREVENTER BOTTOM OF DUCT BOTTOM OF PIPE BRAKE HORSEPOWER BTU PER HOUR BUILDING PRESSURE COMPRESSED AIR CONSTANT AIR VOLUME CONTINUATION CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	NCNORMALLYCLOSEDNFPANATIONALFIREPROTECTIONASSOCIATIONASSOCIATIONNICNOTINCONTRACTNONORMALLYOPENNO.NUMBER(QUANTITY)OBDOPPOSEDBLADEDAMPEROAOUTSIDEAIRPCMPROGRAMMABLECONTROLMODULEP&IDPIPING & INSTRUMENTATIONDIAGRAMPIPRESSUREINDICATORPNLPANELPANEL	-0- ▶ ▼ ▼	OUTLET FIRE HYDRANT – ONE HOSE OUTLET FIRE HYDRANT – TWO HOSE OUTLET & PUMPER CONN. WALL HYDRANT – TWO HOSE OUTLET WATER SYSTEM BLOCK VALVE	D F F	FIRE PROTECTION WATER
 BOD BOP BHP BTUH BP CA CAV CONT CIE DX DACP DV DPV DEMO DFACF DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDC FDC FDMP F.G. FLEX FMS FPM FT. GPH GPM 	BOTTOM OF DUCT BOTTOM OF PIPE BRAKE HORSEPOWER BTU PER HOUR BUILDING PRESSURE COMPRESSED AIR CONSTANT AIR VOLUME CONTINUATION CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	ASSOCIATION NIC NOT IN CONTRACT NO NORMALLY OPEN NO. NUMBER (QUANTITY) OBD OPPOSED BLADE DAMPER OA OUTSIDE AIR PCM PROGRAMMABLE CONTROL MODULE P&ID PIPING & INSTRUMENTATION DIAGRAM PI PRESSURE INDICATOR PNL PANEL	→ X	OUTLET FIRE HYDRANT – TWO HOSE OUTLET & PUMPER CONN. WALL HYDRANT – TWO HOSE OUTLET WATER SYSTEM BLOCK VALVE	FLOW	
 BHP BTUH BP CA CAV CONT CIE CFM CV DX DACP DPV DEMO DFACF DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDC FDC FDMP F.G. FLEX FMS FPM FT. GPH GPM 	BRAKE HORSEPOWER BTU PER HOUR BUILDING PRESSURE COMPRESSED AIR CONSTANT AIR VOLUME CONTINUATION CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	NONORMALLY OPEN NO.NO.NUMBER (QUANTITY)OBDOPPOSED BLADE DAMPER OAOAOUTSIDE AIRPCMPROGRAMMABLE CONTROL MODULEP&IDPIPING & INSTRUMENTATION DIAGRAMPIPRESSURE INDICATOR PNLPNLPANEL		OUTLET & PUMPER CONN. WALL HYDRANT – TWO HOSE OUTLET WATER SYSTEM BLOCK VALVE	FLOW	DIRECTION OF FEOM (SOFIEMAND)
 BP CA CAV CONT CIE CFM CV DX DACP DPV DEMO DFACF DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDC FDC FDMP F.G. FLEX FM FMS FPM FT. GPH GPM 	BUILDING PRESSURE COMPRESSED AIR CONSTANT AIR VOLUME CONTINUATION CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	OBD OPPOSED BLADE DAMPER OA OUTSIDE AIR PCM PROGRAMMABLE CONTROL MODULE P&ID PIPING & INSTRUMENTATION DIAGRAM PI PRESSURE INDICATOR PNL PANEL		WALL HYDRANT – TWO HOSE OUTLET WATER SYSTEM BLOCK VALVE		DIRECTION OF FLOW (GRAPHICAL)
 CAV CONT CIE CFM CV DX DACP DPV DEMO DFACF DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDC FDC FDC FDC FDC FDMP F.G. FLEX FM FMS FPM FT FT. GPH GPH 	COMPRESSED AIR CONSTANT AIR VOLUME CONTINUATION CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	OA OUTSIDE AIR PCM PROGRAMMABLE CONTROL MODULE P&ID PIPING & INSTRUMENTATION DIAGRAM PI PRESSURE INDICATOR PNL PANEL		WATER SYSTEM BLOCK VALVE		
 CAV CONT CIE CFM CV DX DACP DPV DEMO DFACF DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDC FDC FDC FDC FDC FDMP F.G. FLEX FM FMS FPM FT FT. GPH GPH 	CONSTANT AIR VOLUME CONTINUATION CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	PCM PROGRAMMABLE CONTROL MODULE P&ID PIPING & INSTRUMENTATION DIAGRAM PI PRESSURE INDICATOR PNL PANEL				REDUCER OR INCREASER
 CIE CFM CV DX DX DACP DPV DACP DPV DEMO DFACF DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDC FDC FDC FDC FDM FT. GPH GPH 	CONTRACTOR INSTALLED EQUIPMENT CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	MODULE P&ID PIPING & INSTRUMENTATION DIAGRAM PI PRESSURE INDICATOR PNL PANEL		REDUCER		ECCENTRIC REDUCER
 CV DX DACP DPV DEMO DFACE DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDC FDC FDC FDC FDM FT FT GPH GPH 	CUBIC FEET PER MINUTE CHECK VALVE DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	DIAGRAM PI PRESSURE INDICATOR PNL PANEL		ALARM VALVE	U	TOP CONNECTION, 45° OR 90°
DX D DACP DPV DEMO DFACE DV EP ENT EOLD ESS EXH *F FACP FC FD FDC FDC FDMP F.G. FLEX FM FMS FPM FT FT. GPH GPM	DIRECT EXPANSION DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER	PNL PANEL		DRY-PIPE VALVE		BOTTOM CONNECTION, 45° OR 90°
 D DACP DPV DEMO DFACE DV EP ENT EOLD ESS EXH F FACP FC FD FDC FDC FDMPI F.G. FLEX FM FMS FPM FT FT. GPH GPM 	DRAIN DIGITAL ALARM COMMUNICATOR TRANSMITTER				 	SIDE CONNECTION
 DPV DEMO DFACE DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDC FDC FDMPI F.G. FLEX FM FMS FPM FT FT. GPH GPM 	DIGITAL ALARM COMMUNICATOR TRANSMITTER	EXISTING		DELUGE VALVE	U	CAPPED OUTLET
 DEMO DFACE DV EP ENT EOLD ESS EXH F FACP FC FD FDC FDC FDMPI F.G. FLEX FM FMS FPM FT FT. GPH GPM 	TRANSMITTER	POR POINT OF REMOVAL FROM EXISTING	2	ALARM GONG		RISE OR DROP IN PIPE
 DEMO DFACE DV EP ENT EOLD ESS EXH F FACP FC FD FDC FDC FDMPI F.G. FLEX FM FMS FPM FT FT. GPH GPM 		PSIG POUNDS PER SQUARE INCH GAGE	TS	P&ID, TAMPER SWITCH	O	RISE IN PIPE
 DV EP ENT EOLD ESS EXH F FACP FC FDC FDC FDM F.G. FLEX FM FMS FPM FT FT. GPH GPH 	DEMOLISH, DEMOLITION	PRV PRESSURE REDUCING VALVE	FS	P&ID, FIRE SUPPRESSION		
 EP ENT EOLD ESS EXH F FACP FC FD FDC FDC FDMPI F.G. FLEX FM FMS FPM FT FT. GPH GPM 	CONTROL PANEL	PWC POTABLE WATER COLD		WATER FLOW SWITCH P&ID, FIRE SUPPRESSION		UNIVERSAL TEMPERATURE-PRESSUF FITTING
 ENT EOLD ESS EXH F FACP FC FDC FDC FDC FDMPI F.G. FLEX FM FMS FPM FT FT. GPH GPM 	DELUGE VALVE	QTY QUANTITY	PS	PRESSURE SWITCH		OS&Y CONTROL VALVE
EOLD ESS EXH FF FACP FC FD FDC FDC FDMP F.G. FLEX FM FMS FMS FPM FT FT. GPH GPM	ELECTRIC-PNEUMATIC ENTERING	RLA RELIEF AIR RA RETURN AIR		SPRINKLER HEAD SIDE WALL		STRAINER
 EXH F FACP FC FD FDC FDM FMS FPM FT FT. GPH GPH GPH 		RC RETARD CHAMBER	۲	SPRINKLER HEAD IN		JINAINEN
F FACP FD FDC FDC FDMP F.G. FLEX FM FMS FMS FPM FT FT. GPH GPM	SYSTEM	RPM REVOLUTIONS PER MINUTE RTU REMOTE TERMINAL UNIT		SUSPENDED CEILING W\FLEXHEAD		THERMOMETER
FACP FC FD FDC FDMPI F.G. FLEX FM FMS FMS FPM FT FT. GPH GPM	EXHAUST	SP STATIC PRESSURE (INCHES		(UNLESS OTHERWISE NOTED ON PLAN)		PRESSURE GAGE
) FD FDC FDMPI F.G. FLEX FM FMS FMS FPM FT FT. GPH GPM		OF WATER) SA SUPPLY AIR				GAUGE & GAUGE COCK
FDC FDMPI F.G. FLEX FM FMS FMS FT FT. GPH GPM	PANEL FLEXIBLE_CONNECTOR	SLC SIGNALING LINE CIRCUIT SS SAFETY SIGNIFICANT	$ \downarrow \downarrow$	RETARD CHAMBER		BALL VALVE
F.G. FLEX FM FMS FPM FT FT. GPH GPM	FLOOR DRAIN FIRE DEPT CONNECTION	SUPR SUPERVISORY SIGNAL		VALVE	۶	LINE BREAK
FLEX FM FMS FPM FT FT. GPH GPM	R FIRE DAMPER FILTER GAUGE	TX TOILET EXHAUST TYP. TYPICAL		PRESSURE REDUCING VALVE		POST INDICATING VALVE
FMS FPM FT FT. GPH GPM	FLEXIBLE FACTORY MUTUAL	UL UNDERWRITERS LABORATORIES		ANGLE VALVE		
FT FT. GPH GPM	FACILITY MANAGEMENT SYSTEM	VX VACUUM EXHAUST	P	SMOKE DETECTOR		INDICATING CONTROL VALVE
FT. GPH GPM	FEET PER MINUTE FLAT TOP	VAV VARIABLE AIR VOLUME VEL VELOCITY			ф	HEIGHING CONTINUE FALVE
GPM	FEET	VTR VENT THRU ROOF V VALVE		DUCT SMOKE DETECTOR (PHOTOELECTRIC)		GROUND VALVE
; GFE	GALLONS PER HOUR GALLONS PER MINUTE	VAC VOLTS, ALTERNATING CURRENT		UNDERGROUND PIPING		HAND VALVE
	GOVERNMENT FURNISHED EQUIPMENT	W/ WITH		ABOVEGROUND PIPING		
GIE	GOVERNMENT INSTALLED EQUIPMENT				<u> </u>	
HGT HD	HEIGHT HEAD, HUB DRAIN HIGH EFFICIENCY			AL SYMBOLS		·
HEPA	PARTICULATE ARRESTOR HAND-OFF-AUTOMATIC					
HORIZ HP	HORSEPOWER			LISTED IN THE KEYED NOTE	LIST	
HSTAT HTG	HEATING		$\left \left\langle \begin{array}{c} & & \\ & & \\ & & \\ \end{array} \right\rangle$	HYDRAULIC CALCULATION NO	DE	
HTR HVAC	HEATER HEATING, VENTILATING AND					
HW HX	AIR CONDITIONING HOT WATER			HYDRAULIC CALCULATION NOT		AS REQUIRED BY NFPA 13 (2010).
HYD HZ	HEPA EXHAUST AIR HYDRANT				WHERE LATER	AL AND LONGITUDINAL BRACES ARE
	HERTZ		<u> </u>		IAL BRACE WITH	FROM VERTICAL; MAXIMUM SPACING IN 18'-0" OF FREE END OF PIPE.
			1	LATERAL BRACE, MINIMUM 45	• ANGLE FROM	VERTICAL; MAXIMUM SPACING 30'-0".
	· · · · · · · · · · · · · · · · · · ·		<u>/</u>	PROVIDE LATERAL BRACE WIT ON SHEET F—5000.	HIN 15'-0" OF	FREE END OF PIPE. SEE DETAIL 4
	· · ·					
			-			

4

GENERAL NOTES

2

- 1. ALL STRUCTURAL WELDED CONNECTIONS SHALL BE PERFORMED IN ACCORDANCE WITH LANL APPROVED WELDING SPECIFICATION AND AWS D1.1/D1.1M SPECIFICATION FOR WELDING STEEL. ALL PIPE WELDED CONNECTIONS SHALL BE PERFORMED IN ACCORDANCE WITH LANL APPROVED WELDING SPECIFICATION AND THE APPLICABLE NFPA CODE IDENTIFIED IN THE CONSTRUCTION SPECIFICATION.
- 2. INSTALL FIRE PROTECTION SYSTEM PER NFPA 13. THE SYSTEM SHALL INCLUDE CONTROL VALVES, PIPING, FITTINGS, SPRINKLER HEADS, HANGERS, BRACING, DRAINS AND ALL OTHER DEVICES REQUIRED FOR A COMPLETE AND FUNCTIONAL SYSTEM IN ACCORDANCE WITH ALL APPLICABLE CODES. REFER TO SPECIFICATION SECTION 211313 "WET PIPE SPRINKLER SYSTEM".
- 3. THE DESIGN OF THE FIRE PROTECTION SYSTEM FOR THE BUILDINGS SHALL CONFORM TO ORDINARY HAZARD GROUP 2 REQUIREMENTS WITH 500 GPM HOSE STREAM ALLOWANCE FOR 2 HOUR DURATION.
- 4. CONCEALED SPACE ABOVE DROP CEILING MEETS THE REQUIREMENTS OF NFPA 13, SECTION 8.15.1.2 - "CONCEALED SPACES NOT REQUIRING SPRINKLER PROTECTION", THEREFORE NO SPRINKLERS WILL BE PROVIDED IN THE CONCEALED SPACE.
- 5. SYMBOLS SHOWN ON THIS SHEET ARE FOR SINGLE-LINE SCHEMATICS. DRAWINGS DEVELOPED USING REVIT SHOW MODELED PIPING AND COMPONENTS THAT ARE DRAWN TO SCALE AND NOT NECESSARILY INCLUDED IN THE SYMBOL LEGEND.

					and the second			
MAXIM	IUM DIST	ANCE BI	ETWEEN	HANGERS	5 (FT)			
NOMINAL PIPE SIZE	1"	1-1/4"	1-1/2"	2"	2-1/2"	3"		
STEEL PIPE SCHEDULE 40	12	12	15	15	15	15		
MAXIM	MAXIMUM DISTANCE BETWEEN HANGERS (FT)							
NOMINAL	3-1/2"	4"	5"	6"	8"			

SPRINKLER HANGER TABLE

15

PIPE SIZE

STEEL PIPE

SCHEDULE 40

SPRINKLER PIPING SUPPORT NOTES

15

1. THE UNSUPPORTED LENGTH BETWEEN THE END SPRINKLER AND THE LAST HANGER SHALL NOT BE GREATER THAN 36" FOR 1" PIPE, 48" FOR 1-1/4" PIPE AND 60" FOR 1-1/2" OR LARGER PIPE.

15

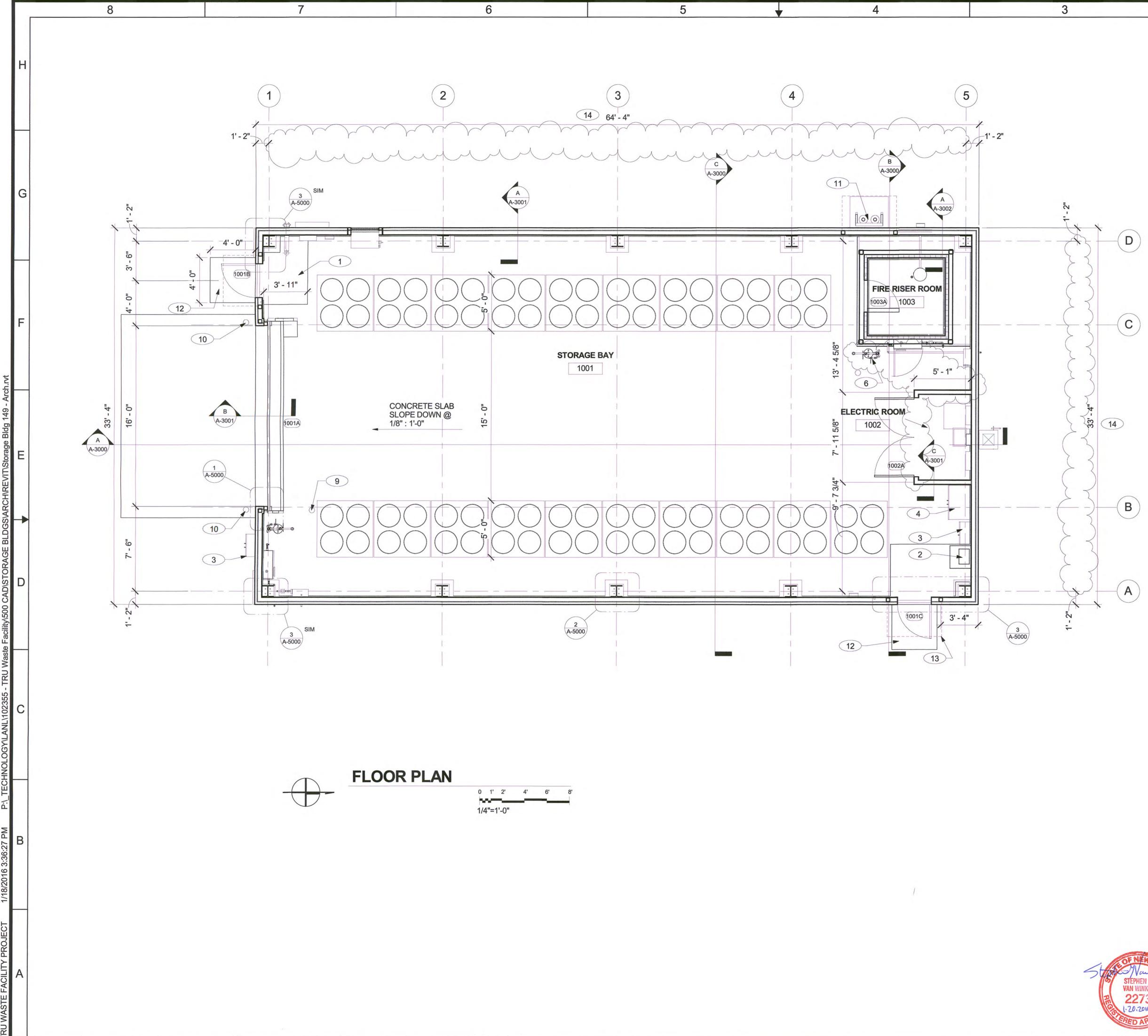
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- 2. THERE SHALL NOT BE LESS THAN ONE HANGER FOR EACH SECTION OF PIPE.
- 3. VERTICAL RISERS SHALL BE SUPPORTED WITHIN 24" OF THEIR HORIZONTAL CONNECTIONS. INTERMEDIATE SUPPORTS SHALL BE PROVIDED TO LIMIT AXIAL MOVEMENT.

	11 00 17			REVISED NOTES				m	m	24	Δ
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	OPERATIONS SUPPORT BUILDING DESIGN E. MIYODA										
	SYMBOL LEGEND AND GENERAL NOTES								CHECKED C. MOYERS		
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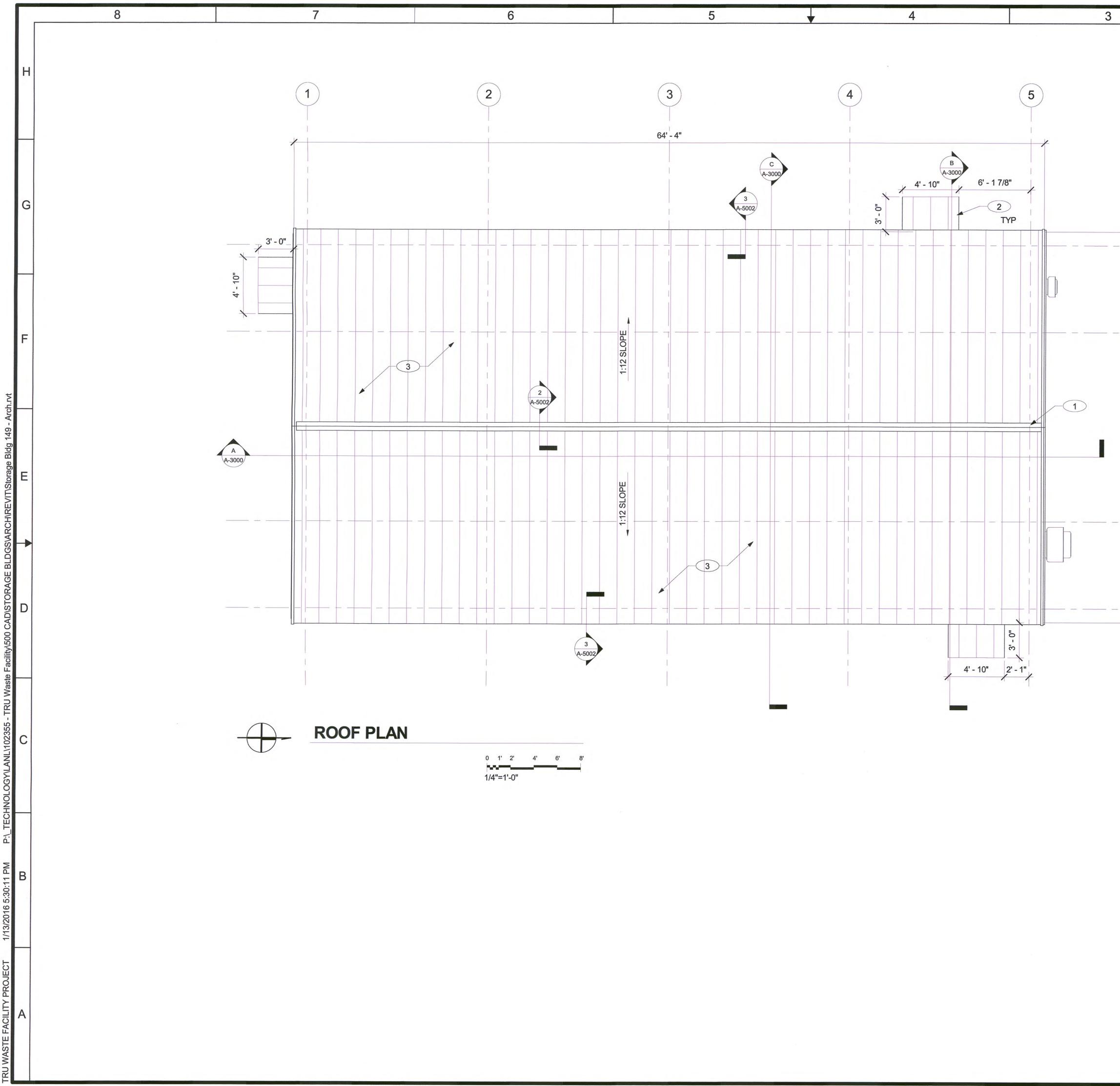




2	1
GENERAL NOTES	
1. IF THIS SHEET IS NOT 24" x 36", THE GRAPHIC SCALE ACCORDINGLY.	EN IT IS A RECUCED SIZE PLOT, USE
2. THIS DRAWING WAS GENERATED II	N REVIT 2011.
3. PALLETS AND STORAGE CANISTER	S ARE NOT IN CONCRACT.
4. 36" HIGH ABOVE FINISHED FLOOR S OUTSIDE CORNERS, TYPICAL.	STAINLESS STEEL CORNER GUARDS AT
5. SEE STRUCTURAL FOR COLUMN LI	NE DIMENSIONS.
hundred	und and a start of the start of
KEYED NOTES	
1. LANDING, SEE STRUCTURAL S	SHEET S-1000
2 COMPUTER WORK STATION S	EE DETAIL 4/A-5002
3 SPILL KIT, GFE	
4 SUPPLY CABINET, GFE	
5 DECONTAMINATION EQUIPME	NT CABINET, GFE
6 EYE WASH AND SHOWER	
7 FIRE RISER	
8 FIRE EXTINGUISHER	
9 BOLLARD, SEE DETAIL 7/A-500	02
10 PERMANENT BOLLARD, SEE D	DETAIL 7/A-5002
11 FIRE SUPPRESSION SYSTEM	NITROGEN GAS CYLINDER RACK
12 CONCRETE STOOP, TYPICAL -	SEE SHEET C55443 C-5004
13 EDGE OF AWNING ABOVE	
14 BUILDING DIMENSIONS ARE SA IS 33.8 FEET. MAXIMUM LENG	AFETY CLASS. MAXIMUM WIDTH TH IS 64.8 FEET.

3	01-15-16	υ		FCR-067/DCN-222; FCR-176/DCN-334; FCR-267/DCN-409	AG	æ	Stul	R3&	
2	05-14-14	U	EA	102355-DRN-C55444-00001 REVISED NOTE	AG	RK	RK	BS	M
1	11-06-13	υ	EA	REVISED FLOOR PLAN	AG	RK	RK	BS	E/
NO	DATE	CLASS REV	ADC	DESCRIPTION	DWN	DSGN	СНКД	SUB	AP
W	EIDL	[NGI	ER-	NAVARRO	IORT	HE	RN	N	M
W				NAVARRO			RN		
W		WAS	STE F	6	DR	AWN A		EGOS	
W		WAS	STE F	FACILITY PROJECT	DR	AWN A	A. GALL	EGOS	

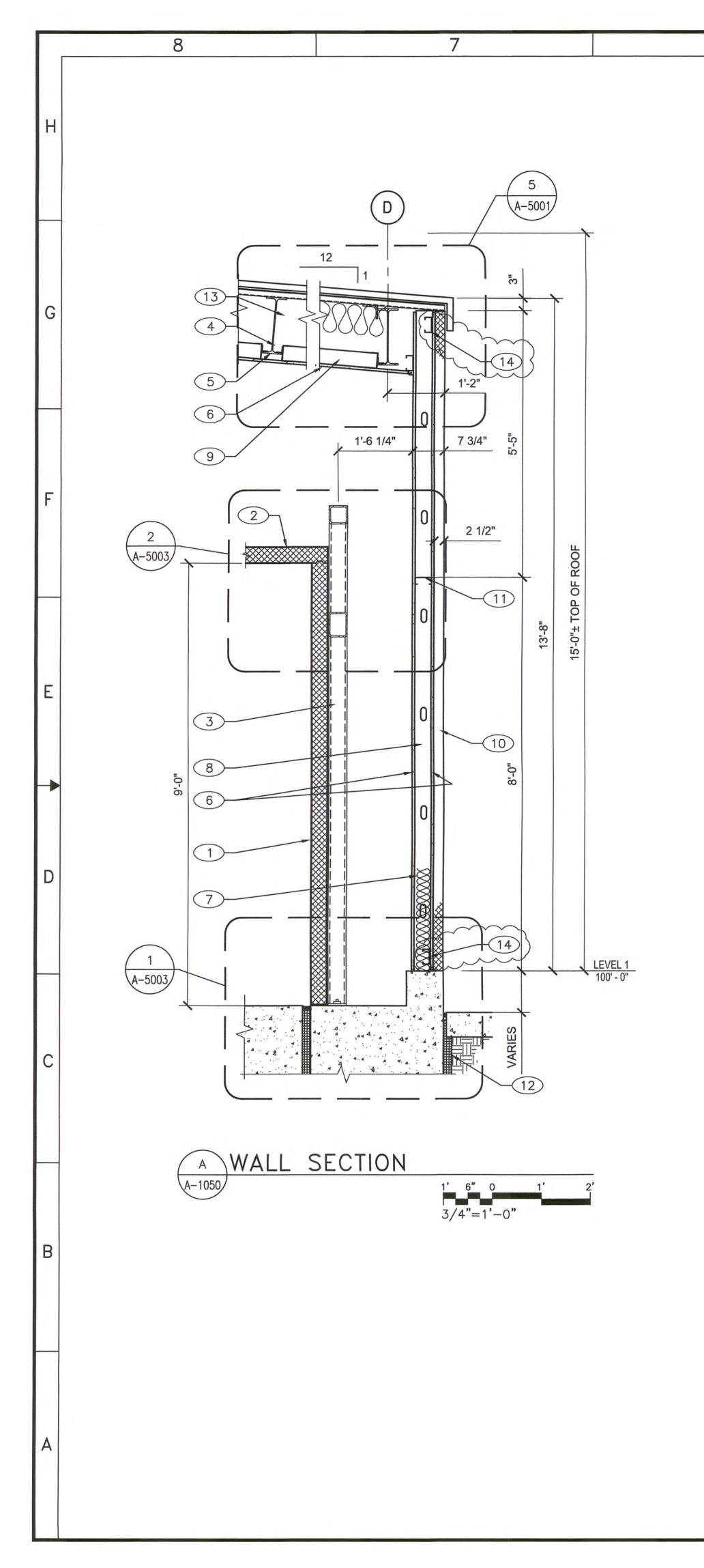
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SUBMITTED	APPROVED FOR REL	EASE			
BRIAN SULLIVAN	ED ARTIGLIA				
A			SHEET	A-'	1050
LOS Alamos NATIONAL LABORATORY		New Mexico 87545	285	OF	827
CLASSIFICATION U	REVIEWE	R ED ARTIGLIA	C	DATE 11-06-	13
PROJECT ID	DRAWING	NO			REV
102355		C55444			3



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	2		1
	GENERAL NOTES 1. IF THIS SHEET IS NOT 24" X GRAPHIC SCALE ACCORDIN 2. THIS DRAWING WAS GENER 3. STANDING SEAM METAL RO AND IS CLASSIFIED AS SAF	NGLY. RATED IN REVIT 2011. OOFTHIS_COMPONENT IS A (
		TAL AWNING, TYP SEE DETA NG SEAM METAL ROOF	IL 5/A-5002
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		FCR-102/DCN-260	AFi SE SW RE
	2 03-20-14 U EA L	DRN-14-63-0149-0045 JPDATED GENERAL NOTE #3 REVISED AWNINGS	AG MT RK BS MP
	NO DATE CLASS REV ADC	DESCRIPTION	DWN DSGN CHKD SUB APP
	WEIDLINGER-N	VAVARRO JV	NORTHERN NM
	TRU WASTE FA	ACILITY PROJECT	DRAWN A. GALLEGOS
	STORAG	E BUILDING	DESIGN D.WALLERSTEDT
	ROC	DF PLAN	CHECKED T. LEACH
	BLDG 63-0149 SUBMITTED	TA APPROVED FOR REL	A- 63 DATE 11-06-13
OFNEW	BRIAN SULLIVAN	ED ARTIGLIA	SHEET
STEPHEN G. VAN WINKLE	• Los Alamos	P0 Box 1663	A-1051 286 o⊧ 827
2273	CLASSIFICATION U	Los Alamos, New Mexico 87545 REVIEWER ED ARTIGLIA	DATE 11-06-13
SPED ARCT	PROJECT ID 102355	C55444	REV 3

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10	STEPHEN G. VAN WINKLE	
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	CRED ARC	

			TA-	63	DATE		11-06-13	
and and a second		APPROVED FO	RRELE	EASE				
		ED ARTIGLIA						
				SHEET	Г	A	-1051	
OS	Box 1663 Alamos, Ne	ew Mexico 875	545	2	86	OF	827	
	REVIEWER	ED ARTIGLIA			DA	TE 11-	06-13	
	DRAWING N	° C554	.44				REV 3	
			Contract Colors					

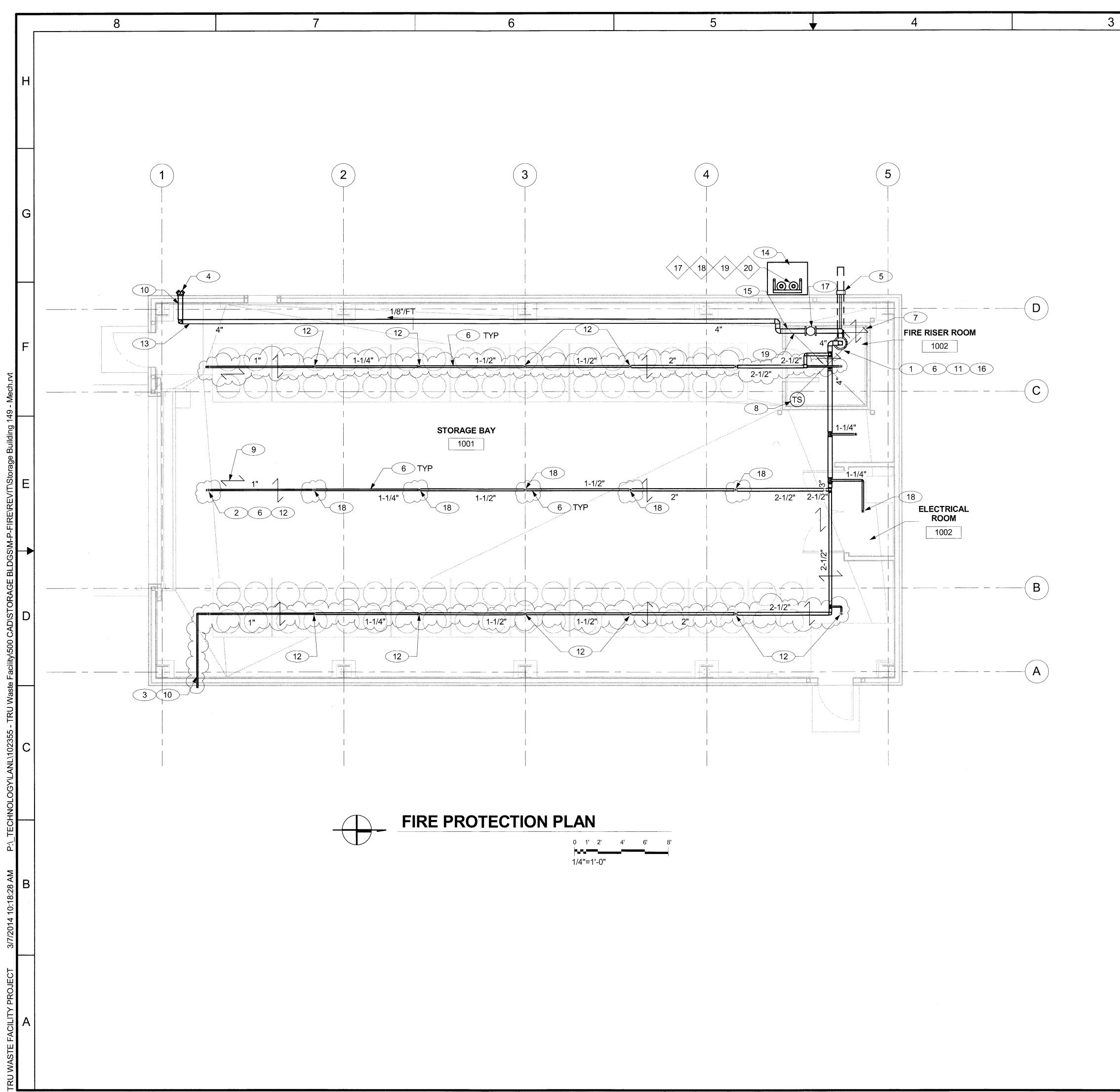


				Automotive
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	2	1
1. IF	ERAL NOTES THIS SHEET IS NOT 24X36, THEN CALE ACCORDINGLY	N IT IS A REDUCED SIZE PLOT. USE GRAPHI
KEYI	ED NOTES	
\bigcirc	4" THICK INSULATED METAL CL	AD INTERIOR WALL PANELS
2	4" THICK INSULATED METAL CL	AD INTERIOR CEILING PANELS
3	SEISMICALLY RATED STRUCTU	RAL FRAME
4	1 1/2" X 3 5/8" 20 GA TRACK	
5	1 1/2 X 1 1/2" CLIP	
6	5/8" TYPE "X" GYP BOARD	
7	BATT INSULATION - R13	
8	1 5/8" X 4" 16 GA METAL STUDS VERTICAL JOINT	@ 16" O.C. AND AT EACH METAL PANEL
9	3 5/8" 25 GA METAL STUDS @ 16	6" O.C.
10	2 1/2" X 36" INSULATED CORE M PER MANUFACTURER INSTRUC	IETAL WALL PANELS SECURE TO STRUCTUR
(11)	HORIZONTAL BLOCKING FOR M HEIGHT.	ETAL PANEL ATTACHMENT. LOCATE AT 108
12	2" PERIMETER INSULATION - R7	
(13)	W14 X 30 BEYOND	
(14)	METAL STUD BLOCKING FOR AT	TACHMENT OF KINGSPAN PANELS AS

4	01-15-16	U		FCR-	183/DCN-341		AG	Se	SW	RE	
3	05-14-14	U	EA	102355-DRN-C5 UPDATED			AG	мт	RK	BS	MP
2	01-06-14	U	EA	DRN 14.63.0144 UPDATED DETAIL	.0036 CALLOUTS		AG	RK	RK	BS	EA
1	11-06-13	U		NEW SHEET			AG	RK	RK	BS	
NO	DATE	CLASS REV	ADC	DESCR	RIPTION		DWN	DSGN	снкр	SUB	APF
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TRU WASTE FACILITY PROJECT DRAWN A. GALLEGOS											
STORAGE BUILDING DESIGN R. KASELOW						1					
			WAL	L SECTION			CHEC	CKED T	LEACH	H	
BLD	G 63-0149	9			TA	-63	DA	TE	11-	06-1	3
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• LOS AIAMOS NATIONAL LABORATORY PO Box 1663 Los Alamos, New Mexico 87545 291 OF 827						7					
	SIFICATION U			REVIEWER	ED ARTIGLIA			DATE	11-06	5-13	
PROJ	ECT ID			DRAWING						RE	V
102355 C55444					4	-					





GENE	RAL	NOT	ES

1. IF THIS SHEET IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.

1

- 2. THIS DRAWING WAS GENERATED IN REVIT 2011.
- 3. SEE SHEET F-0001 FOR SYMBOLS, LEGEND, ABBREVIATION AND STRUCTURAL BRACING INFORMATION.
- 4. FOR SEISMIC BRACING, SEE DETAILS 2 AND 3 ON SHEET F-5000.
- 5. SEE CALCULATION 11-001-FCAL-001 FOR HYDRAULIC CALCULATIONS.
- 6. THE SPRINKLER LAYOUT SHOWS DESIGN INTENT. THE FIRE PROTECTION SUBCONTRACTOR IS RESPONSIBLE TO PROVIDE SHOP DRAWINGS AND SUPPORTING CALCULATIONS.
- 7. PITCH PIPE TO DRAIN TO RISER PER NFPA 13.

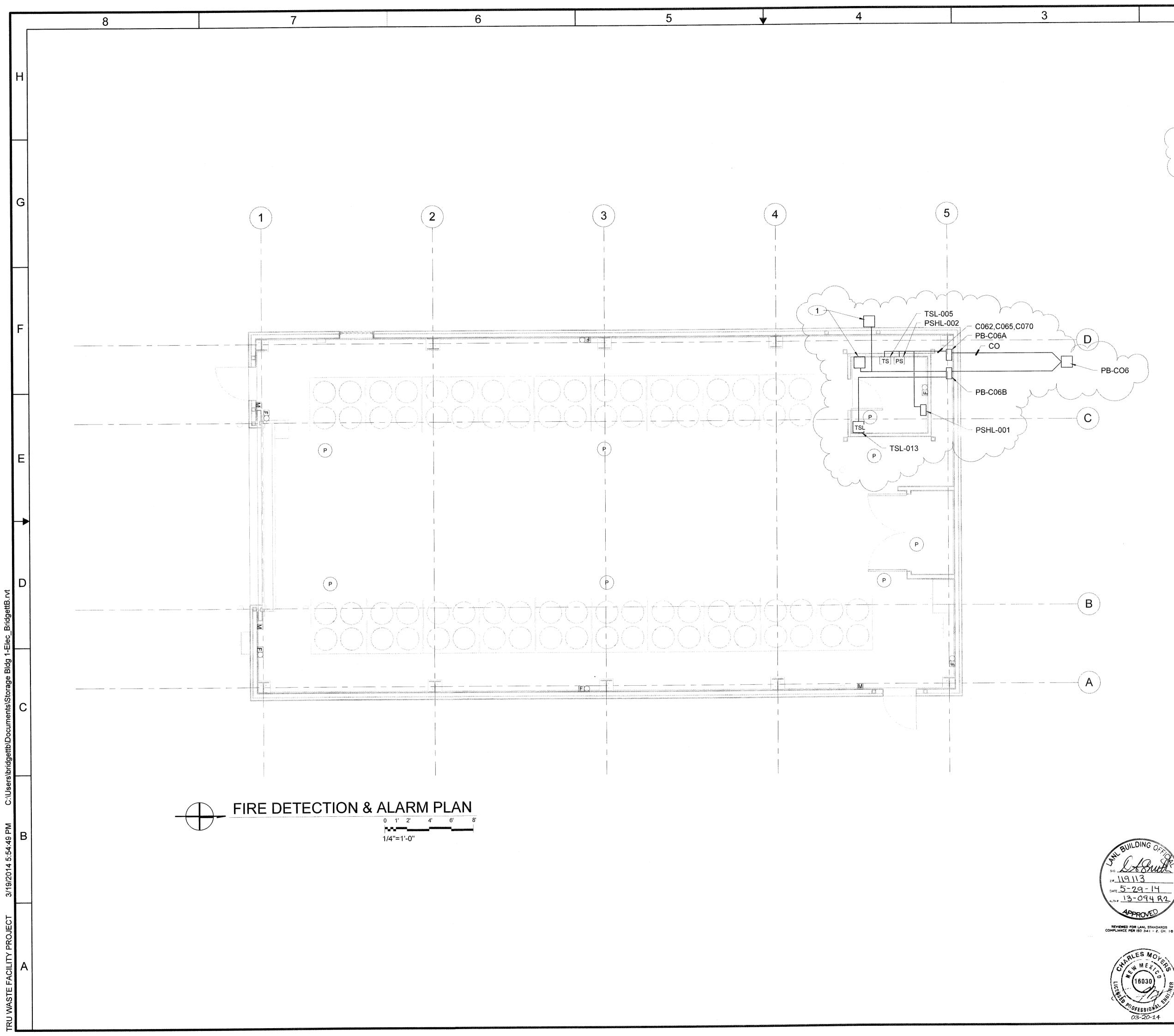
KEYED NOTES

- 1 6" FIRE PROTECTION RISER WITH DRY PIPE VALVE, SEE DETAIL 1 ON SHEET F-5000.
- 2 UPRIGHT SPRINKLER, TYPICAL OF 22.
- 3 INSPECTOR'S TEST STATION.
- 4 FIRE DEPARTMENT CONNECTION.
- 5 WALL POST INDICATOR VALVE, SEE PIPE THRU WALL PENETRATION DETAIL 5 ON SHEET F-5000.
- 6 FIRE PROTECTION COMPONENTS ARE CLASSIFIED AS SAFETY SIGNIFICANT ML-2.
- 7 SEE DETAIL 3 ON SHEET F-5000 FOR SWAY BRACING.
- 8 SAFETY SIGNIFICANT TEMPERATURE SENSOR.
- 9 SEE DETAIL 2 ON SHEET F-5000 FOR SWAY BRACING.
- (10) SEE DETAIL 5 ON SHEET F-5000 FOR PIPE THRU WALL PENETRATION.
- (11)SEE DETAIL 2 ON SHEET F-5001 FOR THERMAL BLOCK PENETRATION.
- 12 INSTALL HIGH TEMPERATURE RATED (286° F) SPRINKLER HEAD NEAR UNIT HEATER.
- 13 BOTTOM OF 4" PIPE AT 6'-10" AFF AT THIS LOCATION.
- 14 2 BOTTLE N2 RACK.
- 15 SEE DETAIL 3 ON SHEET F-5001 FOR ENCLOSURE WALL PENETRATION.
- 16 SEE DETAIL 1 ON SHEET F-5001 FOR ENCLOSURE CEILING PENETRATION.
- (17) CHECK VALVE WITH AUTOMATIC DRIP DRAIN.
- STANDARD 165° F HEAD. 18

REVIEWED FOR LANL STA COMPLIANCE PER ISD 341

(19) PROVIDE DRY SYSTEM AUXILIARY DRAIN. DRAIN SHALL CONSIST OF A VALVE NOT SMALLER THAN 1/2" AND A PLUG OR A NIPPLE AND CAP.

	2	03-07-14	U	hA	PRN-14-63 REVISED FIRE F	- <i>つ ; 49 - の 45</i> PROTECTION SYSTEM		B	m	C3	pe	in P
	1	11-06-13	U	-4	· · ·····	PROTECTION SYSTEM		DB	СМ	CM	BS	
	NO	DATE	CLASS REV	ADC	DESCRI	PTION	D	NWN	DSGN	CHKD	SUB	APP
	W	EIDLI	NGI	ER-	NAVARI		NOR	2TI	HE	RN	N	Μ
BUILDING OF		TRU	WAS	STE F	FACILITY P	ROJECT		DRA	WN D). BROE	RMAN	4
SIG_DASNUTT	STORAGE BUILDING DESIGN E. MIYODA											
2#_119113 DATE 5-29-14	FIRE PROTECTION PLAN							C. MOYE	ERS			
13-094 B2	BLDC	G 63-0149				TA-	63	DA	TE	11-	06-13	
	SUBM	TTED				APPROVED FOR RELI	EASE					
REVIEWED FOR LANL STANDARDS DMPLIANCE PER ISD 341 - 2, CH. 16	BRIAN	SULLIVAN				ED ARTIGLIA						
CHARLES MOL	1	A.					SHEET			F-1	00	0
(=	٩				PO Box 1663 Los Alamos, Ne	w Mexico 87545	29	99	OF	-	827	7
	CLASS	IFICATION U			REVIEWER	ED ARTIGLIA			DATE	11-06-1	3	
Phofessio MA	PROJE	CT ID			DRAWING N	0				T	RE	V
03-07-14		1023	355			C55444					2)

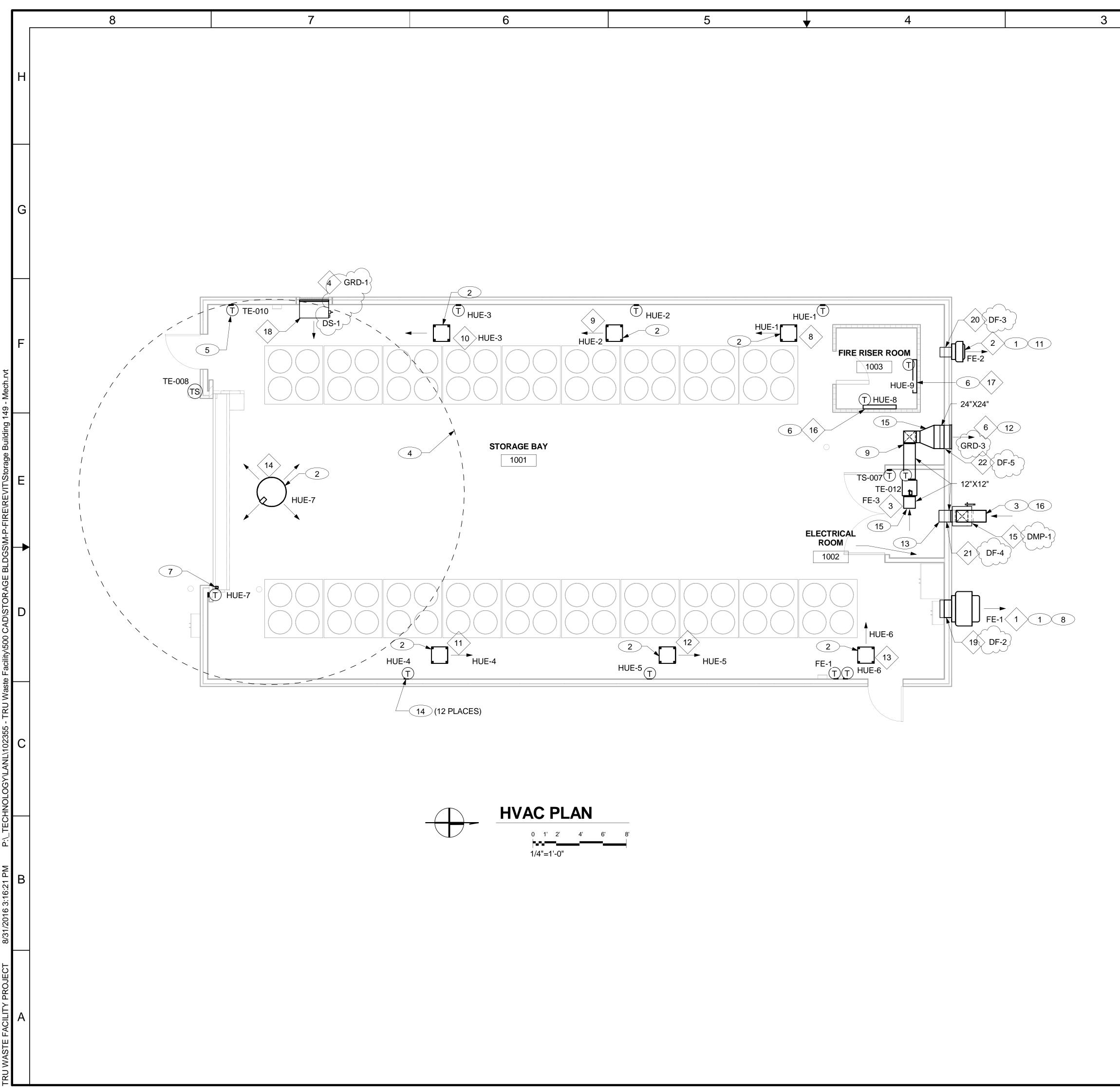


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GENERAL NOTES	
1 IF THIS SHEET IS NOT 24"x36", T SCALE ACCORDINGLY.	HEN IT IS A REDUCED SIZE PLOT. USE GRAPHI
2 THIS DRAWING WAS GENERATE	ED IN REVIT 2011.
	OTIFICATION APPLIANCES IN THIS BUILDING IB-FACP LOCATED IN BUILDING 63-152.
KEYED NOTES	
1 TSL-004, PS-002, AND PIV-002 V SIGNAL ROUTED TO SAP VIA P	WIRE TO SAP. INSTALL ONE TSP FOR EACH B-C06B.

DRN-14-63-0149-0045 olm. RECONFIGURE PANEL 03-20-14 U RELOCATED DEVICES FOR RISER CLOSET 11-06-13 RK CLASS REV ADC DWN DSGN CHKD SUB APP DESCRIPTION NO DATE WEIDLINGER-NAVARRO DRAWN B.BACKER TRU WASTE FACILITY PROJECT STORAGE BUILDING DESIGN R.KRAYER CHECKED C.MOYERS FIRE DETECTION & ALARM PLAN 11-06-13 DATE TA-63 BLDG 63-0149 APPROVED FOR RELEASE SUBMITTED ED ARTIGLIA BRIAN SULLIVAN SHEET F-1001 LES MO • LOS Alamos NATIONAL LABORATORY PO Box 1663 Los Alamos, New Mexico 87545 300 of 827 (16030) CLASSIFICATION U REVIEWER ED ARTIGLIA DATE 11-06-13 PROJECT ID DRAWING NO REV

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GENERAL NOTES:

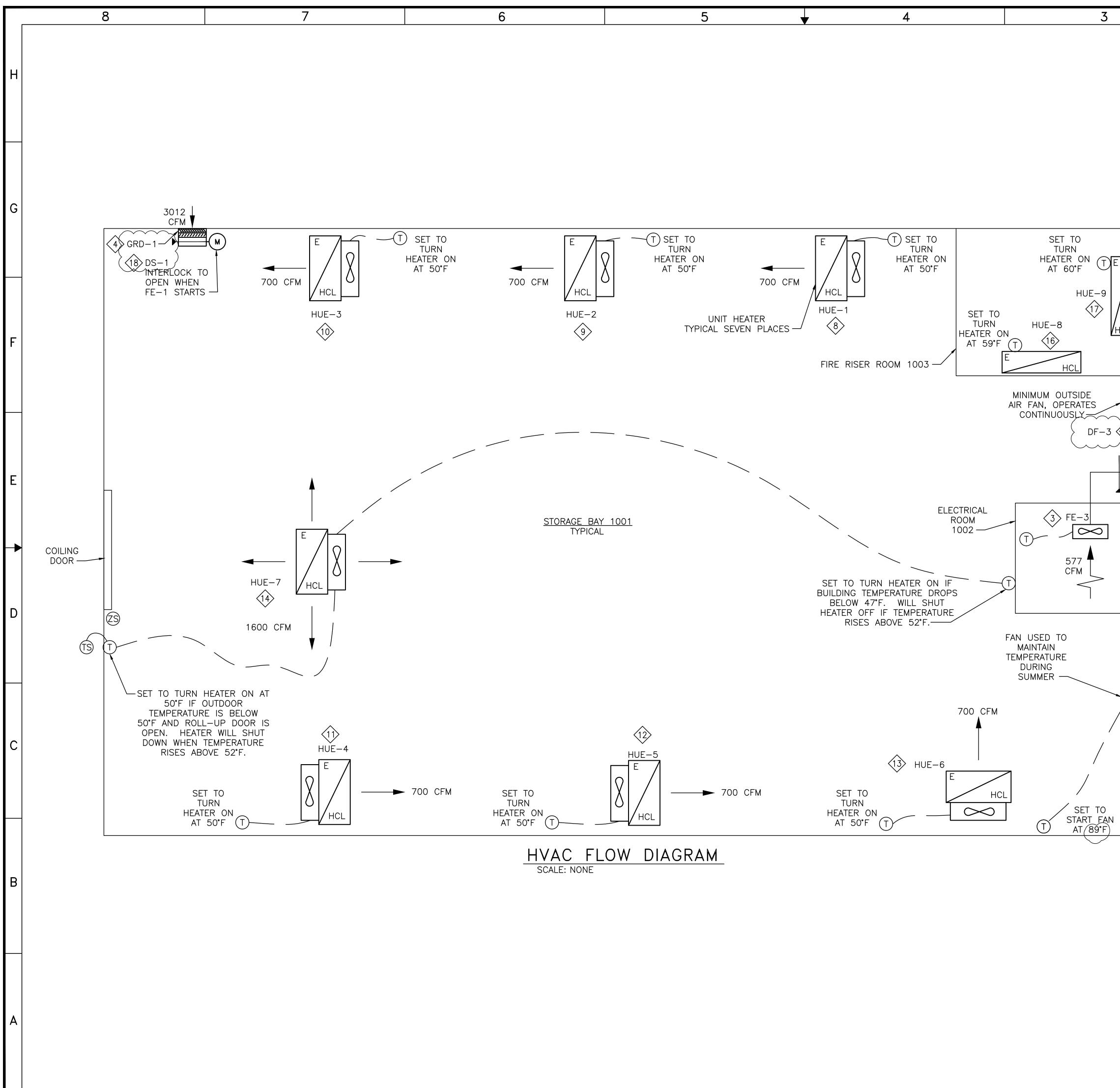
- 1. IF THIS SHEET IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.
- 2. THIS DRAWING WAS GENERATED IN REVIT 2011.
- 3. SEE SHEET M-0001 FOR ABBREVIATIONS, GENERAL NOTES AND LEGEND.
- 4. SEE SHEET M-6000 FOR AIR FLOW DIAGRAM.
- 5. SEE SHEETS M-7000 AND M-7001 FOR EQUIPMENT SCHEDULES.
- 6. SEE DETAIL 4 ON SHEET M-5000 FOR DUCT PENETRATION DETAIL, TYPICAL FOR ALL EXTERIOR WALL PENETRATIONS.

KEYED NOTES

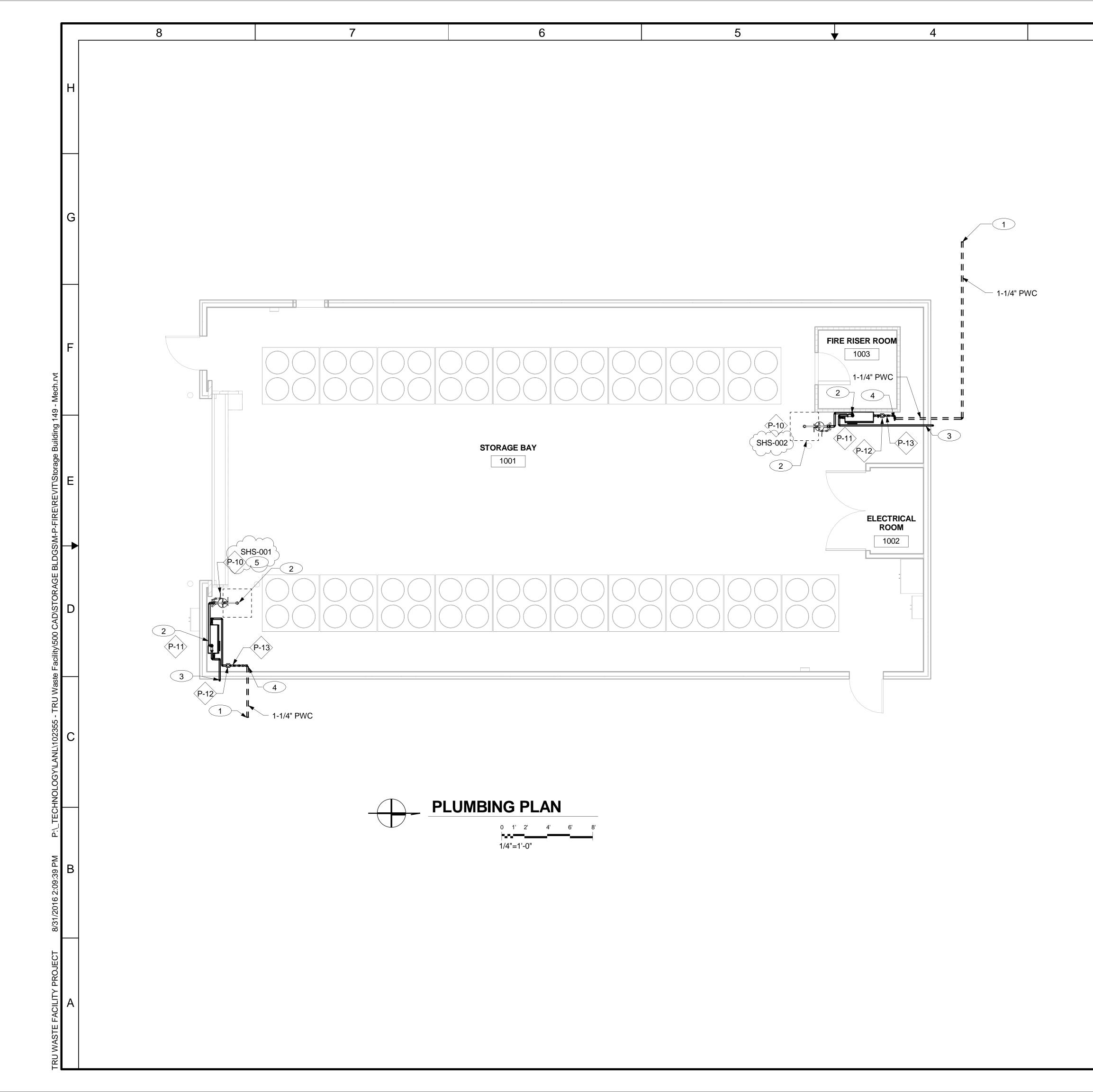
- 1 EXHAUST FAN WITH WEATHERHOOD, SEE DETAIL 1 ON SHEET M-5000.
- 2 MOUNT BOTTOM OF UNIT HEATERS HUE-1 THROUGH HUE-7 AT 10'-10" ABOVE FINISH FLOOR (TYPICAL OF 7).
- 3 SEE DETAIL 6 ON SHEET M-5000.
- 4 DASHED CIRCLE REPRESENTS AIR PATTERN LIMIT FROM HUE-7.
- 5 MOUNT TEMPERATURE SENSOR 12" FROM EDGE OF DOOR OPENING AT 48" ABOVE FINISHED FLOOR.
- 6 MOUNT BOTTOM OF HEATER 8'-6" AFF. MOUNT THERMOSTAT AT 4'-6" AFF.
- 7 DOOR CLOSURE SIGNAL SWITCH, ZS-001.
- 8 MOUNT FE-1 AT 9'-2" AFF TO BOTTOM OF DUCT.
- 9 SEE DETAIL 3 ON SHEET M-5000 FOR DUCT HANGERS.
- 10 MOUNT BOTTOM OF LOUVER AT 3'-6" AFF, SEE DETAIL 2 ON SHEET M-5000.
- (1) MOUNT FE-2 AT 11'-9" AFF TO BOTTOM OF DUCT, ABOVE TOP OF FIRE RISER ROOM 1003.
- 12 MOUNT BOTTOM OF LOUVER AT 9'-0" AFF.
- 13 MOUNT BOTTOM OF INTAKE AT 1'-10" AFF.
- 14 THERMOSTAT MOUNTED ON WALL AT 4'-6" AFF, TYPICAL.
- 15 12"x12" TO 24"x24" TRANSITION, SEE DETAIL 7 ON SHEET M-5000.
- 16 PROVIDE 1/2"x1/2" BIRD SCREEN, SEE DETAIL 4 ON SHEET M-5000.

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5	08-31-16	U		INCORPO	RATE AS-BUILTS		AB	PE	BCS	BE	
4	03-09-16	U		FCR-	357/DCN-496		DB	RB	JM	BS	
3	01-15-16	U	EA	FCR-226/DCN-379; FCR-267/DCN-409				RB	JM	BS	
2	05-14-14	U	EA	102355-DRN-C554	44-00001 REVISED NO	TE	DB	MT	СМ	BS	
1	11-06-13	U	EA	ADDED FIF	RE RISER ROOM		DB	СМ	СМ	BS	EA
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w	WEIDLINGER-NAVARRO										
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STORAGE BUILDING DESIGN P. MCMAH							HON				
			Н∨	AC PLAN			CHECKED		C. MOYERS		
BLDO	G 63-0149				TA-	- 63	DATE 11-06-13				
SUBM	ITTED				APPROVED FOR RELI	EASE					
BRIAN	SULLIVAN				ED ARTIGLIA						
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577 CFM OMP-1 OREN_WHEN FE-3 STARTS			
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	WEIDLINGER-NA	لـــــل	DRAWN D. BROERMAN
	TRU WASTE FAC STORAGE		DESIGN P. McMAHON
	HVAC FLOW BLDG 63-0149		-63 DATE 11-06-13
	SUBMITTED BRIAN SULLIVAN	APPROVED FOR RE ED ARTIGLIA	ELEASE
HICHAEL OFAR	• LOS Alamos NATIONAL LABORATORY	D Box 1663 os Alamos, New Mexico 87545	SHEET M—6000 318 ог 827
Barn Bruther	CLASSIFICATION U PROJECT ID	REVIEWER ED ARTIGLIA DRAWING NO	DATE 11-06-13 REV
55/0NAL EN 8/31/16	102355	C5544	



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GENERAL NOTES

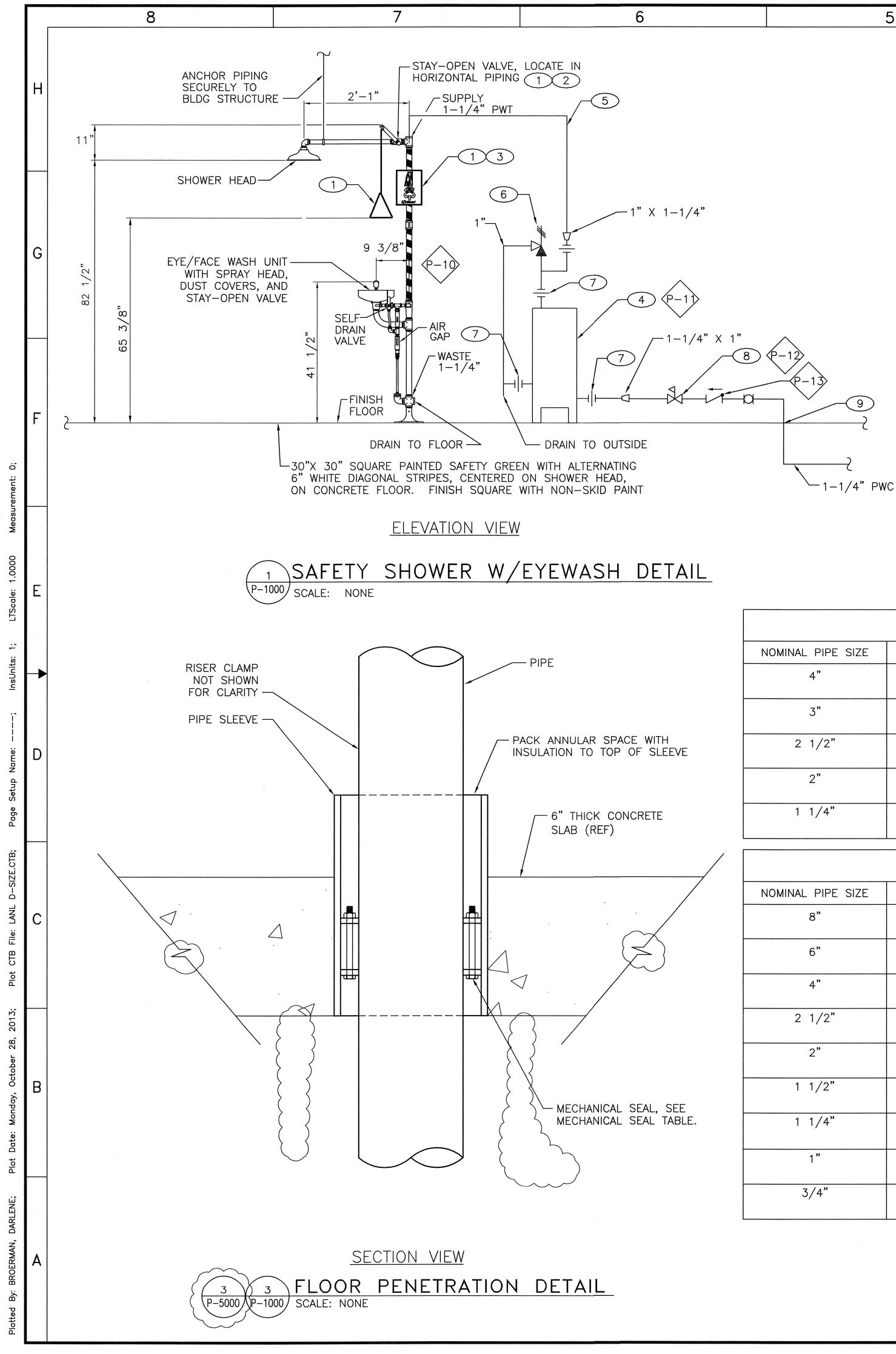
- 1. IF THIS SHEET IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.
- 2. THIS DRAWING WAS GENERATED IN REVIT 2011.
- 3. SEE SHEET P-0001 FOR SYMBOLS, GENERAL NOTES AND LEGEND.
- 4. SEE SHEET P-7000 FOR EQUIPMENT SCHEDULES.

KEYED NOTES

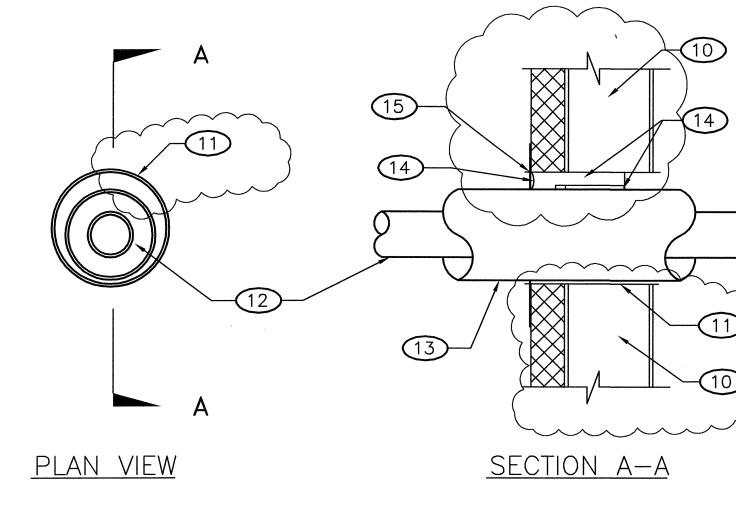
- 1 SEE SITE UTILITY PLAN, SHEET C55443-C-1006 FOR CONTINUATION.
- 2 SEE DETAIL 1 ON SHEET P-5000 FOR WATER HEATER, CONNECTIONS AND FLOOR PAINTING INSTRUCTIONS.
- 3 1" DRAIN FROM WATER HEATER RELIEF VALVE TO OUTSIDE. SEE DETAIL 2 ON SHEET P-5000 FOR WALL PENETRATION.
- 4 SEE DETAIL 3 ON SHEET P-5000 FOR FLOOR PENETRATION.
- 5 FIELD LOCATE EMERGENCY SHOWER TO ACCOMMODATE REQUIRED ELECTRICAL CLEARANCES.

3	08-31-16	U		B	KE	BCS	R				
2	01-15-16	U		FCR-226/DCN-37	9; FCR-267/DCN-409		DB	RB	BS	BS	
1	11-06-13	U	EA	REVISED LOCATION OF EYEWASH D		DB	CM	СМ	BS	EA	
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w	WEIDLINGER-NAVARRO										
	TRU WASTE FACILITY PROJECT								RMAN	N	
	STORAGE BUILDING						DESIGN		C. MOYERS		
	PLUMBING PLAN						CHECKED		E. MIYODA		
BLDC	G 63-0149				TA	- 63	DATE 11-06-13				
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BRIAN	SULLIVAN				ED ARTIGLIA						
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² PIPE THROUGH WALL PENETRATION P-1000 SCALE: NONE

		MECHAN	ICAL SEAL TABLE	
N	MECH NOMINAL PIPE SIZE 4" 6" 3" 5" 2 1/2" 4" 2" 4"	NOMINAL SLEEVE SIZE	METRASEAL MODEL NO.	REMARKS
	4"	6"	10MS-300ES	PIPE SCHEDULE 40 STEEL PIP SLEEVE SCHEDULE 40 STEEL P
	3"	5"	8MS-300ES	PIPE SCHEDULE 40 STEEL PIP SLEEVE SCHEDULE 40 STEEL P
	2 1/2"	4"	9MS-200ES	PIPE SCHEDULE 40 STEEL PIF SLEEVE SCHEDULE 40 STEEL F
	2"	4"	6MS-300ES	PIPE SCHEDULE 40 STEEL PIP SLEEVE SCHEDULE 40 STEEL P
	1 1/4"	3"	7MS-275ES	PIPE SCHEDULE 40 STEEL PIF SLEEVE SCHEDULE 40 STEEL F

	MECHAN	IICAL SEAL TABLE	
NOMINAL PIPE SIZE	NOMINAL SLEEVE SIZE	METRASEAL MODEL NO.	REMARKS
NUMINAL PIPE SIZE	NOMINAL SLEEVE SIZE	METRASEAL MODEL NO.	REMARKS
8"	10"	9MS-325ES	COPPER TUBE, SLEEVE SCHEDULE 40 STEEL PIPE
6"	8"	7MS-325ES	COPPER TUBE, SLEEVE SCHEDULE 40 STEEL PIPE
4"	6"	5MS-325ES	COPPER TUBE, SLEEVE SCHEDULE 40 STEEL PIPE
2 1/2"	4"	10MS-275ES	COPPER TUBE, SLEEVE SCHEDULE 40 STEEL PIPE
2"	3 1/2"	8MS-275ES	COPPER TUBE, SLEEVE SCHEDULE 40 STEEL PIPE
1 1/2"	3"	7MS-275ES	COPPER TUBE, SLEEVE SCHEDULE 40 STEEL PIPE
1 1/4"	3"	4MS-300ES	COPPER TUBE, SLEEVE SCHEDULE 40 STEEL PIPE
1"	2 1/2"	5MS-275ES	COPPER TUBE, SLEEVE SCHEDULE 40 STEEL PIPE
3/4"	2"	4MS-200ES	COPPER TUBE, SLEEVE SCHEDULE 40 STEEL PIPE

KEYED NOTES:

- 1) FURNISHED WITH EMERGENCY EQUIPMENT.
- 2 VALVE TO BE ACCESSIBLE FOR MAINTENANCE.
- $\overline{(3)}$ EMERGENCY SIGN(S).
- (4) ELECTRIC SAFETY SHOWER TEPID WATER HEATER.
- 5 TEPID WATER SUPPLY.
- 6 TEMPERATURE AND PRESSURE RELIEF VALVE.
- 7 PROVIDE DIELECTRIC UNION AT POINTS OF DISSIMILAR METALS.
- (8) PRESSURE REDUCING VALVE.
- 9 FLOOR PENETRATION, SEE DETAIL 3 ON SHEET P-5000.
- (10) 1 HOUR WALL ASSEMBLY STEEL STUDS.
- (11) STEEL SLEEVE CYLINDRICAL SLEEVE.
- (12) THROUGH PENETRANTS PIPE OR CONDUIT TO BE RIGIDLY SUPPORTED ON BOTH SIDES OF WALL ASSEMBLY. THE FOLLOWING TYPES OF METALLIC PIPES OR TUBES MAY BE USED:

STEEL PIPE - NOM. 2" (51 mm) (OR SMALLER) SCHEDULE 5 (OR HEAVIER) STEEL PIPE.

- (13) PIPE COVERING.
- (14) PACKING MATERIAL MIN. 3" (76 mm) THICKNESS OF MIN. 4 PCF (64 kg/m³) MINERAL WOOL BATT INSULATION FIRMLY PACKED INTO OPENING AS A PERMANENT FORM. PACKING MATERIAL TO BE RECESSED FROM FINISHED SURFACE OF WALL TO ACCOMMODATE THE REQUIRED THICKNESS OF FILL MATERIAL.

STUDS - THICKNESS, TYPE, NUMBER OF LAYERS AND FASTENERS AS REQUIRED IN THE INDIVIDUAL WALL AND PARTITION DESIGN. MAX SIZE OF OPENING IS 9.800"2 (63.2 cm²) WITH A MAX. DIMENSION OF 100" (254 cm).

(15) METAL RODENT SHIELD LOCATED ON EXTERIOR OF BUILDING.

	1	11-06-13	U	3A		REVISE) details		AB	m	m	p <u>R</u>	A
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		TRU W	/AST	E F	ACIL	_ITY	PROJEC	Т	DRA). BRC	DERM	AN
BUILDING OF										ign (C. MOI	'ERS	
5 19113				D	ETAIL	S			CHEC	KED F	P. McN	IAHOI	N
DATE 12-12-12 AUTH# 13-094	BLD	G 63-0149	9					TA-63	DA	TE	11-	06—1	13
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REVIEWED FOR LANL STANDARDS	BRIAN	I SULLIVAN					ED ARTIGLIA	SMA					
MPLIANCE PERIOD 341 - 2, CH. 16 ARLES MOLA ARLES ARLES ARL	1	A.						SHER		Ρ-	-50	00	0
16030	9							545 3	10	OF	- 8	327	7
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PROFESSIONAL	PROJ	IO DATE CLASS REV ADC DESCRIPTION IC NEIDLINGER-NAVARRO JV NOR TRU WASTE FACILITY PROJECT STORAGE BUILDING NOR DETAILS DETAILS LDG 63-0149 TA-63 JBMITTED APPROVED FOR RELEASE ED ARTIGLIA NAME PO Box 1663 Los Alamos, New Mexico 87545 ASSIFICATION U REVIEWER ED ARTIGLIA ROJECT ID DRAWING NO									RE	V	
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н			<u>GENERAL</u>	<u>. STRUCTURAL N</u>	<u>IOTES</u>
	FOR BUILDINGS AND OTHER C. ACI 318-05 BUILDING CODE RI AISC 360-05, MANUAL OF STEEL CONS E. DOE-STD-1020-2002 NATURAL CRITERIA FOR DOE FACILITIE F. ENGINEERING STANDARDS M	ENGINEERS, ASCE 7-05, MINIMUM DESIGN LOADS STRUCTURES. EQUIREMENTS FOR REINFORCED CONCRETE.D. TRUCTION. PHENOMENA HAZARDS DESIGN AND EVALUATION S. ANUAL ISD 341-2, CHAPTER 5, REV. 5, 11-19-2008	A. 28 DAY NORMAL WE B. REINFORCING: (1) REINFORCEM ASTM A706, G (2) STIRRUPS AN C. STD HOOKS, LAP SP TO REINFORCING SI D. SPECIAL INSPECTIO	D TIES: ASTM A615, GRADE 6 LICES, AND DEVELOPMENT LEN PLICE AND EMBEDMENT SCHED N FOR CONCRETE CONSTRUCT	E STRENGTH: 4000 PS ASTM A615, GRADE 6 O OR ASTM A706, GRA GTHS PER ACI 318-05 ULE ON S-7000.
G	10-27-2006. H. LANL DRAFTING MANUAL OST I. AISC 341-05 SEISMIC PROVISIO INCLUDING SUPPLEMENT NO	IANUAL ISD 341-2, CHAPTER 13, REV. 1, 7-220-03-01-DM REV. 4, 10-27-2006. DNS FOR STRUCTURAL STEEL BUILDINGS, .1. DF SAFETY INTO THE DESIGN PROCESS.		SHALL HAVE THE FOLLOWING (HERWISE ON THE DRAWINGS:	CONCRETE COVER,
	K. AWS D1.1 STRUDTURAL WELD 2. DESIGN LOADS A. NEW BUILDING CLASSIFICATI	ON PER DOE-STD-1020: PC-2 THE BUILDING IS		ONS (TOP AND BOTTOM BARS) -	
F	B. SEISMIC DESIGN CATEGORY C. MINIMUM DESIGN LOADS: IN ACCORDANCE WITH LANL LIVE LOADS, UNLESS NOTED (a) DEAD LOADS: (a1) SELFWEIGHT OI (a2) WEIGHT OF PEF		#14 BAF FORMED CONCRET EXPOSED TO #5 BARS W #6 THOU	EARTH, WATER AND WEATHER S AND SMALLER, 31 OR D31 WIRE AND SMALLER JGH #8BARS,	1 1/2"
	(b) LIVE LOADS: (b1) ROOF DESIGN L CONCENTRATED LOA (b2) SLAB-ON-GRAD 17,500 LB D. THE STRUCTURE HAS BEEN I	IVE LOAD: 30 PSF UNIFORM LOAD OR 2000 LB.	FORMED BEAMS AN DRY CONDITIO STIRUP PRINCIP EXPOSED TO STIRUP	ONS - S AND TIES PAL REINFORCEMENT EARTH, WATER AND WEATHER S AND TIES	2"
E	PARTIALLY COMPLETED STR CONTRACTOR AND SO INCLU FORMWORK, AND OTHER SU CONSTRUCTION OF THE STR THAT ALL CONSTRUCTION LO INDICATED ON THE STRUCTU NOT IMPOSED ON THE STRUC	JCTURE SHALL BE CONSIDERED BY THE DED IN THE DESIGN OF SHORING, BRACING, PPORTING ELEMENTS PROVIDED FOR UCTURE. THE CONTRACTOR SHALL ENSURE DADS DO NOT EXCEED THE DESIGN LIVE LOADS IRAL DRAWINGS AND THAT THESE LOADS ARE CTURAL MEMBERS PRIOR TO THE TIME THAT ALL EIR CONNECTIONS ARE IN PLACE.	WALLS: DRY CONDITIO #11 BAF #14 AND	RS AND SMALLER 0 #18 BARS EARTH, WATER AND WEATHER	2 1/2" 3/4" 1 1/2" - 2"
	E. WIND LOAD PARAMETERS: (1) BASIC WIND SPEED: 11 (2) EXPOSURE: C (3) WIND IMPORTANCE FA (4) INTERNAL BUILDING PF F. SEISMIC LOAD PARAMETERS: (1) PER LANL ESM REV 5, 7 (2) OCCUPANCY CATEGOF	7 MPH CTOR I=1.0 RESSURE COEFFICIENT: GCpi =±0.18 AND DOE-STD 1189, APPENDIX A RY IV	BEARIN AT UNFORME	URFACES AND BOTTOM G ON CONCRETE WORKMAT D SURFACES AND BOTTOMS FACT WITH EARTH INGS	2" 3" SAME AS SLABS 2"
D	Sds = 0.75 (6) IMPORTANCE FACTOR (7) SEISMIC FORCE RESIS ORDINARY STEEL MON (8) DESIGN BASE SHEAR \	OIL SPONSE ACCELERATION PARAMETERS: 11 = 0.64 I = 1.5 TING SYSTEM: MENT FRAME Y=CsW: Cs = 0.40, V = 35.10 KIPS	REQUIREMENTS OF PRACTICE PER SEC G. CAST-IN ANCHORS I SPECIFICATION SEC		I MANUAL OF STANDA ONCRETE SPECIFICA REQUIREMENTS OF
	(10) ANALYSIS PROCEDUR EQUIVALENT LATERAL G. SNOW LOAD PARAMETERS: (1) PER LANL ESM REV 5. (2) GROUND SNOW LOAD: (3) SNOW LOAD IMPORTAN (4) SNOW EXPOSURE FAC	FORCE Pg=29 PSF NCE FACTOR: I=1.2 TOR: Ce =1.0	A. STRUCTURAL STEEL B. MISCELLANEOUS ST C. HOLLOW STRUCTUF D. STANDARD STEEL P E. HIGH STRENGTH BO 5/8"Ø A "SC" (SLIP CRITIC	SPECIFICATION SECTION 05 100 W-SHAPES: ASTM A992, GRADE EEL SHAPES AND PLATES: ASTI AL SHAPES: ASTM A500 GRADE IPE: ASTM A53, GRADE B. LTS: 3/4"Ø AND 1"Ø ASTM A490 (STM A325 ("TURN OF THE NUT" CAL) FOR THIS PROJECT ONLY R	E 50. M A36. B. TENSION CONTROL) METHOD OR AS INDIC
С	(7) RAIN-ON-SNOW SURCH 3. GEOTECHNICAL INFORMATION: A. PER KLEINFELDER GEOTECH TECHNICAL AREA 63, KLEINFI MAY 18, 2011.	The second secon	I. ANCHOR RODS: AST J. DRILLED IN ANCHOR REQUIRED FOR PLA REPORT ESR-1917 I K. WELDS:	STM A29/A29M-04, GRADE A M F1554, GRADE 36. S: EXPANSION HILTI KB TZ, UNO CEMENT OF ALL HILTI KB TZ PO SSUED MAY 1, 2011.	ST INSTALLED ANCHO
	C. ALLOWABLE BEARING PRESS (1) FOUNDATIONS, FOUND 2500 PSF D. SUBGRADE MODULUS:	Y CLAY (CL), SILT WITH SAND (ML). URE FOR: ED ON TUFF/COMPACTED STRUCTURAL FILL: ED ON TUFF/COMPACTED STRUCTURAL FILL:	CHAPTER 13. (2) ELECTRODE: (3) 3/16" MINIMUM FILLE L. WELDED SHEAR STU M. NON-SHRINK GROU N. HEADED ANCHOR S	ALL BE IN ACCORDANCE WITH A USE 70,000 PSI ULTIMATE TENSI ET WELDS TO APPLY UNLESS OT JD CONNECTORS: ASTM A36 T - MINIMUM COMPRESSIVE STR TUD: ASTM A307 N FOR STEEL CONSTRUCTION F	LE STRENGTH MINIM THERWISE NOTED. ENGTH 7000 PSI.
в	PLAN TPLN-005". F. SOIL COEFFICIENT OF FRICTI 0.45 STRUCTURAL FILL G. "AT REST" LATERAL SOIL PRE		CRACKED AND UNC INSPECTION REQUI SPECIAL INSPECTIC Q. WELDS DESIGNATE METAL CAPABLE OF 20 FT-LB AT -20°F AS TEST METHOD OR M	TI-HIT-RE 500-SD FOR ADHESIVE RACKED CONCRETE ICC REPOR RED FOR ALL EPOXY APPLICATION	RT ESR-2322. SPECIAL ONS PER PROJECT "T . BE MADE WITH A FIL Y V-NOTCH TOUGHNE RIATE AWS CLASSIFIC
			A. STEEL ROOF DECK (GRADE 40. B. DECK TYPE, PROFIL	PECIFICATIONS SECTION 05 300 GALVANIZED) CONFORMING TO E, AND SECTION PROPERTIES A N FOR STEEL ROOF DECK PER I I TPLN-005".	ASTM A 653, S INDICATED ON PLA
A			7. GENERAL CONSTRUCTION A. EXECUTE ALL ACTIV		
			8. SPECIAL INSPECTION: A. REQUIREMENTS ARI PLAN TPLN-005".	E DESCRIBED IN THE PROJECT "	TESTS & SPECIAL INS

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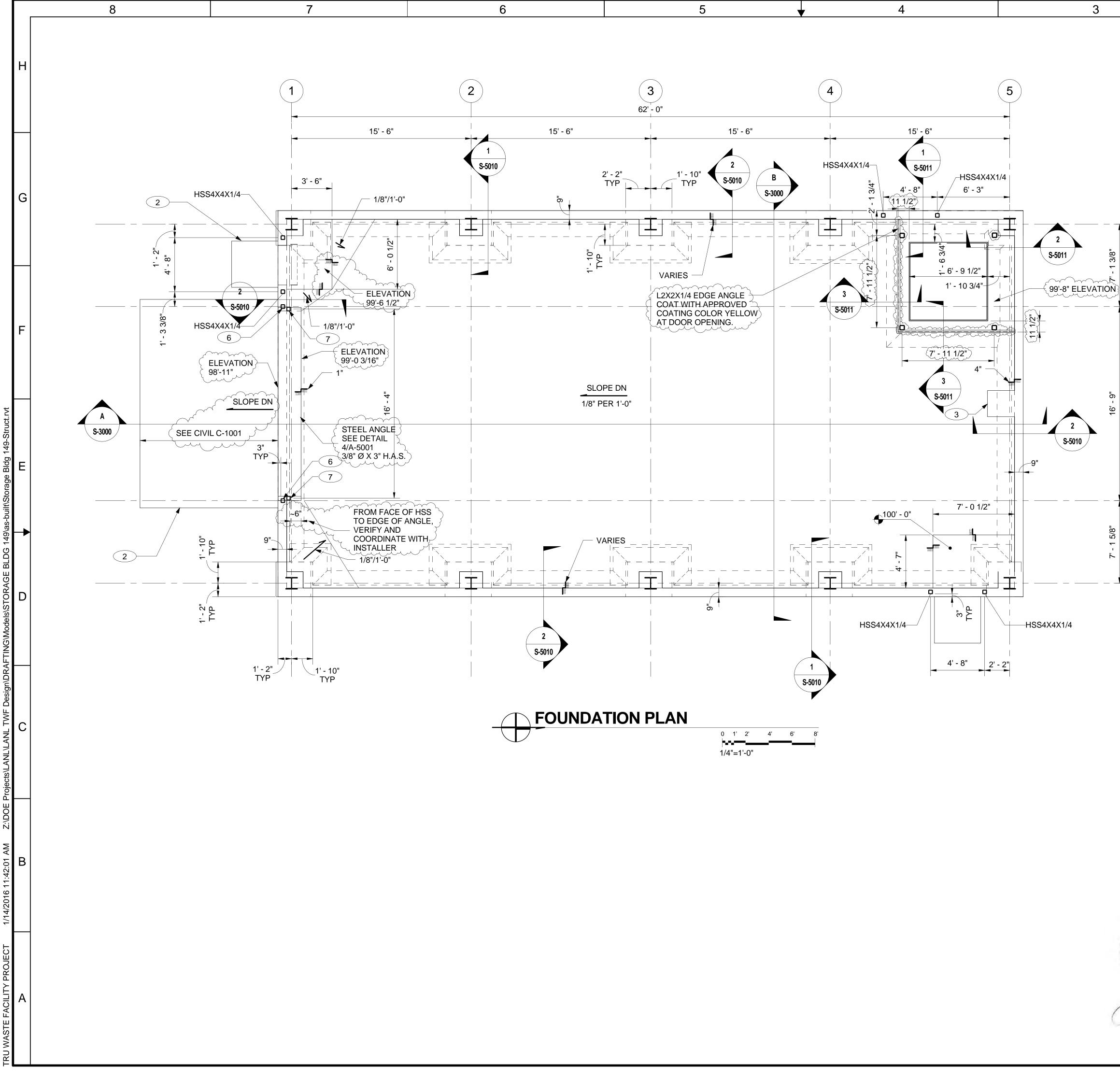
ANS. PECIAL

ISPECTIONS

9. LIGHT GAGE STEEL (SEE SPECIFICATION SECTION 05 4000, 01 4444 A. THE LIGHT GAGE STEEL DESIGN OF MEMBERS AND ALL CON

- THE REFERENCED CODES, LIVE LOADS AND WIND LOADS LIS LOADS" NOTES, AND DEAD LOADS AS IMPLIED FROM ARCHIT MECHANICAL DRAWINGS.
- B. ALL MEMBERS SHALL BE FORMED FROM CORROSION-RESIS MEETING ASTM A1003, STRUCTURAL STEEL GRADE 50, ZINC FORMED TO CHANNEL SHAPE. SEE SPECIFICATION SECTION COLD-FORMED METAL FRAMING.
- C. ALL OF THE COLD FORMED MEMBERS SHALL COME FROM A MANUFACTURER, "DIETRICH" OR EQUAL. THE INSTALLATION WITH THE MANUFACTURER'S RECOMMENDATIONS.
- D. BASE TRACKS SHALL BE SET ON SMOOTH AND LEVEL CONCI NON-SHRINK GROUT SUCH AS "MASTERFLOW 713" BY MASTE E. PRIOR TO FABRICATION OF FRAMING, THE CONTRACTOR SH
- FABRICATION AND ERECTION DRAWINGS TO THE ENGINEER SAID DRAWINGS SHALL BE SIGNED AND SEALED BY A STRUC REGISTERED IN THE STATE OF NEW MEXICO.
- F. ALL CONNECTIONS SHALL BE WELDED CONNECTIONS AND PERFORMED IN ACCORDANCE WITH THE LATEST EDITION OI SPECIFICATION FOR WELDING SHEET STEEL IN STRUCTURE SHALL BE PERFORMED BY AWS CERTIFIED WELDERS. ALL W CLEANED AND COATED WITH RUST INHIBITIVE ZINC PAINT.
- G. EXPANSION ANCHORS PROVIDE MINIMUM 1/2" DIAMETER K EXPANSION ANCHORS BY HILTI OR EQUAL (ICC ESR-1917 ISS WITH A MINIMUM 3 1/4" EMBEDMENT INTO CONCRETE. MINIM BETWEEN ADJACENT EXPANSION ANCHORS TO BE 5". EXPAN SHALL BE LOCATED A MINIMUM OF 3" FROM CONCRETE EDG WASHERS FOR ATTACHING COLD-FORMED MEMBERS WITH ANCHORS. INSTALL PER THE MANUFACTURER'S SPECIFICAT COLD-FORMED CONNECTIONS TO CONCRETE.
- H. SPLICES IN FRAMING COMPONENTS OTHER THAN TOP AND E ARE NOT PERMITTED.
- I. STUDS SHALL BE INSTALLED SO THE ENDS ARE POSITIONED. INSIDE OF THE RUNNER TRACK WEB PRIOR TO FASTENING WELDED TO BOTH FLANGES OF THE UPPER AND LOWER RUI J. FRAMING OF WALL OPENINGS SHALL INCLUDE HEADERS AND
- STUDS AS SHOWN IN DETAILS. K. ADDITIONAL STUDS SHALL BE INSTALLED IN THE WALLS TO F
- VERTICAL COMPONENTS OF BRACING LOADS. L. THE ALLOWABLE DEFLECTIONS (IN.) FOR VERTICAL WALLS S DIVIDED BY 400. THE ALLOWABLE VERTICAL DEFLECTIONS (
- HORIZONTAL FRAMING SHALL BE SPAN (IN.) DIVIDED BY 480 I AND SPAN (IN.) DIVIDED BY 360 FOR TOTAL LOADS. M. THE MINIMUM YIELD STRENGTH OF THE COLD-FORMED FRAI
- SHALL BE AS FOLLOWS: (a) 16 GAGE (54 MILS) OR HEAVIER - MINIMUM 50,000 PSI (b) ALL TRACKS & ACCESSORIES - MINIMUM 50,000 PSI UN
- OTHERWISE N. THE COLD-FORMED FRAMING SHALL BE DESIGNED IN ACCOR
- FOLLOWING CODES, STANDARDS AND SPECIFICATIONS: (1) IBC 2006
- (2) ANSI/ASCE 7-05
- (3) AISI "SPECIFICATIONS FOR DESIGN OF COLD-FORMED STRUCTURAL MEMBERS" - 1996
- (4) AISI "STANDARD FOR COLD-FORMED STEEL FRAMING: **GENERAL PROVISIONS"-2004**
- (5) AISI "STANDARD FOR COLD-FORMED STEEL FRAMING: WALL STUD DESIGN"-2004
- (6) AISI "STANDARD FOR COLD-FORMED STEEL FRAMING: HEADER DESIGN"-2004
- (7) AISI "STANDARD FOR COLD-FORMED STEEL FRAMING: LATERAL DESIGN"-2004
- (8) AISI "STANDARD FOR COLD-FORMED STEEL FRAMING:
- TRUSS DESIGN"-2004 (9) AISI "CODE OF STANDARD PRACTICE FOR STRUCTURA
- STEEL FRAMING"-2005 O. ALL MEMBERS SHALL BE CUT SQUARELY FOR ATTACHMENT
- PERPENDICULAR MEMBERS OR SLOPE CUT AS REQUIRED FOR AGAINST ABUTTING MEMBERS.
- P. FIELD CUTTING OF COLD-FORMED MEMBERS SHALL BE DONI SHEARING. TORCH CUTTING OF COLD-FORMED MEMBERS IS Q. ADDITIONAL TEMPORARY BRACING AND SHORING SHALL BE
- REQUIRED TO STABILIZE THE FRAMING AND TO SUPPORT CO LOADS. TEMPORARY BRACING SHALL REMAIN IN PLACE UNT BRACING IS INSTALLED AND/OR ADDITIONAL CONSTRUCTION REMOVED.
- R. THESE DRAWINGS ARE INTENDED TO INDICATE THE MEMBER SPACINGS REQUIRED. LIGHT GAGE STEEL SUBCONTRACTOR SUBSTITUTIONS PROVIDED THAT THE SUBSTITUTIONS CAN DESIGN LOADS AND ARE COORDINATED WITH THE PROJECT STRUCTURAL ENGINEER.
- S. SHEATHING ON THE COLD-FORMED FRAMING SHALL BE INST
- INDICATED IN THE ARCHITECTURAL DRAWINGS. T. ALL CONSTRUCTION SHALL BE IN ACCORDANCE WITH OSHA

& 01 4455) INECTIONS TO MEET STED IN "DESIGN FECTURAL AND						
TANT STEEL COATED (G90) N 05 4000 FOR						
SINGLE SHALL COMPLY						
RETE OR ER BUILDERS. IALL SUBMIT & FOR APPROVAL. CTURAL ENGINEER						
SHALL BE F THE AWS D1.3-98 S. ALL WELDING VELDS SHALL BE						
WIK BOLT TZ SUED MAY 1, 2011), IUM SPACING NSION ANCHORS GES. USE OVERSIZE EXPANSION FIONS FOR						
BOTTOM TRACKS						
AGAINST THE AND SHALL BE NNER TRACKS. D SUPPORTING						
RESIST THE						
GHALL BE HEIGH (IN.) IN.) FOR FOR LIVE LOADS						
MING COMPONENTS						
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AL COLD-FORMED						
TO OR AN ANGULAR FIT						
E BY SAWING OR S NOT PERMITTED. E PROVIDED AS ONSTRUCTION FIL PERMANENT N LOADS ARE						
R SIZES AND R MAY OFFER SUPPORT THE F ARCHITECT AND	3 01/15/16 2 01-06-14 1 11-06-13 NO DATE	UUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUU	FCR-028, FCR-158, DO "GENERAL STRUCTURAL "GENERAL STRUCTURAL DESCRIPTION	NOTES MODIFIED"	GF DMA CR	BS SUB APP
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	<u>GENERAL N</u>	IOTES
1.		ELEVATION 100'-0" = 7215.83'. SEE PLANS FOR JNDATION PLAN S-1000 AND CIVIL GRADING PLAN

FLOOR SLOPE = 1/8" PER 1'-0". 2.

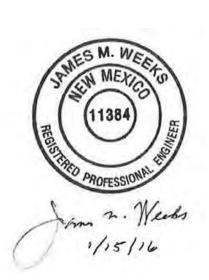
C-1005.

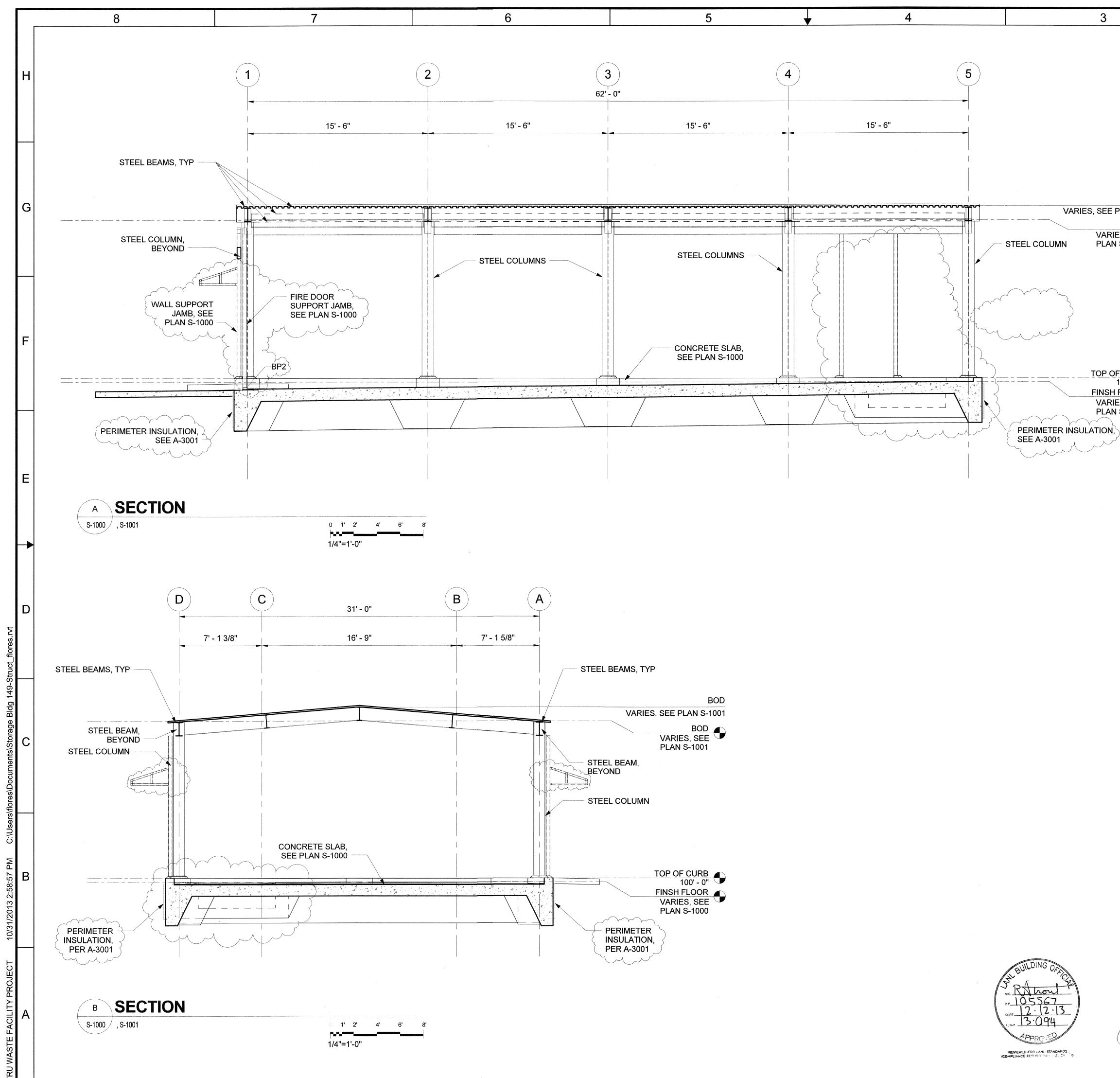
- SEE CIVIL PLANS FOR EXTERIOR SLAB AND PAVING. 3.
- SEE SOILS REPORT FOR UNDER SLAB AND FOOTING REQUIREMENTS. 4.
- IF THIS SHEET IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.
- THIS DRAWING WAS GENERATED IN REVIT 2014.
- CONCRETE SLAB, FOOTINGS, AND ALL REINFORCEMENT THEREIN ARE CLASSIFIED AS SAFETY SIGNIFICANT, ML-2.
- FOR SLAB STEPS, SEE 3/S-5010. 8.



- 1 8" CONCRETE MAT SLAB WITH #6@9"O.C. EACH WAY, SEE DETAIL 3/S-5000. SLAB IS PART OF THE LFRS. SAW CUTTING OF SLAB PROHIBITED.
- 2 CONCRETE STOOPS/RAMPS, SEE CIVIL SITE PLAN C-1001.
- 3 6" MIN HOUSEKEEPING PAD PER DETAIL 1/S-5001 AND SCHEDULE ON SHEET S-7000.
- 4 (HSS5X5)FOR FIRE RISER ROOM SUPPORT, SEE DETAIL 4/S-5025.
- FLOOR SLOPE IS CLASSIFIED AS SAFETY CLASS. MINIMUM FLOOR SLOPE 5 TOWARDS ROLL UP DOOR IS 1%.
- 6 HSS4X4X1/4 WALL SUPPORT JAMB.
- 7 HSS4X4X1/4 FIRE DOOR SUPPORT JAMB. VERIFY LOCATION WITH DOOR MANUFACTURER.

3 2 1	01/15/16 01-06-14 11-06-13	4 U "DETAIL CUT ADDED" 3 U "ADDITION OF AWNING SUPPORT FRAMING" CLASS ADC DESCRIPTION							DA.K. CZ CR	DL DL BS	-
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	<u>GENERAL N</u>	NOTES

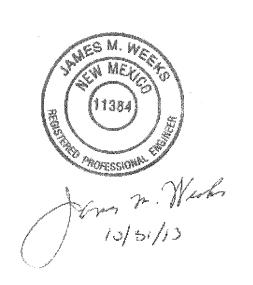
- BASE PLATE SCHEDULE IS LOCATED IN DETAIL 1/S-5000. 1.
- FINISH FLOOR REFERENCE ELEVATION 100'-0" = 7215.83'. SEE PLANS FOR MAT SLAB ELEVATIONS, FOUNDATION PLAN S-1000 AND CIVIL GRADING PLAN 2. C-1005.
- IF THIS SHEET IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE 3. GRAPHIC SCALE ACCORDINGLY.
- THIS DRAWING WAS GENERATED IN REVIT 2011. 4.

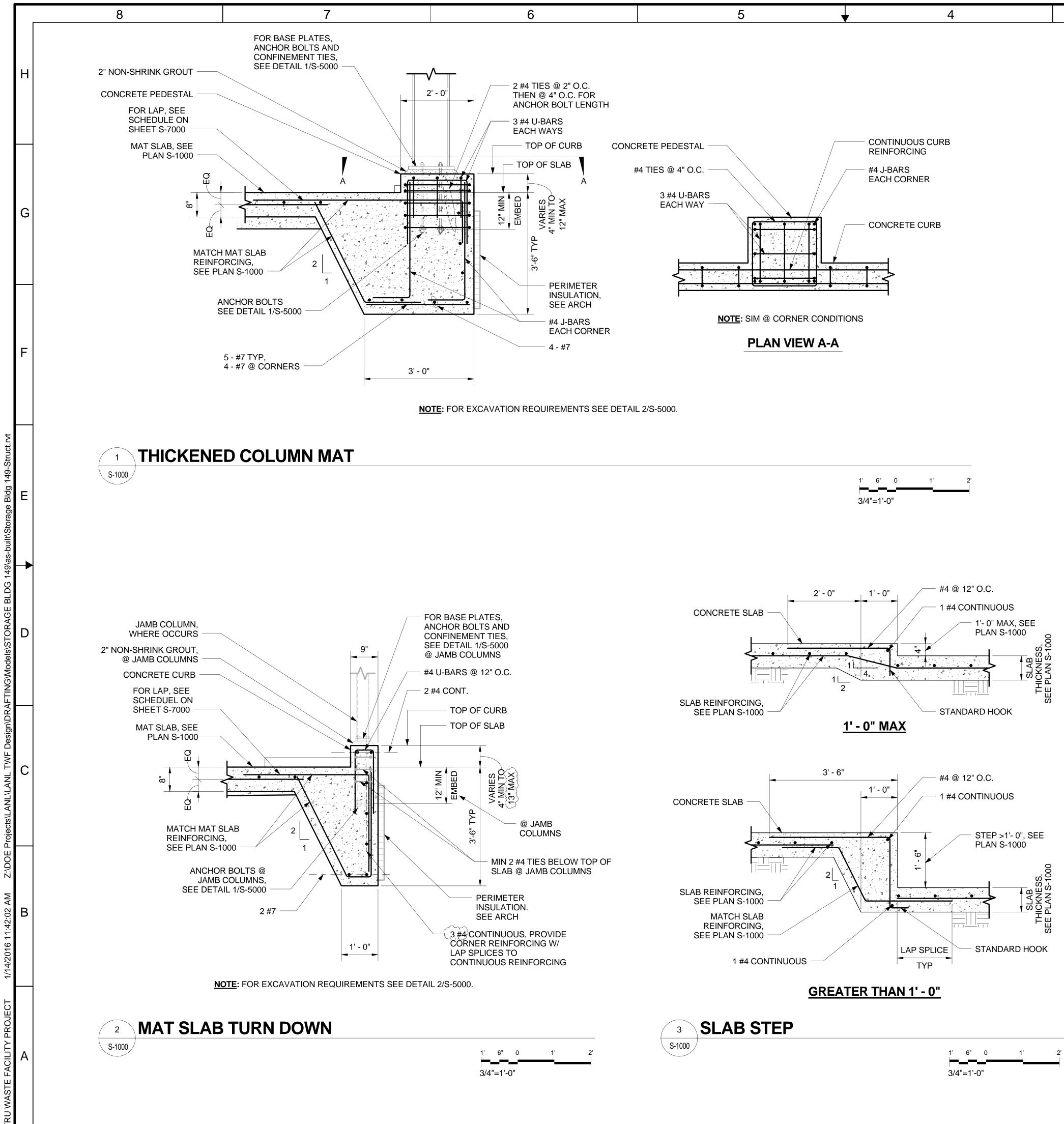
BOD VARIES, SEE PLAN S-1001 BOD VARIES, SEE

PLAN S-1001

TOP OF CURB 100' - 0" FINSH FLOOR VARIES, SEE **PLAN S-1000**

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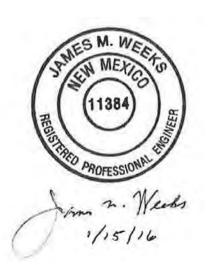


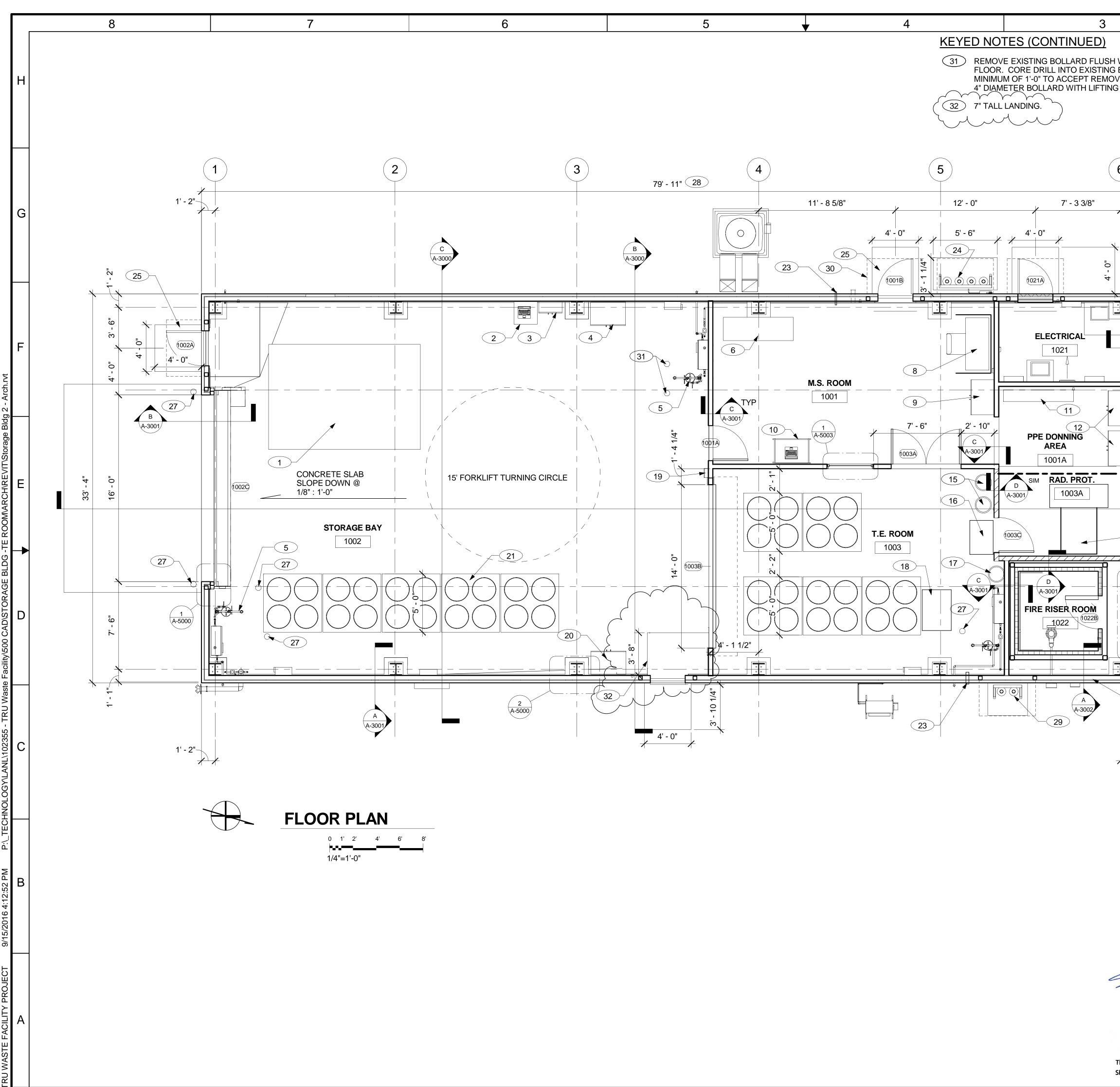


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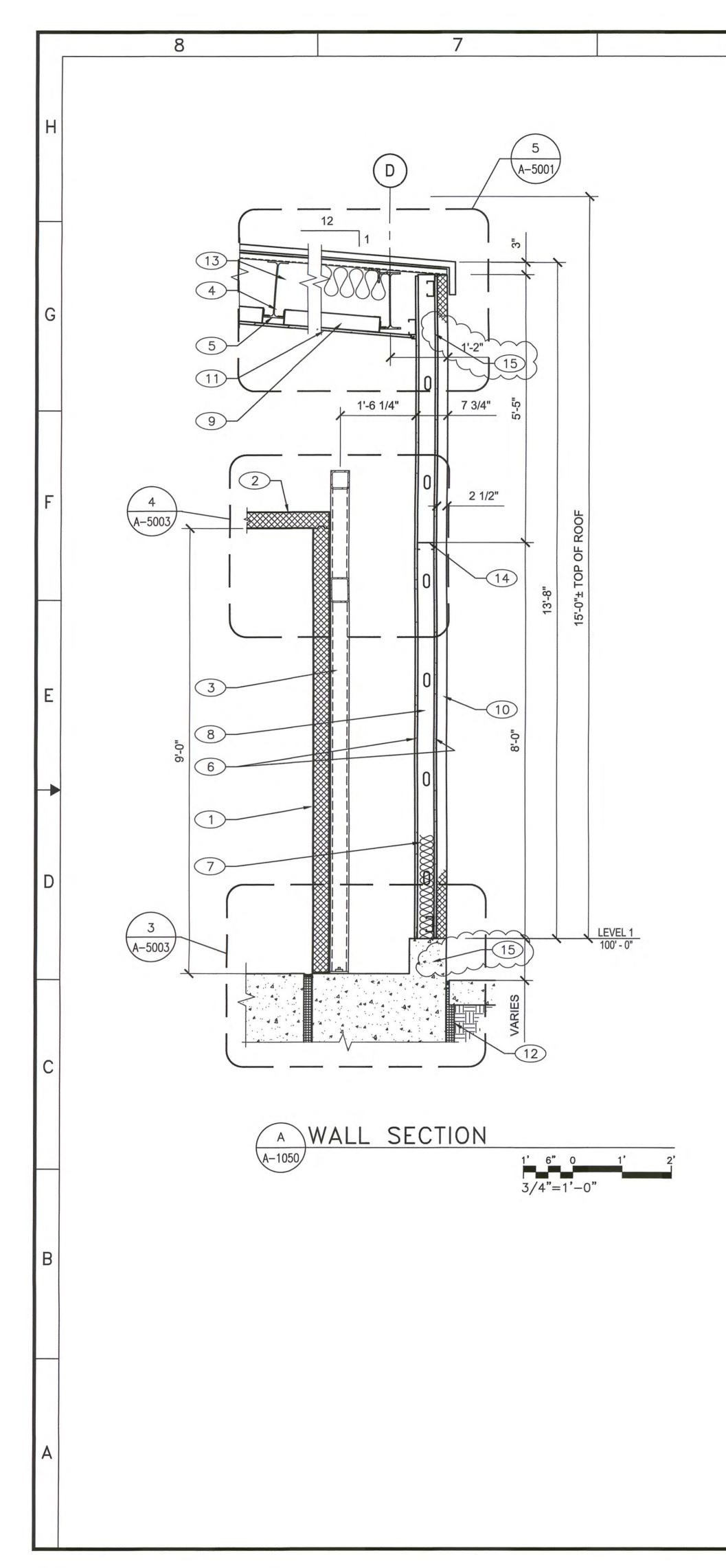
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	<u>GENERAL N</u>	<u>NOTES</u>
1.		ND ARE LOCATED ON SHEET S-0001 AND TES ARE LOCATED ON SHEET S-0002.
2.	IF THIS SHEET IS NOT 24"x36 GRAPHIC SCALE ACCORDING	5", THEN IT IS A REDUCED SIZE PLOT. USE GLY.
3.	THIS DRAWING WAS GENER	ATED IN REVIT 2014.

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NG EYE.													
	3.					HANICAL ROOMS, AD C 3/16" THICK x 2" x 6							
						IELVETICA BOLD LAE ABOVE THE FLOOR (
		OF THE DC											
	4.					STAINLESS STEEL O	ORNE	ER GU	ARD	S AT			
6		OUTSIDE C	ORNER	RS, TYP	ICAL.								
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58)		5 LAUNI	ORY BIN	I (NIC)									
		6 STEP-	OFF PA	D, GFE									
33' - 4		7 WAST	E BIN (N	IIC)									
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13						PMENT CABINET (NIC	;)						
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		22) NOT L											
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			-			OCATION, SEE DETA	II 3/D_	5000					
						CAL - SEE SHEET C55							
						0 FEET EITHER SIDE							
A-5000 - A						DR VALVE		ALL					
		PERM	ANENT	BOLLA	RD, SE	EE DETAIL 7/A-5002							
						RE SAFETY CLASS, M			JM				
26		_				XIMUM WIDTH IS 33.8							
		29) FIRE S	SUPRES	SION S	SYSTE	M GAS BOTTLE RACH	<						
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+	6 5	09-15-16 06-01-16	UU		L	419/DCN-553 329/DCN-470 R1			AG	SVV. SC	svw	MT BS	
	4	02-23-16	U	EA		329/DCN-470			AG	SC	SVW	BS	
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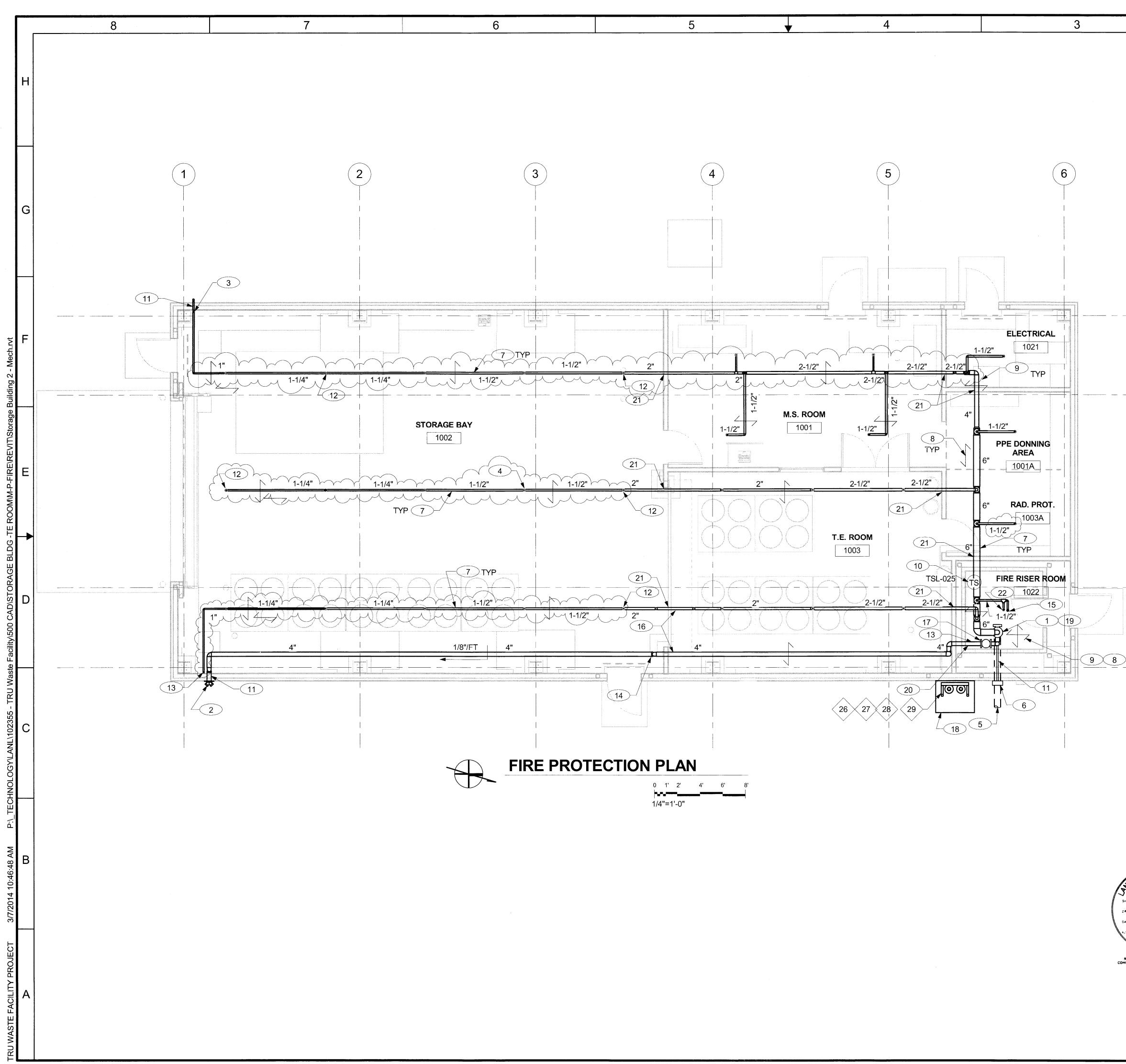


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I K	SCALE ACCOF	T IS NOT 24X36, THE	N IT IS A REDUCED SIZE PLOT. USE GR	APHIC
I K	IF THIS SHEET SCALE ACCOF	T IS NOT 24X36, THE	N IT IS A REDUCED SIZE PLOT. USE GR	APHI
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	1 4" THICK IN	2.5		
		SULATED METAL CL	AD INTERIOR WALL PANELS	
\subset	2 4" THICK IN	SULATED METAL CL	AD INTERIOR CEILING PANELS	
	3 SEISMICAL	LY RATED STRUCTU	JRAL FRAME	
\langle	4 1 1/2" X 3 5/	8" 20 GA TRACK		
\langle	5) 1 1/2 X 1 1/2	" CLIP		
\langle	6 5/8" TYPE "2	x" gyp board - 1 la	AYER ON EACH SIDE OF METAL STUD W	ALL
\langle	7 BATT INSUL	ATION - R13		
\langle	3 1 5/8" X 4" 1 VERTICAL		@ 16" O.C. AND AT EACH METAL PANEL	-
\langle	9 3 5/8" 25 GA	METAL STUDS @ 1	6" O.C.	
(1		INSULATED CORE M FACTURER INSTRUC	METAL WALL PANELS SECURE TO STRU CTIONS.	CTUR
C	1) 5/8" TYPE "	K" GYP BOARD		
(1	2 2" PERIMET	ER INSULATION - R7	7	
(1	3 W14 X 30 B	EYOND		
	4 HORIZONTA HEIGHT	AL BLOCKING FOR M	IETAL PANEL ATTACHMENT. LOCATE A	T 108
		D BLOCKING FOR A TOP AND BOTTOM	TTACHMENT OF KINGSPAN PANELS AS OF WALL	

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2	01-06-14	U	EA	DRN 14.63.0144 UPDATED DETAIL	.0041 CALLOUTS		AG	RK	RK	BS	EA
1	11-06-13	U		REVISED SECTION	IS & NOTES		AG	RK	RK	BS	
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GENERAL NOTES:

2

- 1. IF THIS SHEET IS NOT 24"x36", IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.
- 2. THIS DRAWING WAS GENERATED IN REVIT 2011.
- 3. SEE SHEETS F-0001 AND F-0002 FOR ABBREVIATIONS, GENERAL NOTES, LEGEND AND STRUCTURAL BRACING.
- 4. FOR SEISMIC BRACING SEE DETAILS 2 AND 3 ON SHEET F-5000.
- 5. SEE CALCULATION 11-001-FCAL-001 FOR HYDRAULIC CALCULATIONS.
- 6. SEE DETAIL 3 ON SHEET F-5001 FOR FLOOR PENETRATION DETAIL.
- 7. THE SPRINKLER LAYOUT SHOWS DESIGN INTENT. THE FIRE PROTECTION SUBCONTRACTOR IS RESPONSIBLE TO PROVIDE SHOP DRAWINGS AND SUPPORTING CALCULATIONS.
- 8. PITCH PIPE TO DRAIN TO RISER PER NFPA 13, UNLESS NOTED OTHERWISE.

KEYED NOTES:

(D)

-(C)

-(B)

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PPROVE

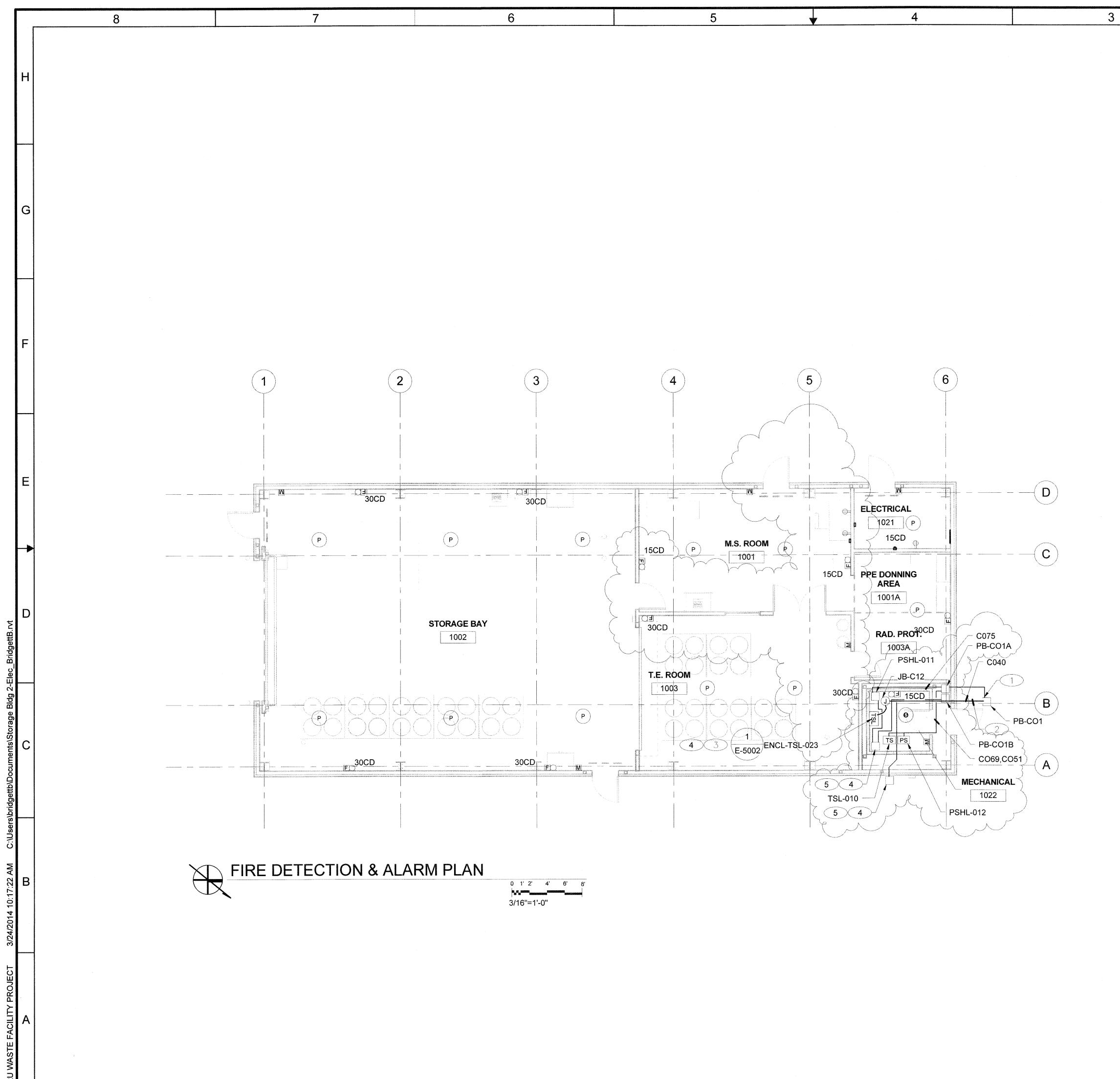
REVIEWED FOR LANL STANDARDS COMPLIANCE PER ISD 341 - 2. CH. 16

03-07-14

2# 119113 DATE 5-29-14 13-094 R2

- 1 6" FIRE PROTECTION RISER WITH DRY PIPE VALVE, SEE DETAIL 1 ON SHEET F 5000.
- 2 FIRE DEPARTMENT CONNECTION.
- 3 INSPECTOR'S TEST STATION, SEE WALL PENETRATION DETAIL 5 ON SHEET F-5000.
- (4) UPRIGHT SPRINKLER HEAD (165° F), TYPICAL, UNLESS NOTED OTHERWISE.
- 5 SEE SHEET C-1007 FOR CONTINUATION.
- 6 WALL MOUNTED POST INDICATOR VALVE, SEE WALL PENTRATION DETAIL 5 ON SHEET F-5000.
- 7 FIRE PROTECTION COMPONENTS ARE CLASSIFIED AS SAFETY SIGNIFICANT, ML-2.
- 8 SEE DETAIL 2 ON SHEET F-5000.
- (9) SEE DETAIL 3 ON SHEET F-5000.
- (10) SAFETY SIGNIFICANT TEMPERATURE SENSOR.
- 11 SEE DETAIL 5 ON SHEET F-5000 FOR PIPE PENETRATION.
- 12 INSTALL HIGH TEMPERATURE RATED (286° F) SPRINKLER HEAD NEAR UNIT HEATER.
- 13 PROVIDE DRY SYSTEM AUXILIARY DRAIN. DRAIN SHALL CONSIST OF A VALVE NOT SMALLER THAN 1/2" AND A PLUG OR A NIPPLE AND CAP.
- 14 PIPE AT 10'-6" AFF AT THIS LOCATION.
- 15 PENDANT SPRINKLER (165° F).
- 16 ROUTE PIPE OVER DOOR AND FRAMING.
- 17 4" CHECK VALVE.
- (18) 2 BOTTLE N2 RACK, SEE DETAIL 7 ON F-5000.
- (19) SEE DETAIL 1 ON SHEET F-5001 FOR ENCLOSURE CEILING PENETRATION.
- 20 SEE DETAIL 3 ON SHEET F-5001 FOR ENCLOSURE WALL PENETRATION.
- 21 SIMILAR TO DETAIL 5 ON SHEET F-5000, PIPE PENETRATION DETAIL.
- (22) UPRIGHT SPRINKLER HEAD LOCATED ABOVE FIRE RISER ROOM.

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GENERAL NOTES

2

1 IF THIS SHEET IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.

1

- 2 THIS DRAWING WAS GENERATED IN REVIT 2011.
- 3 ALL INITIATING DEVICES AND NOTIFICATION APPLIANCES IN THIS BUILDING SHALL BE SUPPORTED BY THE SUB-FACP LOCATED IN BUILDING 63-0152.
- 4 COORDINATE ENCLOSURE LOCATION FOR FIRE SYSTEM INSTRUMENTS WITH RTU TEMPERATURE MONITORING SYSTEM. SEE DRAWING C55443 SHEET E-4005.

KEYED NOTES

- 1 SEE DRAWING C55443 E-1012 FOR LOCATION OF PULL BOX.
- 2 TRANSITION ABOVE GROUND CONDUIT INSIDE BUILDING FROM 3/4" EMT TO 1-1/2" SCHEDULE 80 PVC UNDERGROUND CONDUIT BY WAY OF RMC 90 DEGREE SWEEP.
- ENCLOSURE DETAILS ARE SHOWN ON DRAWING C55445 SHEET E-5002.X (3)

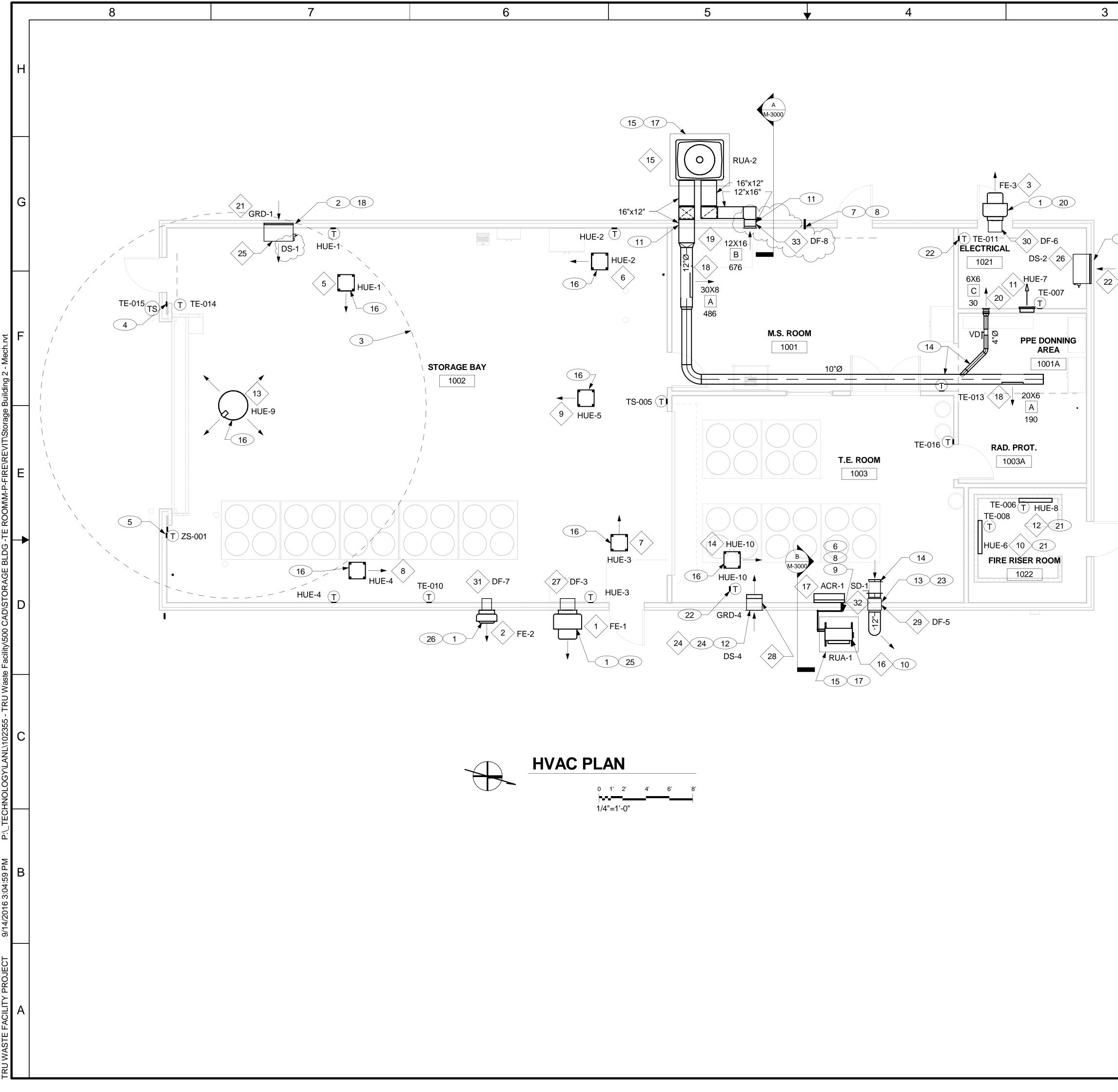
4 TSL-023. TS, PS-007, AND PIV-007 WIRE TO SAP. INSTALL ONE TSP FOR EACH SIGNAL ROUTED THROUGH PD-CO1B

5 WIRE IN 3/4" CONDUIT

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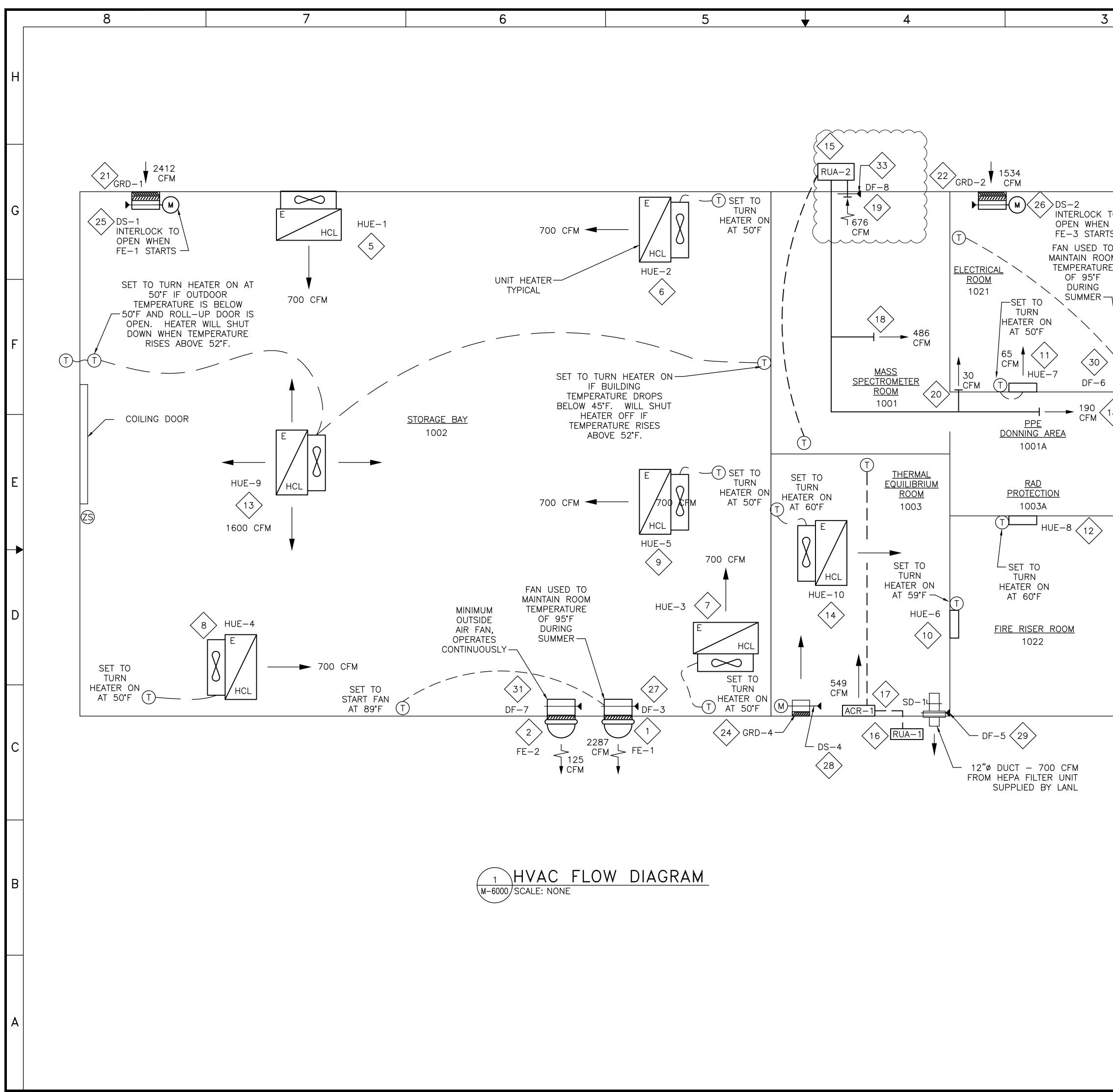






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	GENERAL NOTES:		
	1. IF THIS SHEET IS NOT 24"x36", GRAPHIC SCALE ACCORDINGL		PLOT. USE
	2. THIS DRAWING WAS GENERAT	ED IN REVIT 2011.	
	3. SEE SHEET M-0001 FOR ABBRE	EVIATIONS, GENERAL NOTES	SAND LEGEND.
	4. SEE SHEET M-6000 FOR HVAC	FLOW DIAGRAM.	
	5. SEE SHEETS M-7000 AND M-700	01 FOR MECHANICAL EQUIP	VENT SCHEDULES.
	KEYED NOTES:		
	1 SEE DETAIL 1, SHEET M-5000.		
	2 SEE DETAIL 2 ON SHEET M-50	000.	
2 19	3 DASHED CIRCLE INDICATES A	AIR PATTERN LIMIT FOR HUE	-9.
	4 MOUNT TEMPERATURE SENS 48" ABOVE FINISHED FLOOR.	SOR 12" FROM EDGE OF DOC	R OPENING AT
GRD-2	5 DOOR CLOSURE SIGNAL SWI	TCH ZS-001.	
	6 1/2" SUCTION, 1/4" LIQUID, 1/2	" CONDENSATE DRAIN.	
	7 1" STAINLESS STEEL EXHAUS LOCATED AT 8'-0" AFF.	T PIPE FOR MASS SPECTRO	METER,
	8 SEE DETAIL 1 ON SHEET M-50	001 FOR PIPE THRU WALL PE	NETRATION.
	9 ROUTE DRAIN THROUGH WAI	LL TO 6" ABOVE GRADE.	
	10 SEE DETAIL 3 ON SHEET M-50	000 FOR SPLIT SYSTEM UNIT	DETAIL.
	11 SEE DETAIL 2 ON SHEET M-50	001 FOR DUCT THRU WALL P	ENETRATION.
	12 SEE DETAIL 3, SHEET M-5002	FOR DUCT DETAIL.	
	13 SEE DETAIL 2, SHEET M-5002	FOR HEPA EXHAUST DUCT F	PENETRATION.
	14 SEE DETAIL 4, SHEET M-5000	FOR DUCT HANGER DETAIL.	
	15 CONCRETE PAD, REFER TO S	SHEET C55445-S-7000.	
	16 MOUNT BOTTOM OF UNIT HEA HUE-10 AT 10'-10" AFF.	ATERS, HUE-1 THRU HUE-5, I	HUE-9, AND
	17 CONCRETE PAD SHALL EXTE SIZE OF PAD WITH GENERAL		, COORDINATE
	18 MOUNT BOTTOM OF LOUVER	AT 8'-2" AFF.	
	(19) MOUNT BOTTOM OF LOUVER	AT 8'-2" AFF.	
	20 MOUNT FE-3 AT 10'-6" AFF TO	BOTTOM OF DUCT.	
	21 MOUNT BOTTOM OF HEATER	8'-6" AFF.	
	22 MOUNT THERMOSTAT AT 48"	AFF, TYPICAL.	
	(23) MOUNT BOTTOM OF DUCT AT	⁻ 6'-8" AFF.	
	(24) MOUNT BOTTOM OF LOUVER	AT 9'-2" AFF.	
	25 MOUNT FE-1 AT 8'-2" AFF TO E		
	(26) MOUNT FE-2 AT 8'-11" AFF TO	BOTTOM OF DUCT.	
			DE TOB - Man-
	4 08-31-16 U INCO	CR-448/DCN-579 RPORATE AS-BUILTS	B RB JMC BS
		FCR-315/DCN-471 FCR-233/DCN-386	DBRBJMCBSDBRBJMCBSEA
	1 11-06-13 U EA ADI	DED FIRE RISER ROOM	DB CM CM BS EA
	REV ADC		
	WEIDLINGER-NAV	ARRO JV NO	RTHERN NM
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	HVAC PLAN	l	CHECKED C. MOYERS

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"PRIORITY DRAWING"

FCR-448/DCN-579

INCORPORATE AS-BUILTS FCR-315/DCN-471

REVISED EQUIPMENT

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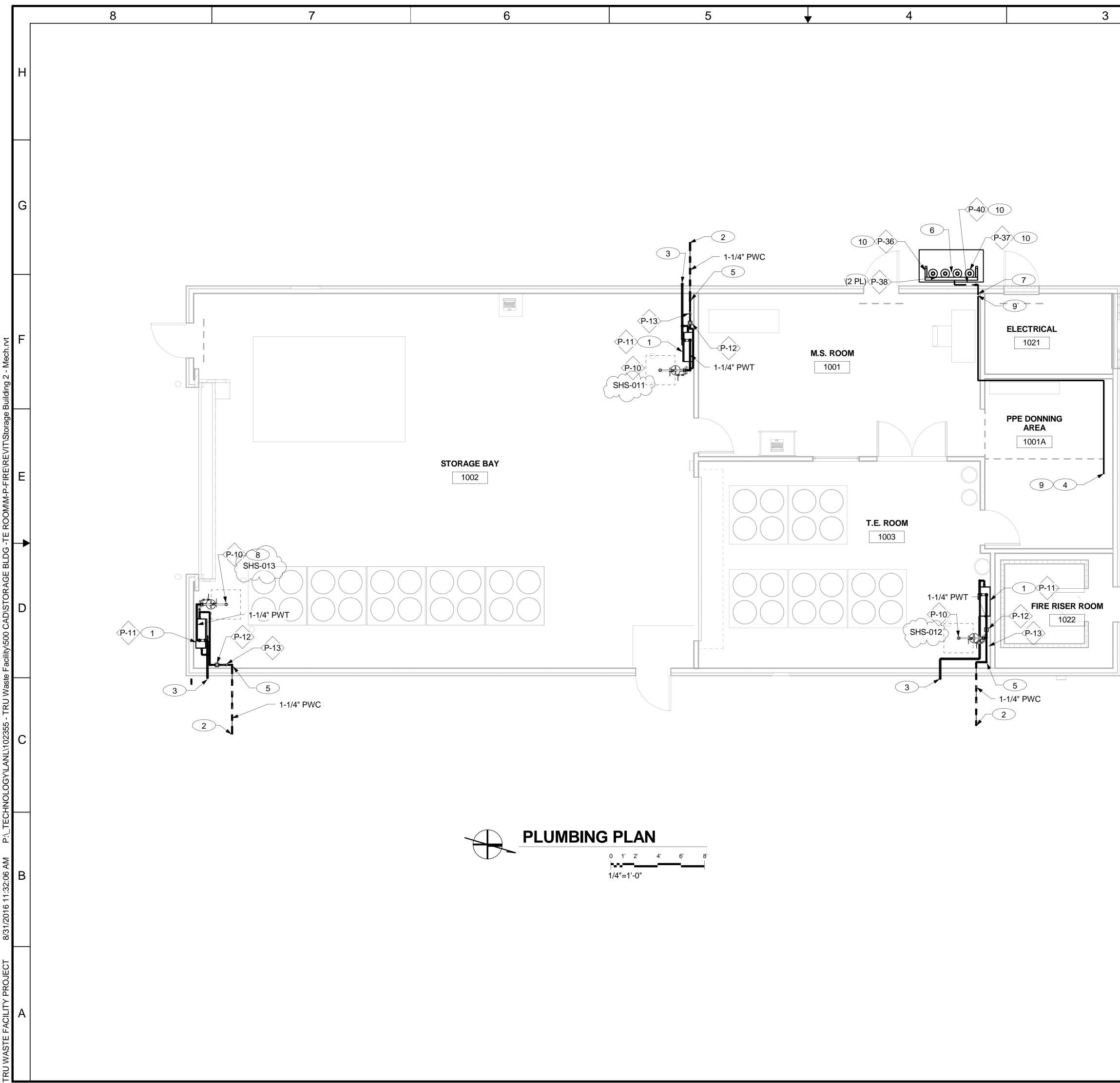
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GENERAL NOTES:

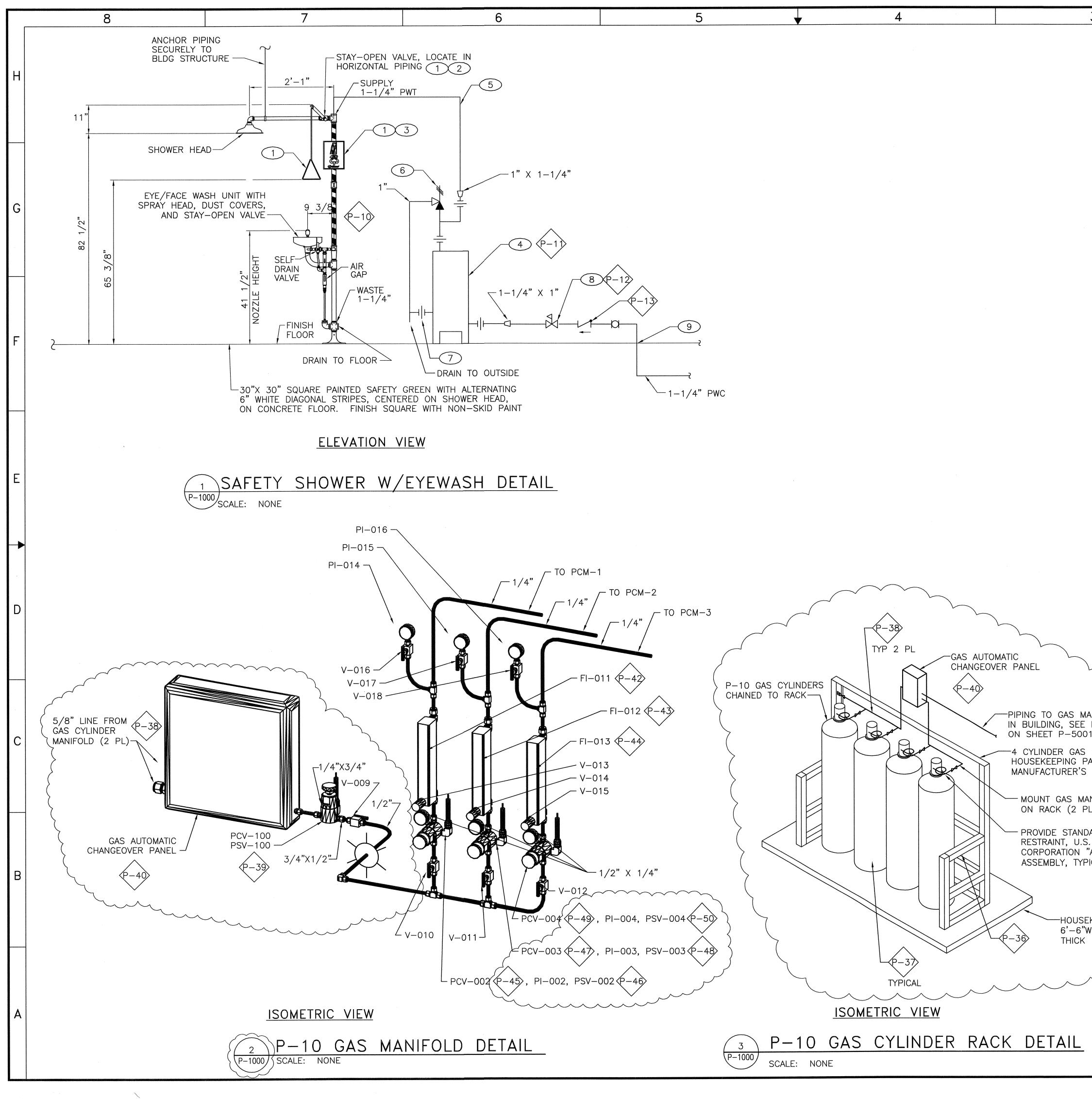
- 1. IF THIS SHEET IS NOT 24"x36", IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.
- 2. THIS DRAWING WAS GENERATED IN REVIT 2011.
- 3. SEE SHEET P-0001 FOR SYMBOLS, GENERAL NOTES AND LEGEND.
- 4. SEE SHEET P-7000 FOR EQUIPMENT SCHEDULE.

KEYED NOTES:

- 1 SEE DETAIL 1, SHEET P-5000 FOR WATER HEATER, CONNECTIONS, AND FLOOR PAINTING INSTRUCTIONS.
- 2 SEE SHEET C55443-C-1006 FOR CONTINUATION.
- 3 1" DRAIN FROM WATER HEATER RELIEF VALVE TO OUTSIDE. SEE DETAIL 2 ON SHEET P-5001 FOR PIPE THRU WALL PENETRATION.
- 4 ROUTE P-10 GAS PIPING TO RAD. PROT. AREA. SEE DETAIL 2 ON SHEET P-5000 FOR GAS MANIFOLD. FUTURE.
- 5 SEE DETAIL 1 ON SHEET P-5001 FOR PIPE THRU FLOOR PENETRATION.
- 6 SEE DETAIL 3 ON SHEET P-5000 FOR P-10 GAS CYLINDER RACK DETAIL. FUTURE.
- 7 P-10 PIPE THRU WALL. SEE DETAIL 2 ON SHEET P-5001 FOR PIPE THRU WALL PENETRATION. FUTURE.
- 8 CENTERLINE OF EMERGENCY SHOWER TO BE 5'-0" FROM EAST WALL. DASHED LINES DENOTE FREE SPACE REQUIRED FOR SHOWER.
- 9 CAP ABOVE CEILING.
- 10 FUTURE.

3	08-31-16	U		INCORPORAT	E AS-BUILTS		AB	KB	BCS	BE	
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GENERAL NOTES:

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1. SEE SHEET P-7000 FOR EQUIPMENT LIST.

KEYED NOTES:

1) FURNISHED WITH EMERGENCY EQUIPMENT.

2 VALVE TO BE ACCESSIBLE FOR MAINTENANCE.

3 EMERGENCY SIGN(S).

4 ELECTRIC SAFETY SHOWER TEPID WATER HEATER.

5 TEPID WATER SUPPLY.

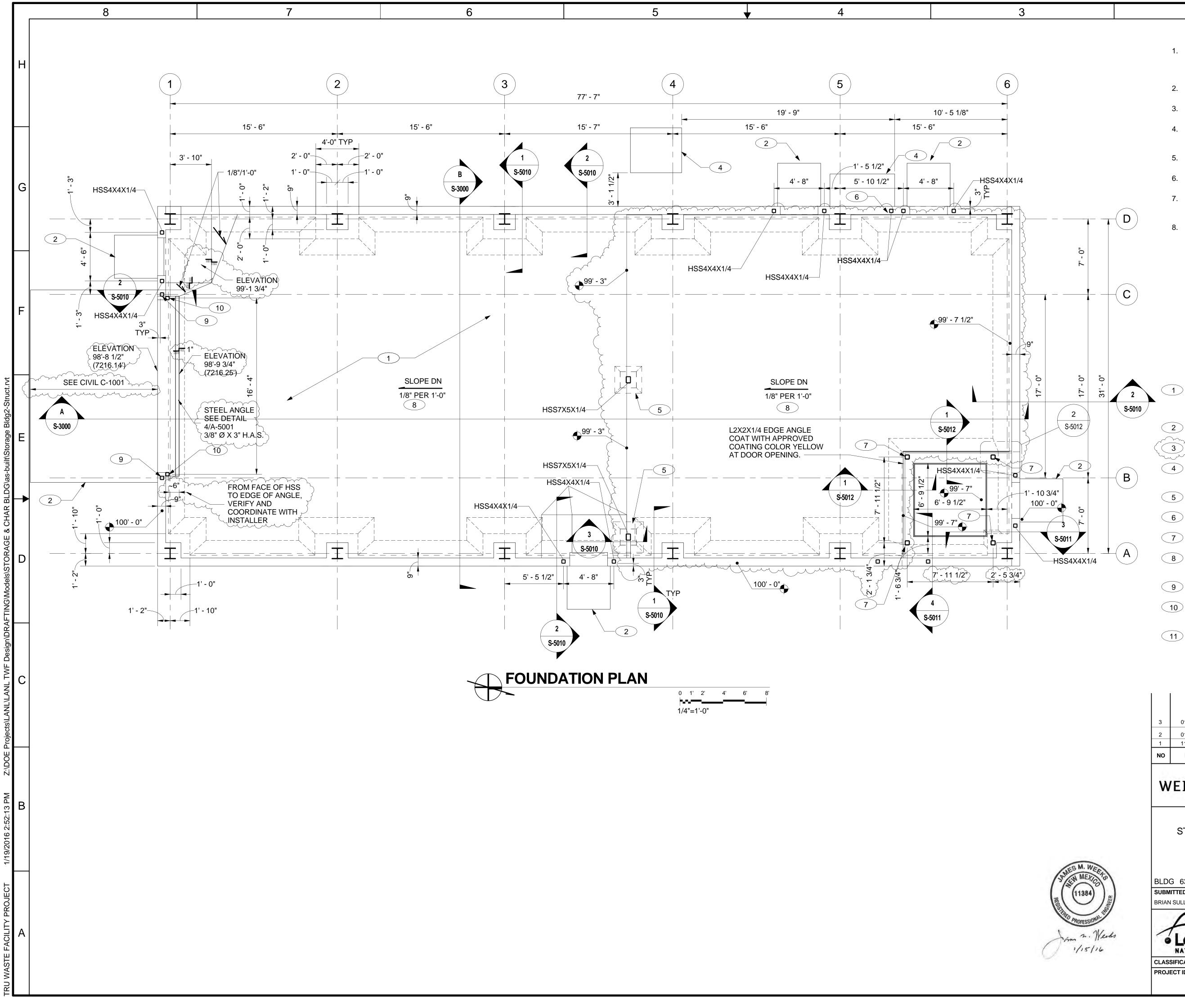
6 TEMPERATURE AND PRESSURE RELIEF VALVE.

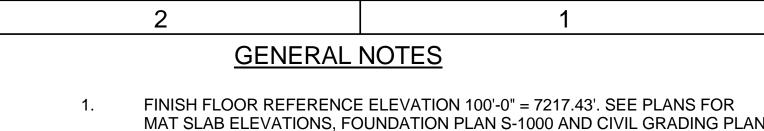
7 PROVIDE DIELECTRIC UNION AT POINT OF DISSIMILAR METALS.

8 PRESSURE REDUCING VALVE.

9 FLOOR PENETRATION, SEE DETAIL 1 ON SHEET P-5001.

ANIFOLD DETAIL 2											
RACK ANCHOR TO CONCRETE AD IN ACCORDANCE WITH WRITTEN INSTRUCTIONS										-	
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- SEE CIVIL PLANS FOR EXTERIOR SLAB AND PAVING. 2.
- SEE SOILS REPORT FOR UNDER SLAB AND FOOTING REQUIREMENTS. 3.
- IF THIS SHEET IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE 4. GRAPHIC SCALE ACCORDINGLY.
- THIS DRAWING WAS GENERATED IN REVIT 2014. 5.
- COORDINATE DRAIN PIPES THRU CURB WITH ARCH. 6.
- CONCRETE SLABS, FOOTINGS, AND ALL REINFORCEMENT THEREIN ARE 7. CLASSIFIED AS SAFETY SIGNIFICANT, ML-2.
- FOR SLAB STEPS, SEE 1/S-5011

C-1005.

8.

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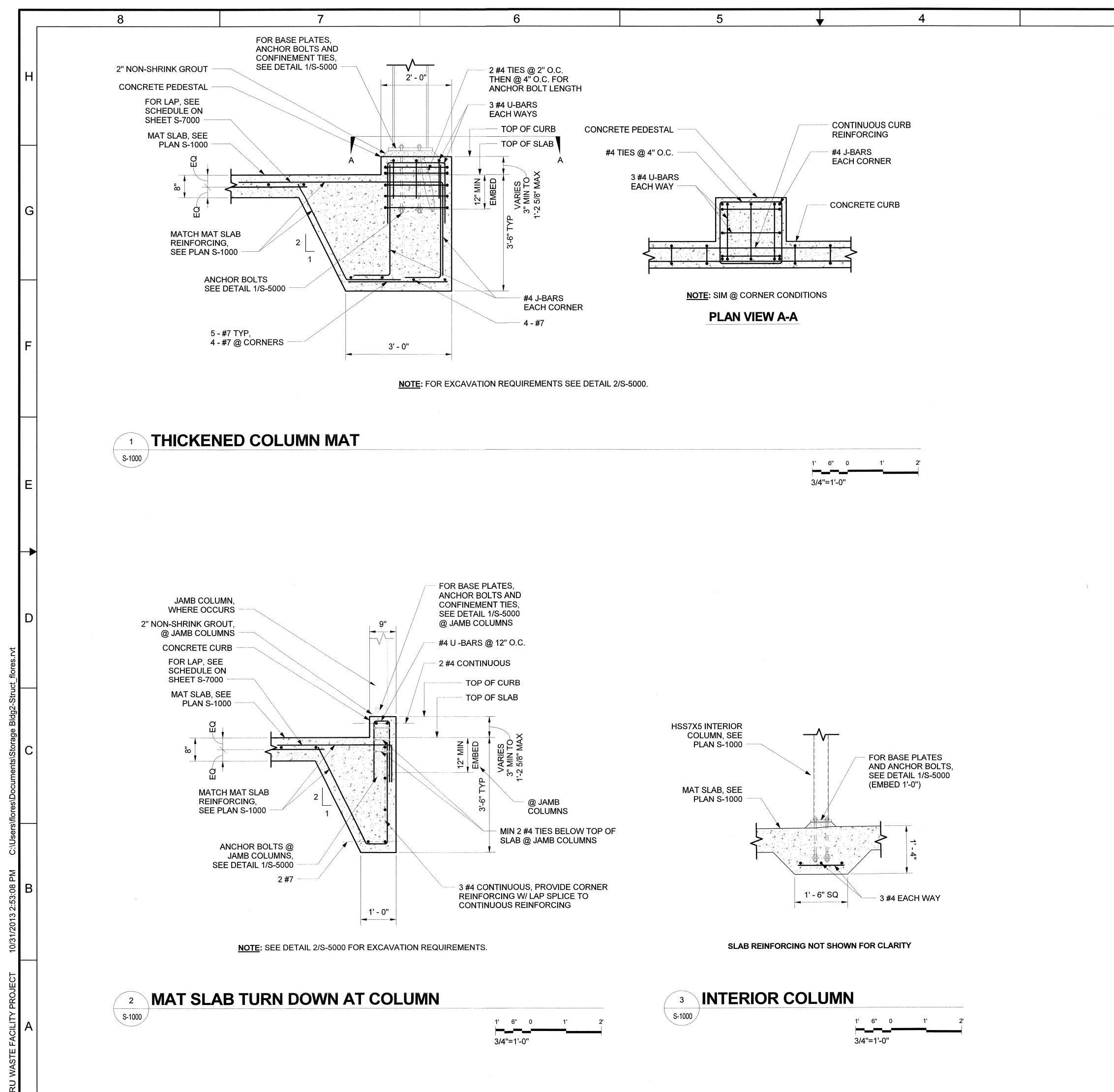
- 8" CONCRETE MAT SLAB WITH #6@9"O.C. EACH WAY, SEE DETAIL 3/S-5000. FOR STEPS IN SLAB SEE DETAIL 1/S-5011. SLAB IS PART OF THE LFRS, SAW CUTTING OF SLAB IS PROHIBITED.
- 2 CONCRETE STOOPS/RAMPS, SEE CIVIL SITE PLAN C-1001.

3 DELETED. mun

- 6" MIN HOUSEKEEPING PAD, SEE DETAIL 1/S-5001 AND SCHEDULE ON SHEET S-7000.
- THICKENED SLAB, SEE DETAIL 3/S-5010. (5)
- 6 AWNING SUPPORT, FOR LOACATION SEE A-1002.
- (HSS 5X5)FOR FIRE RISER ROOM, SEE DETAIL 4/S-5025. 7
- FLOOR SLOPE IS CLASSIFIED AS SAFETY CLASS. MINIMUM FLOOR SLOPE TOWARDS ROLL UP DOOR IS 1%. 8
- 9 HSS4X4X1/4 WALL SUPPORT JAMB.
- (10) HSS4X4X1/4 FIRE DOOR SUPPORT JAMB. VERIFY LOCATION WITH DOOR MANUFACTURER.
- 11 FOR FLOOR SLOPE ELEVATIONS, SEE ENLARGDE PLAN S-1010.

3	01/15/16	U			FCR-058, FCR-133, DCN-223, DCN-303	Þ	A.K.	50	DA.K.	P.C.	
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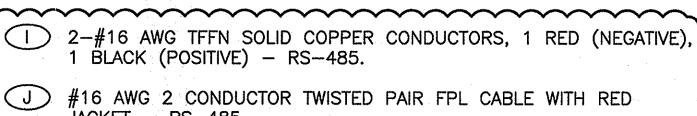


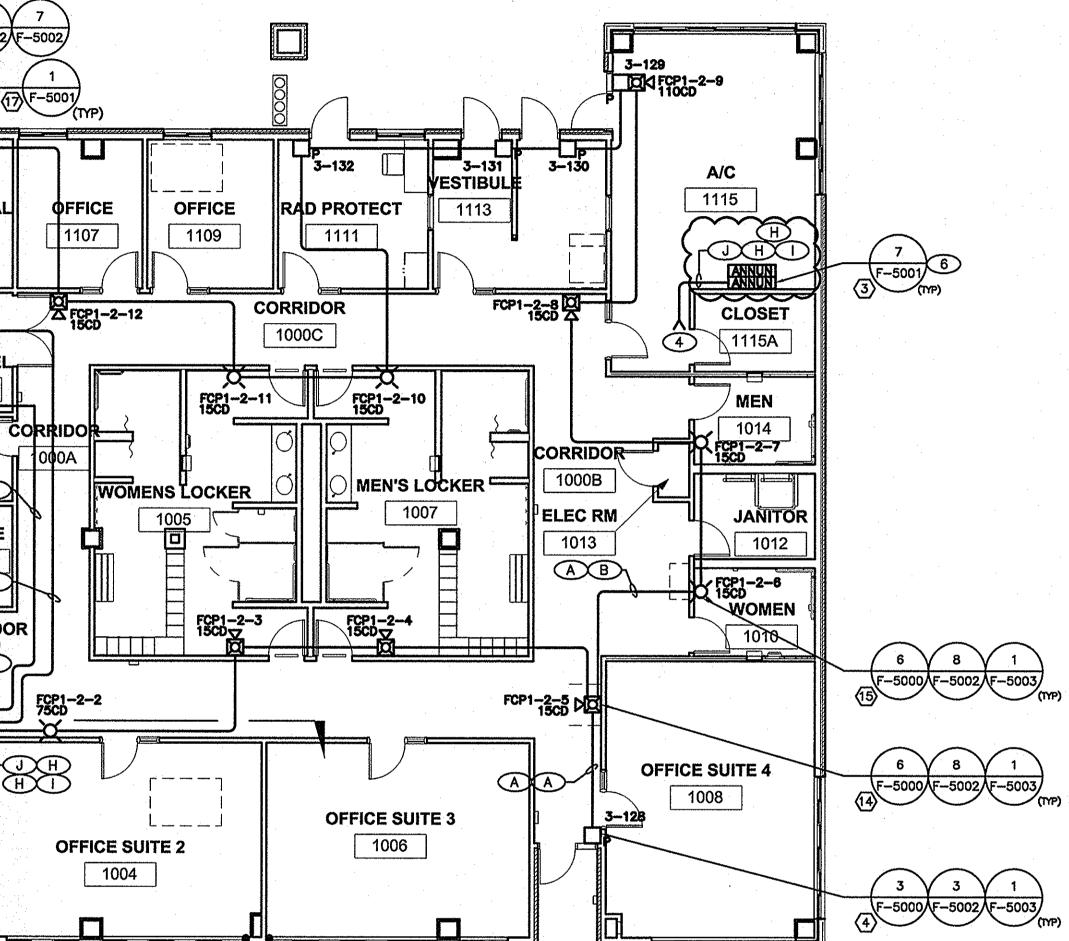


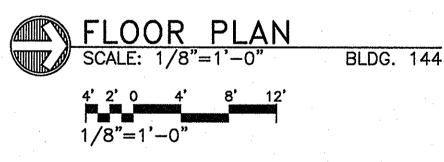
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		GENERAL	NOTES
	1.		ND ARE LOCATED ON SHEET S-0001 AND TES ARE LOCATED ON SHEET S-0002.
	2.	IF THIS SHEET IS NOT 24"x36 GRAPHIC SCALE ACCORDIN	6", THEN IT IS A REDUCED SIZE PLOT. USE GLY.
	3.	THIS DRAWING WAS GENER	ATED IN REVIT 2011.

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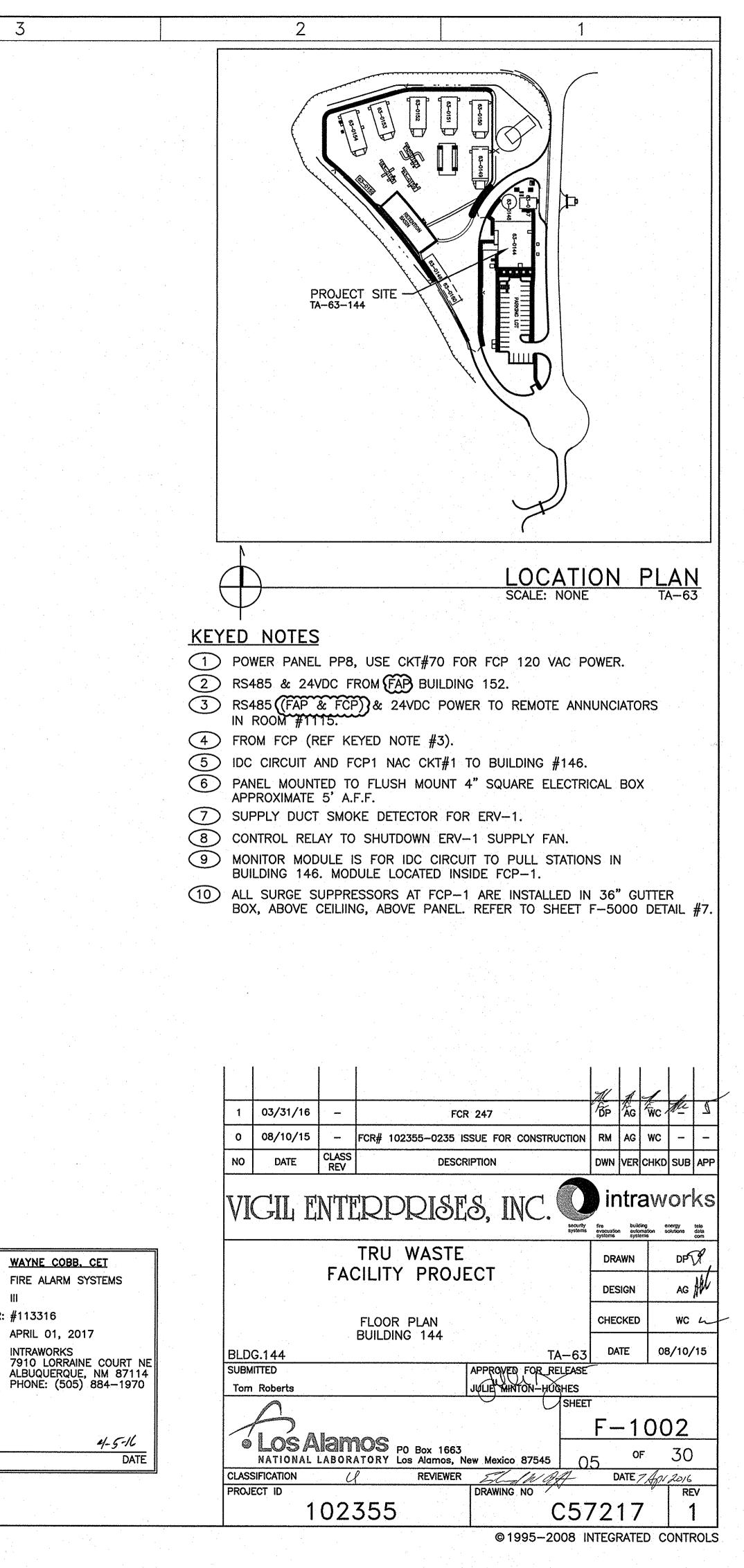
8 WIRING LEGEND (A) #16 AWG 2 CONDUCTOR TWISTED PAIR FPL CABLE WITH RED (|)JACKET – SLC. BLACK (POSITIVE) - RS-485. B 2-#12 AWG THHN SOLID COPPER CONDUCTORS, 1 BLUE \bigcirc (NEGATIVE), 1 YELLOW (POSITIVE) - NAC. JACKET - RS-485. C) 3-#12 AWG THHN SOLID COPPER CONDUCTORS, 1 BLACK (PHASE), 1 WHITE (NEUTRAL), 1 GREEN (GROUND) - 120VAC. \bigcirc 2-#16 AWG TFFN SOLID COPPER CONDUCTORS, 1 GRAY (NEGATIVE), 1 VIOLET (POSITIVE) - IDC. (E) LANL TELECOMMUNICATIONS GROUP TO FURNISH (2) CAT 5E CABLES (4 PAIR) WITH RED SHEATH. (F) 2-#16 AWG TFN SOLID COPPER CONDUCTORS, 1 GRAY (NEGATIVE), 1 VIOLET (POSITIVE) - RLED. G #16 AWG 2 CONDUCTOR FPLR CABLE WITH BLACK JACKET-"WET LOCATION" - SLC UNDERGROUND. -5002/F-5002 (H) #12 AWG THHN SOLID RED & BLACK-ANNUNCIATOR POWER FROM FAP. F-5001 ABD 3-133 ELECTRICAL MECHANICAL 1105 7 3-135 102 FILED 3-135 138 FV 3-002 F 3-002 A CICICI A CR 3-140 B 3-137/138/159 8 V DATA / TEL (TYP) F-5000 F-5002 8A A B 1103 9 2 F-5001 F-5002 9 MAIL CONF. / BREAK 1101 1001 E FCP1-2-14 OFFICE 5 1003 F-5000/F-5002//5 \odot CORRIDOR 1000 3-001 AXA HU F-3000 **OFFICE SUITE 1** 3-128 91 1002 **PIV** #2370 GENERAL NOTES LANL TELECOMMUNICATIONS GROUP SHALL FURNISH AND TERMINATE ALL TELEPHONE CABLING. ELECTRICAL CONTRACTOR IS TO INSTALL TELECOMMUNICATIONS CONDUIT. FIRE ALARM CONTRACTOR TO PULL LANL SUPPLIED TELEPHONE CABLE. 2. ALL CONDUITS SHOWN SHALL BE 3/4" EMT UNLESS OTHERWISE NOTED. 3. ELECTRICAL CONTRACTOR SHALL INSTALL CONDUIT AND CONDUCTORS FOR POWER 120VAC SYSTEM. ELECTRICAL CONTRACTORS SHALL INSTALL AND TERMINATE 120VAC SURGE SUPPRESSION DEVICES SUPPLIED BY THE FIRE ALARM CONTRACTOR. ELECTRICAL CONTRACTOR SHALL INSTALL THE FIRE ALARM CONDUIT 4. SYSTEM, INCLUDING JUNCTION BOXES, SUPPORTS, ETC. FIRE ALARM CONTRACTOR SHALL INSTALL WIRE, DEVICES AND TERMINATE THE FIRE ALARM CONDUCTORS. REFER TO THE F-8000 SERIES OF SHEETS FOR BATTERY & VOLTAGE 5. DROP CALCULATIONS. CONDUIT SYSTEM ROUTING SHOWN ON DRAWING IS DIAGRAMMATIC. 6. ELECTRICAL CONTRACTOR MAY DEVIATE FROM PATH SHOWN IF REQUIRED BY EXISTING FIELD CONDITIONS WITHIN THE BUILDING AND/OR EXISTING FIELD CONDITIONS WITHIN THE CEILING SPACE. FIRE ALARM DEVICE SEQUENCE SHALL REMAIN AS SHOWN. ELECTRICAL CONTRACTOR SHALL INSTALL PULL BOXES ON THE NEW CONDUIT RUNS, AS REQUIRED, TO COMPLY WITH NFPA 70 AND TO LIMIT THE CABLE PULLING TENSION AS TO NOT DAMAGE THE NEW CABLING. 7. ALL FIRE ALARM DEVICES. CONDUIT AND CABLING SHOWN IS NEW UNLESS OTHERWISE NOTED. REFER TO SHEETS F-0001 AND E-0001 FOR ADDITIONAL 8. INFORMATION APPLICABLE TO THIS PROJECT. 9. IF THIS SHEET IS NOT 24" X 36". THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.

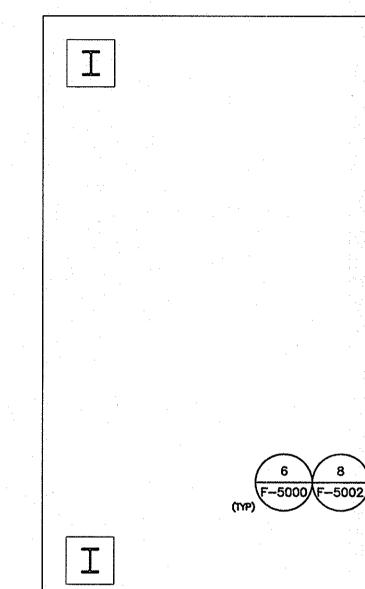






NAME: NICET SUB FIELD: NICET LEVEL: CERTIFICATE NUMBER: #113316 CERT. EXP. DATE: ADDRESS: Wh Chh SIGNATURE





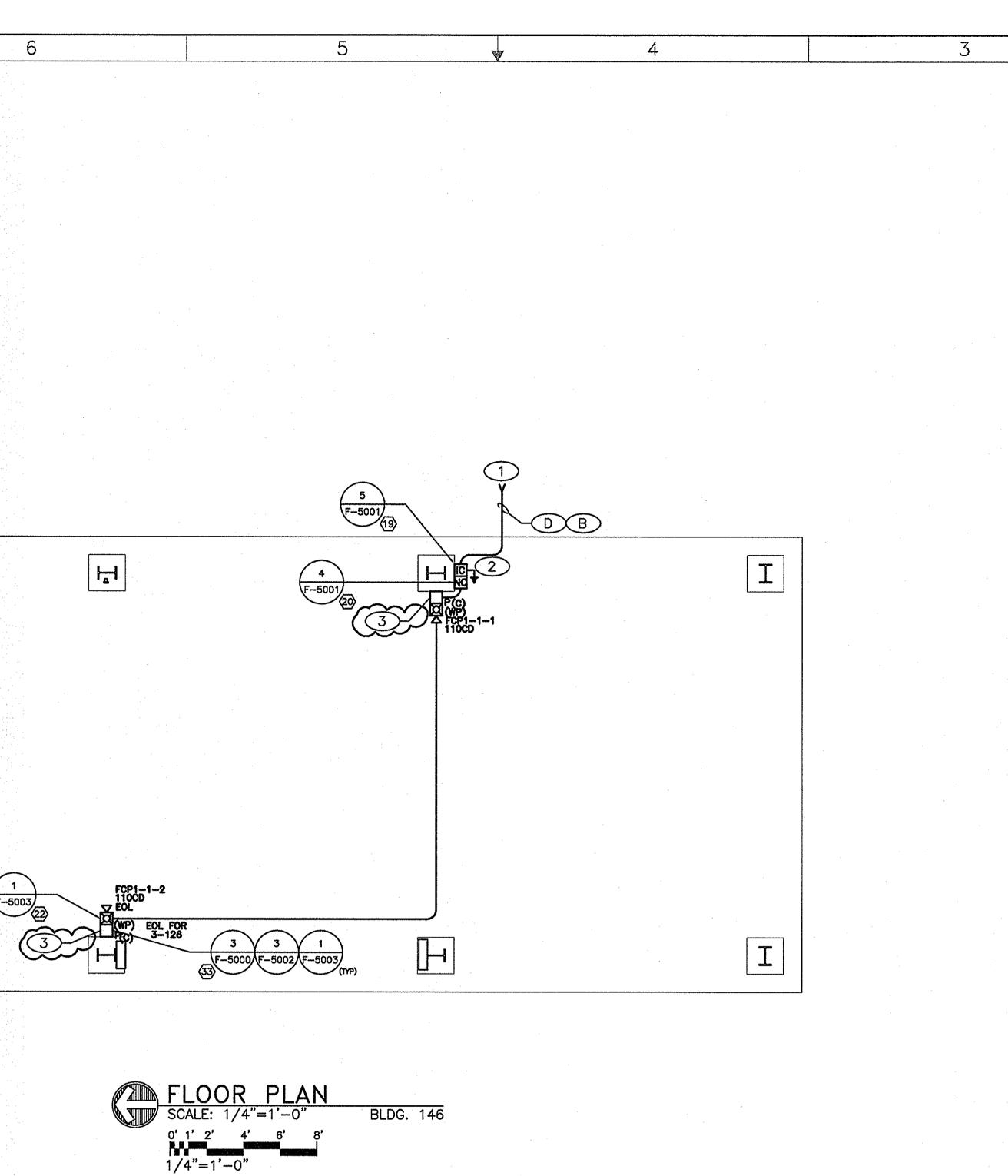
GENERAL NOTES

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- 1. LANL TELECOMMUNICATIONS GROUP SHALL FURNISH AND TERMINATE ALL TELEPHONE CABLING. ELECTRICAL CONTRACTOR IS TO INSTALL TELECOMMUNICATIONS CONDUIT. FIRE ALARM CONTRACTOR TO PULL LANL SUPPLIED TELEPHONE CABLE.
- 2. ALL CONDUITS SHOWN SHALL BE 3/4" EMT UNLESS OTHERWISE NOTED.
- 3. ELECTRICAL CONTRACTOR SHALL INSTALL CONDUIT AND CONDUCTORS FOR POWER 120VAC SYSTEM. ELECTRICAL CONTRACTORS SHALL INSTALL AND TERMINATE 120VAC SURGE SUPPRESSION DEVICES SUPPLIED BY THE FIRE ALARM CONTRACTOR.
- 4. ELECTRICAL CONTRACTOR SHALL INSTALL THE FIRE ALARM CONDUIT SYSTEM, INCLUDING JUNCTION BOXES, SUPPORTS, ETC. FIRE ALARM CONTRACTOR SHALL INSTALL WIRE, DEVICES AND TERMINATE THE FIRE ALARM CONDUCTORS.
- 5. REFER TO THE F-8000 SERIES OF SHEETS FOR BATTERY & VOLTAGE DROP CALCULATIONS.
- 6. CONDUIT SYSTEM ROUTING SHOWN ON DRAWING IS DIAGRAMMATIC. ELECTRICAL CONTRACTOR MAY DEVIATE FROM PATH SHOWN IF REQUIRED BY EXISTING FIELD CONDITIONS WITHIN THE BUILDING AND/OR EXISTING FIELD CONDITIONS WITHIN THE CEILING SPACE. FIRE ALARM DEVICE SEQUENCE SHALL REMAIN AS SHOWN. ELECTRICAL CONTRACTOR SHALL INSTALL PULL BOXES ON THE NEW CONDUIT RUNS, AS REQUIRED, TO COMPLY WITH NFPA 70 AND TO LIMIT THE CABLE PULLING TENSION AS TO NOT DAMAGE THE NEW CABLING.
- 7. ALL FIRE ALARM DEVICES, CONDUIT AND CABLING SHOWN IS NEW UNLESS OTHERWISE NOTED.
- 8. REFER TO SHEETS F-0001 AND E-0001 FOR ADDITIONAL INFORMATION APPLICABLE TO THIS PROJECT.
- 9. IF THIS SHEET IS NOT 24" X 36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.

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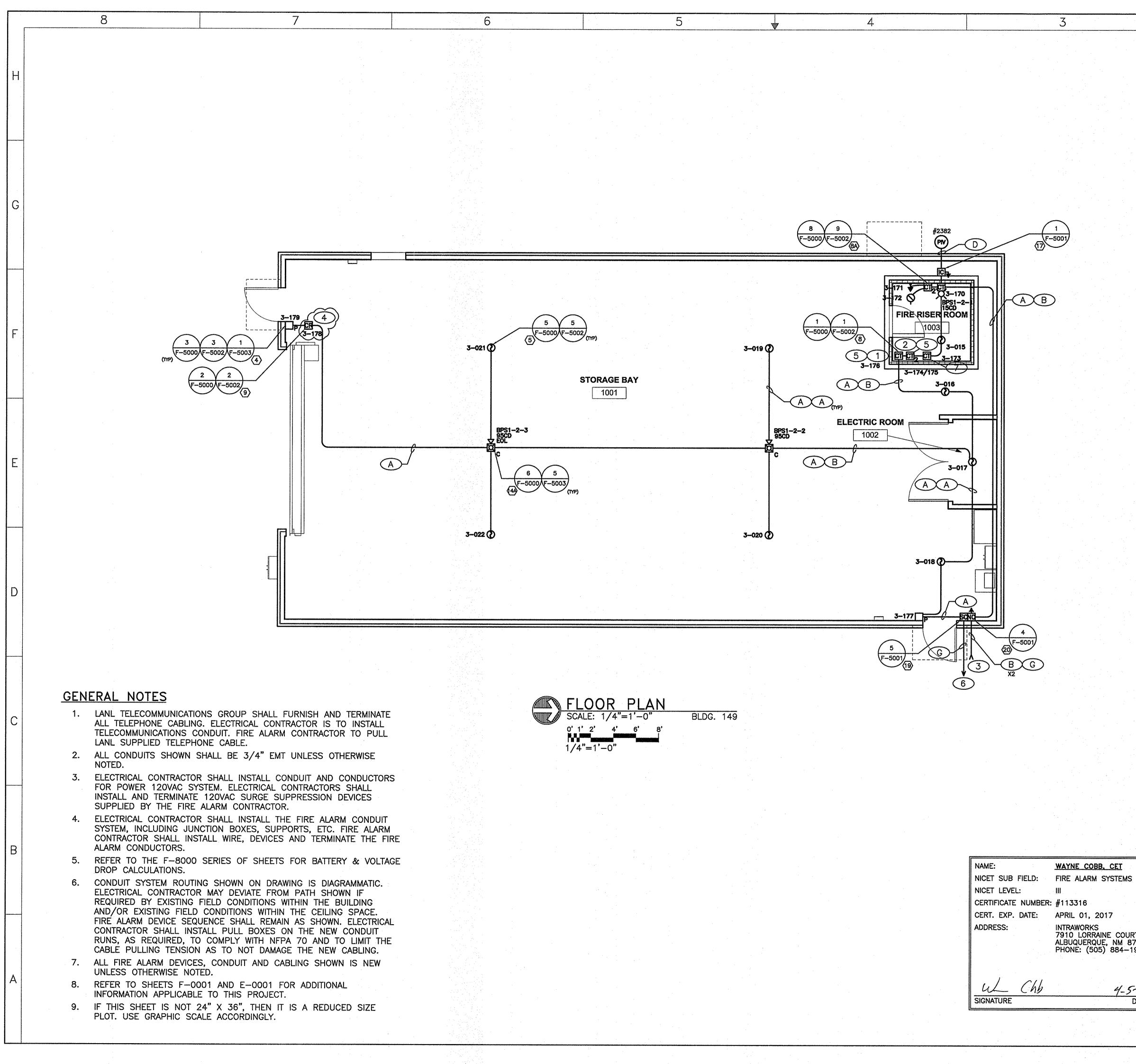
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NAME:	WAYNE COBB.
NICET SUB FIELD:	FIRE ALARM S
NICET LEVEL:	111
CERTIFICATE NUMBER:	#113316
CERT. EXP. DATE:	APRIL 01, 201
ADDRESS:	INTRAWORKS 7910 LORRAIN ALBUQUERQUE

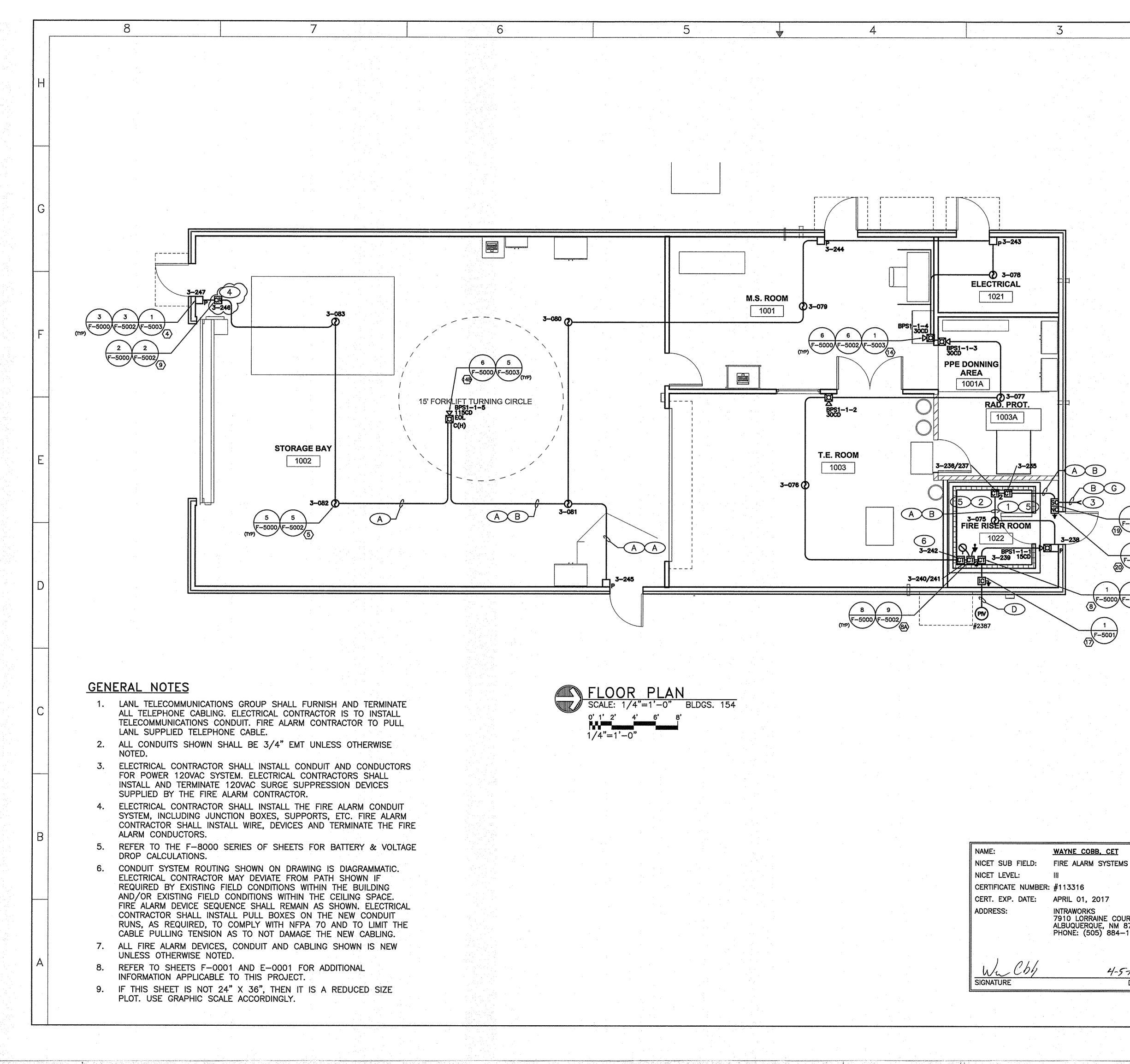
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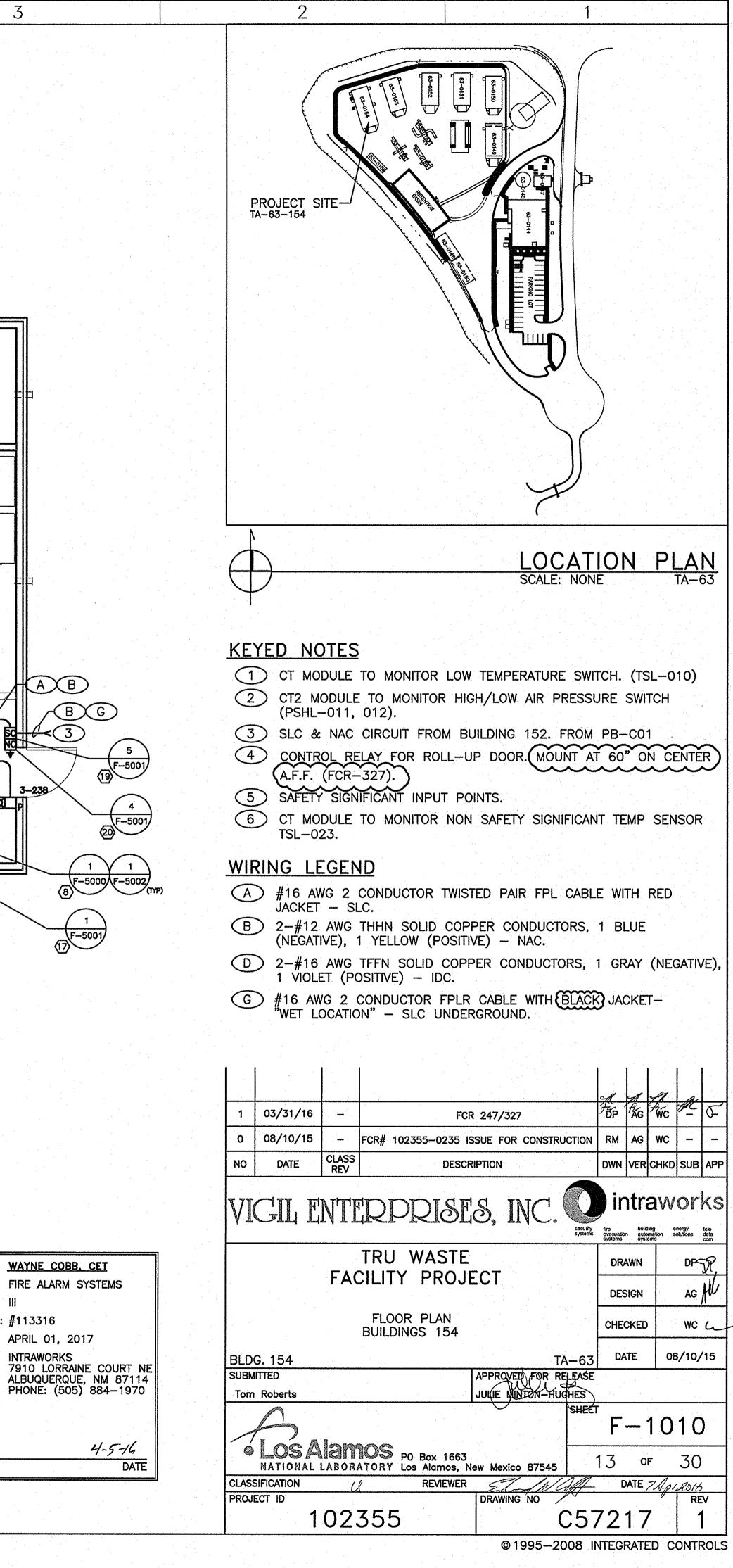
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	LOCATION PLAN
	SCALE: NONE TA-63
	KEYED NOTES
	1) IDC & NAC CIRCUIT FCP-1 FROM FCP IN BUILDING #144.
	2 INSTALL NAC AND SLC SURGE SUPPRESSORS IN NEMA ENCLOSURE (6"x6")
	(3) INSTALL PULL STATION IN WEATHER PROOF ENCLOSURE
	(MODEL# STI-1230)
	WIRING LEGEND
	(A) #16 AWG 2 CONDUCTOR TWISTED PAIR FPL CABLE WITH RED JACKET – SLC.
	B 2-#12 AWG THHN SOLID COPPER CONDUCTORS, 1 BLUE (NEGATIVE), 1 YELLOW (POSITIVE) - NAC.
	D 2-#16 AWG TFFN SOLID COPPER CONDUCTORS, 1 GRAY (NEGATIVE) 1 VIOLET (POSITIVE) - IDC.
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WAYNE COBB. CET FIRE ALARM SYSTEMS	FACILITY PROJECT
III	FLOOR PLAN
#113316 APRIL 01, 2017	BUILDING 146
INTRAWORKS 7910 LORRAINE COURT NE ALBUQUERQUE, NM 87114	BLDG. 146 TA-63 DATE 08/10/15 SUBMITTED APPROVED FOR RELEASE
ALBUQUERQUE, NM 87114 PHONE: (505) 884-1970	Tom Roberts DULLE MINTON HUGHES
	F-1003
<u>4-5-16</u> DATE	• LOS Alamos PO Box 1663 NATIONAL LABORATORY Los Alamos, New Mexico 87545 06 OF 30
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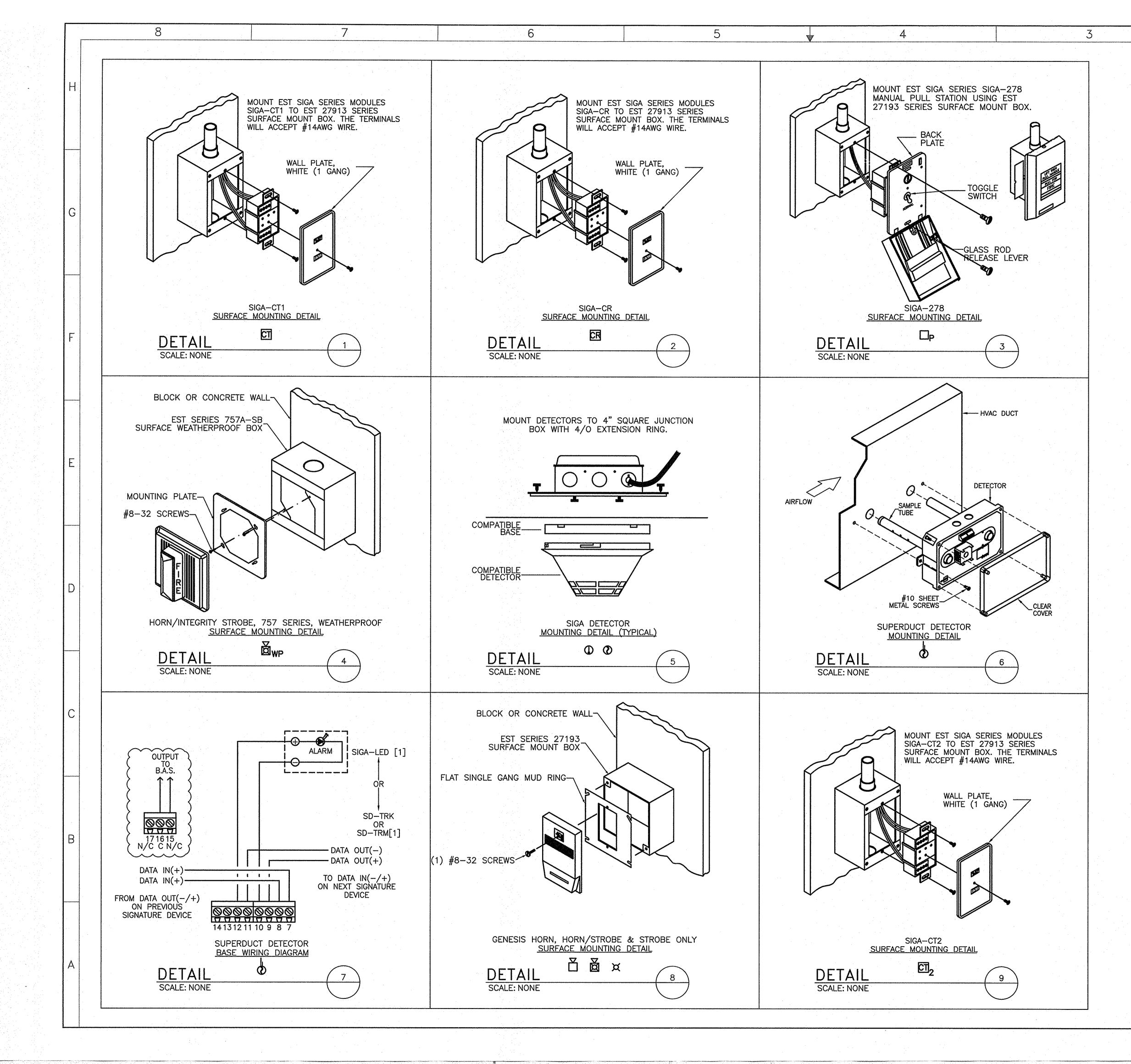


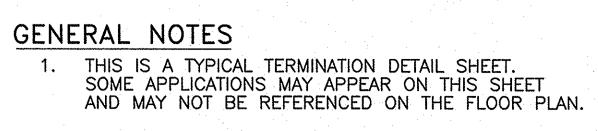
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NAME:	WAYNE COBB, CET
NICET SUB FIELD:	FIRE ALARM SYSTEMS
NICET LEVEL:	111
CERTIFICATE NUMBER:	#113316
CERT. EXP. DATE:	APRIL 01, 2017
ADDRESS:	INTRAWORKS 7910 LORRAINE COURT NE ALBUQUERQUE, NM 87114 PHONE: (505) 884-1970
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SIGNATURE	DATE

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WAYNE COBB, CET NAME: NICET SUB FIELD: FIRE ALARM SYSTEMS NICET LEVEL: 111 CERTIFICATE NUMBER: #113316 CERT. EXP. DATE: APRIL 01, 2017 INTRAWORKS 7910 LORRAINE COURT NE ALBUQUERQUE, NM 87114 PHONE: (505) 884–1970 ADDRESS: DATE SIGNATURE

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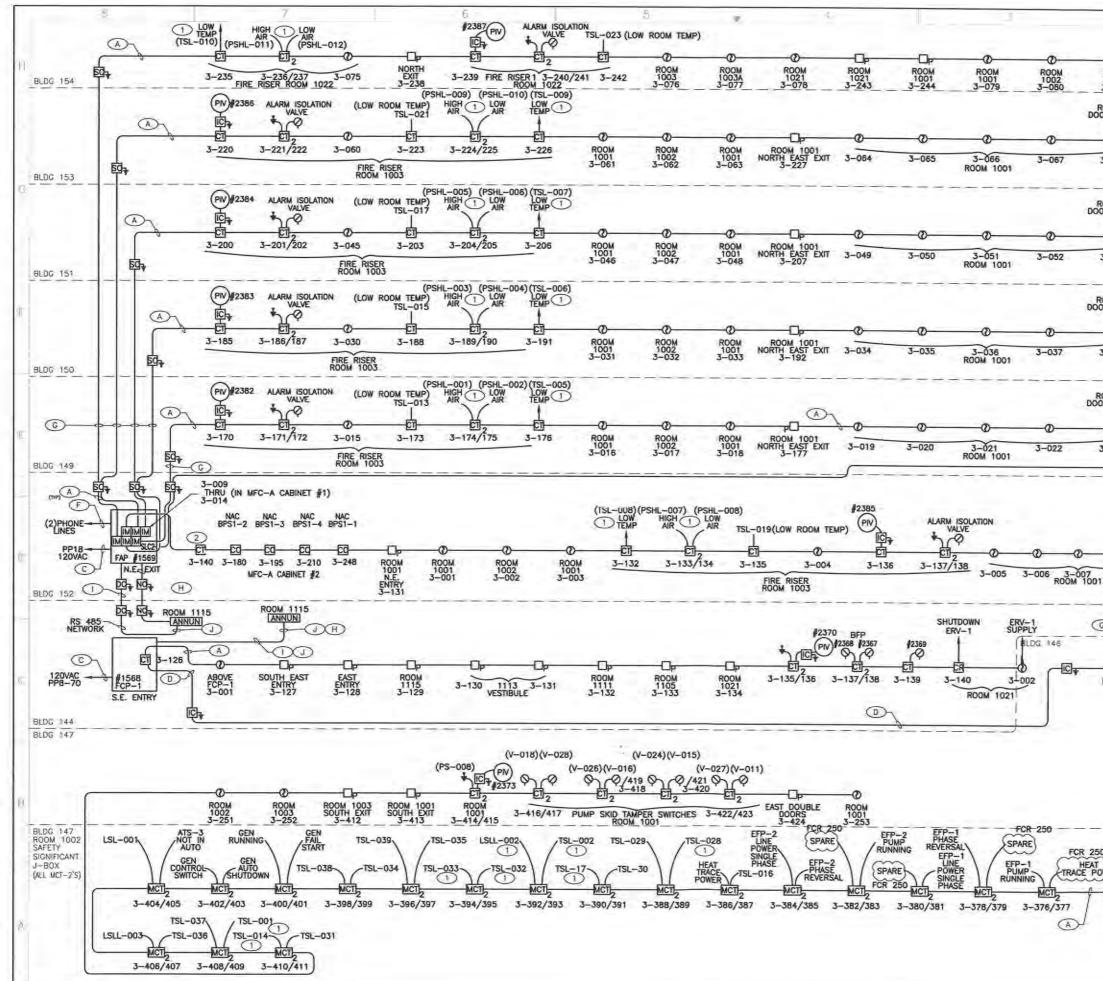
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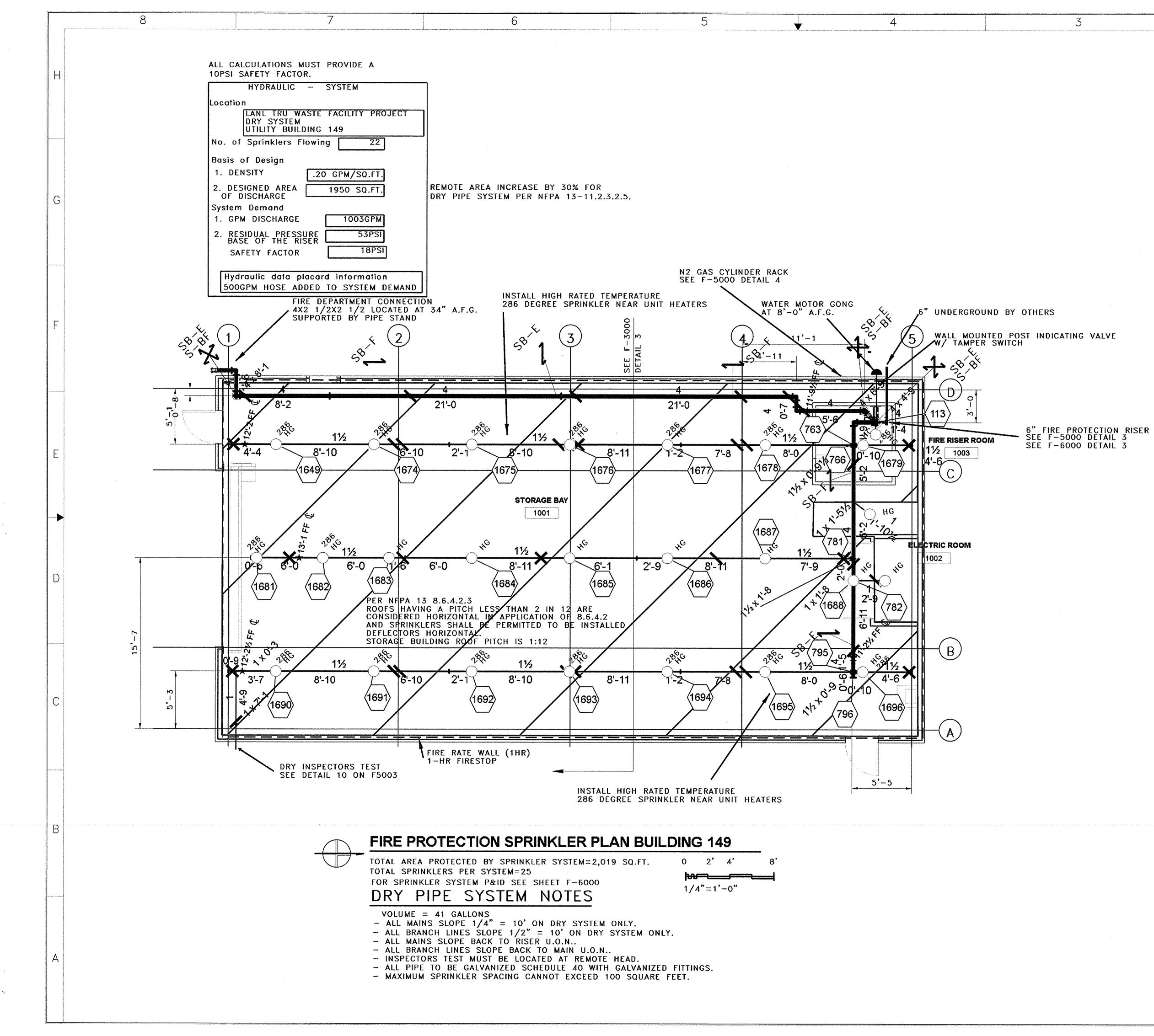
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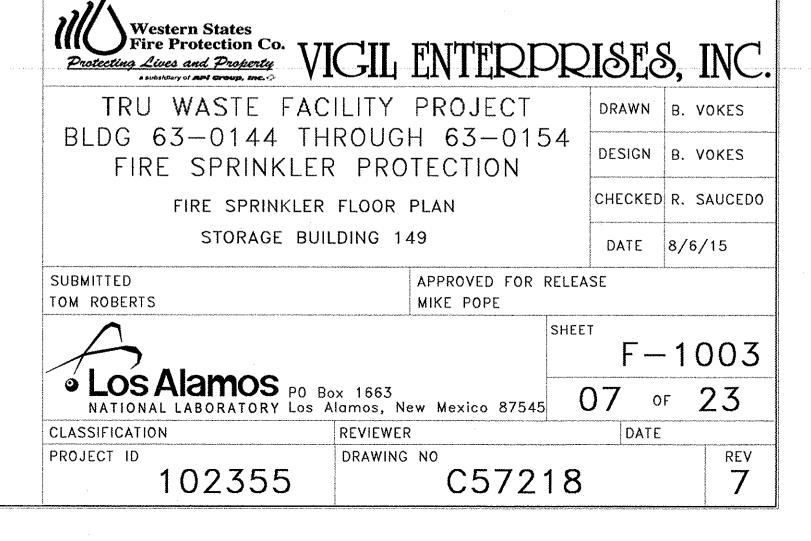
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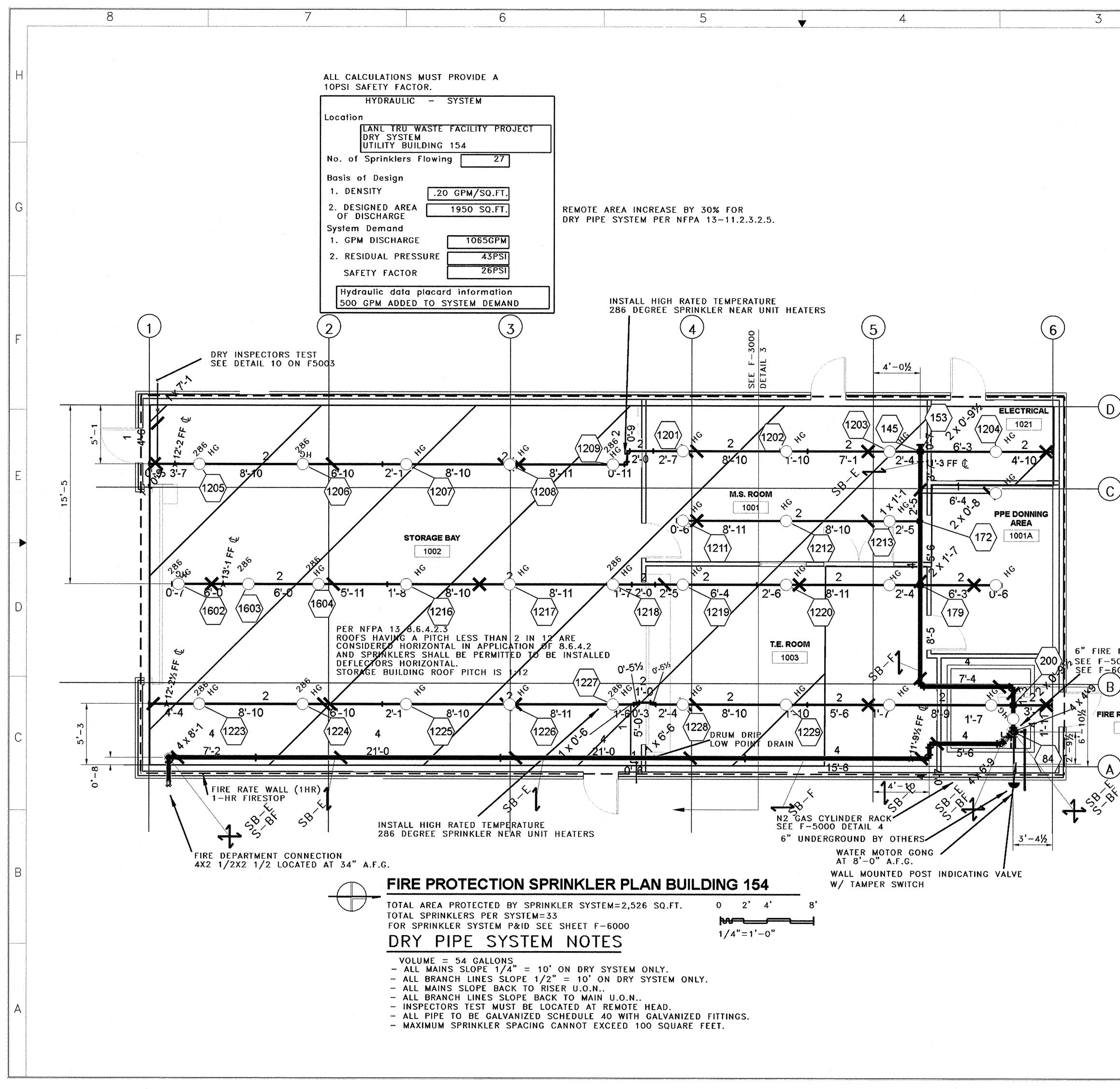


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100103 NICET No.

Document:TA-63 TWF Construction ReportDate:January 2017

Hydraulic Calculation 14055020-FP-C-001

Document:TA-63 TWF Construction ReportDate:January 2017

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VIGIL ENTERPRISES, INC.

ENGINEERING CALCULATIONS

Checking Parameters

	Check Parameter	Y	Ν	Remarks
1	A new calculation has a unique number; a revised	V		
	calculation has the next revision number.	Х		
2	The objective is clearly stated	Х		
3	Any limitations of the calculation are documented.	Х		
4	The acceptance criteria are valid and appropriate	Х		
5	The analytical methods are valid and appropriate	Х		
6	Any computer code used meets the requirements of QIP 3.2	Х		
7	The assumptions are reasonable, adequately justified, and appropriately conservative	Х		
8	The input values accurately reflect the design and operation that no transcription errors have occurred.	Х		
9	The appropriate and conservative input value was selected (especially when an input value may legitimately vary within a range).	х		
10	The reference documents for input values are appropriate	Х		
11	The calculation employs the stated methodology.	Х		
12	The calculation uses the documented input values and assumptions	Х		
13	All formulae, input values, and assumptions, used in the calculation are documented in the corresponding sections.	Х		
14	The numerical results of hand calculations are accurate by checking each line and performing each mathematical computation.	х		
15	The numerical results of spreadsheet calculations are accurate by verifying that the input values and computational formulas are correct.*	х		
16	The macros created with commercial off-the-shelf software are properly written and produce correct results.	Х		
17	The numerical results of computer-generated calculations are reasonable, the computer program is applicable and valid, the computer inputs are correct.	х		
18	The results correspond to the objective of the calculation.	Х		
19	The results are correctly evaluated against the acceptance criteria	Х		
20	The calculation is complete from start to finish, that no gaps are present.	Х		
21	The summary and conclusions are accurate	Х		

* **Note:** If formula is repeated across multiple spreadsheet cells, the Checker should verify that one cell has the correct formula and spot check the same formula was copied to the other cells.

* **Note:** If the spreadsheet is an approved standard spreadsheet, then it must comply with the requirements of QIP 3.2

a) Alternate Calculation: Checker checks the calculations for attributes as described under the Detailed Review above, except that it is not necessary to check the calculation line by line for numerical accuracy.

1. Checker prepares a new calculation called the "Alternate Calculation" that applies another appropriate method to achieve the same or similar result to gauge the reasonableness and accuracy of the original calculation.

Signature	Date

VIGIL ENTERPRISES, INC.

CALCULATION COVER SHEET									
Client: LANL	A 62 TWE	Page 1 of							
Project: LANL TA-63 TWF Calc. Title: Fire Sprinkler Hydraulic Calculations QA Class: (refer to EWP)									
	055020-FP-CAL-0								
Task No.:NA			Design Verification Req'd:						
Discipline: FIRE	SPRINKLER	Alternate Method Calculation Used:							
Approvals – Signati	Assumption(s) Require Confirmation Yes No								
Preparer	Preparer Checker Design Rev. or Verifier New Calc No.								
BRAD VOKES	RUDY SAUCEDO	REV 2							
DISTRIBUTION									
Senior Project Manager QA Files									

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Assumptions	3
Method	3
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Conclusions	4

Objective

 Analyze flow and pressure requirements of the sprinkler systems for Buildings 144, 147, 149, 150, 151, 152, 153 and 154 to ensure compliance with the authority having jurisdiction, national codes and standards.

Assumptions

1. The sprinkler head layout is based on coordinated design.

Method

- 1. Layout fire protection piping systems on CAD based engineering equipment. Includes Buildings 144, 147, 149, 150, 151, 152, 153 and 154.
- Run hydraulic calculations to optimize system requirements. See NFPA 13 (2010 Edition) Section 22.
- 3. Make decisions on the most efficient use of the sprinkler system.
- 4. Check compliance with national codes and standards.
- 5. Submit for approval to the authority having jurisdiction.
- 6. Verification and Validation for the MEPCAD Software was performed prior to calculations. See attached log sheet and test calculation. See attachment A.

Inputs

- 1. NFPA 13 (2010 Edition)
- 2. Fire Hydrant Flow Data was from Hydrant 17-455 at TA-63 near TRU Waste Facility and Building 65-111. Hydrant elevation is 7,201 feet. Test date was 12-11-14. Static Pressure 68 psi, Hydrant Flow was 637 gpm at a Residual Pressure of 60 psi.
- 3. Fire Pump (by others) rated at 1250 gpm at 52 psi. The fire pump is located in Utility Building 147.
- 4. Pipe lengths and fittings for piping from Hydrant 17-455 were taken from Fire Protection Site Plan.
- 5. LBO Drawings C55443, C55444, C55445, C55446, C55904, C55905, C55906 and C55907.

Incoming Letters

1. NA

Software

1. M.E.P.CAD Autosprink VR11, Version: VR11 11.0.30.0, Manufacturer: M.E.P.CAD, Inc. Machine ID CNU2310PVX

References

1. NFPA 13 (2010 Edition)

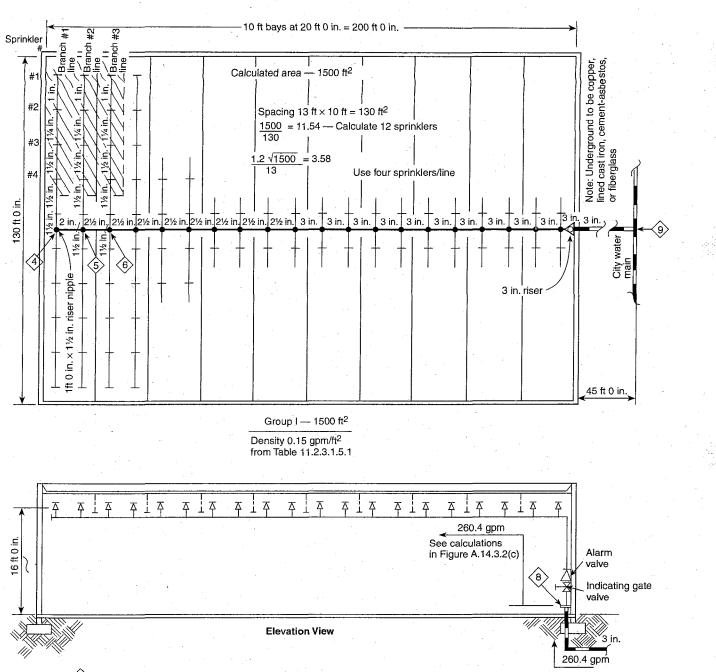
- 2. IFC, 2009 International Fire Code, International Code Council, Inc., Washington D.C.
- 3. M.E.P.CAD Autosprink VR11
- 4. LANL ESM, Engineering Standards Manual, ISD 341-2, Los Alamos National Laboratories, Los Alamos, New Mexico. Chapter 2, "Fire Protection," Section D40, ""Fire Protection," Rev. 3, 6/18/08.
- 5. DOE Standard-Fire Protection Design Criteria DOE-STD-1066-99
- 6. LANL Specification 21 1313 (Wet Pipe Sprinkler Systems)

Conclusions

 Results are based on the hydraulic calculations provided in attachment B. They include hydraulic calculations for Buildings 144, 147, 149, 150, 151, 152, 153 and 154. The system demands for all buildings are within the capabilities of the TA-63 water supply and fire pump. All calculations included a minimum of 10 psi safety factor and a 500 gal/min hose allowance.

Attachment A

MEPCAD Verification and Validation



----- Reference step

2002 Edition

FIGURE A.14.3.2(b) Hydraulic Calculation Example (Plan View and Elevation View).

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Step No.	Τ		е 🛄		UPI	1500 ft ²						Sheet 2_0	f <u>3</u>
		Nozzie Ident. and ocation		-low in gpm	Pipe Size	Pipe Fittings and Devices	Equiv. Pipe Length	Friction Loss psi Foot	Pr Su	essure mmary	Pressure	D = 0.15 GPM/ ft ² Notes K = 5.6	Ref. Step
1	1	BL-1	q Q	19.5	1	- 	L 13.0 F T 13.0	C=120 0.124	P _t P _e P _f	12.1 1.6	P _t P _v P _n	Q = 130 x 0.15 = 19.5 P = (19.5/5.6) ² = 12.1 psi	
2	2		q	20.7 40.2	1 ¹ /4		L 13.0 F T 13.0	0.125	P _t P _e P _f	13.7	P _t P _v P _n	q = 5.65 √13.7	-
3	3		q Q	21.9 62.1	1 ¹ /2		L 13.0 F T 13.0	0.131	P _t P _e P _f	15.3	P _t P _v P _n	q = 5.65 √15.3	4
4	4	DN RN	q	23.1 85.2	1 ¹ /2	2T-16	L 20.5 F 16.0 T 36.5	0.236	P _t P _e P _f	17.0 0.4 8.6	P _t P _v P _n	$q = 5.65 \sqrt{17}$ $P_e = 1 \times 0.433$	5
5		CM TO BL-2	q	85.2	2		L 10.0 F T 10.0	0.07	P _t P _e P _f	26.0 0.7	P _t P _v P _n	$K = \frac{\underline{85.2}}{\sqrt{26}}$ K = 16.71	
6		BL-2 CM TO BL-3		86.3 171.5	2 ¹ /2		L 10.0 F T 10.0	0.107	P _t P _e P _f	26.7	P _t P _v P _n	q = 16.71 √26.1	6
7		BL-3 CM	q	0.0.1	2 ¹ /2		L 70.0 F T 70.0	0.231	P _t P _e P _f	27.8 16.2	P _t P _v P _n	q = 16.7 √27.8	
8		CM TO FIS	q	259.6	3		L 119.0 F 21 T140.0	0.081	P _t P _e P _f	44.0	P _t P _v P _n	P _e = 15 x 0.433	в
9		THROUGH UNDER- GROUND TO CITY MAIN	q	259.6	3	E5 GV1 T15	L 50.0	С=150 ТҮРЕ'М'	P _t P _e P _f	61.7	P_t P_v P_n	$F = F_{40} \times 1.51 \times F_c$ $F_c = [2.981/3.068]^{4.87} = 0.869$ $F = 21 \times 1.51 \times 0.869$ F = 27.6	9
			q Q				L F T		P _t P _e P _f	66.4	P _t P _v P _n	· - <u>0</u> /.V	
			q Q				L F T		P _t P _e P _f		P _t P _v P _n	· .	

FIGURE A.14.3.2(c) Hydraulic Calculations.

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13–295

2002 Edition

INSTALLATION OF SPRINKLER SYSTEMS

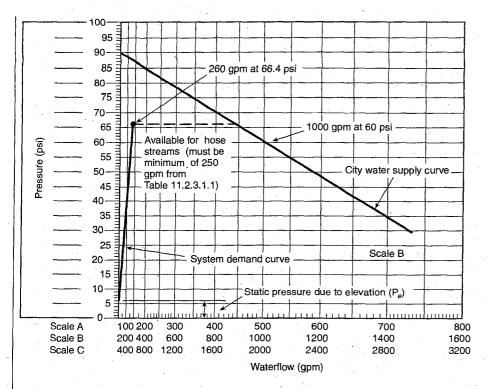


FIGURE A.14.3.2(d) Hydraulic Graph.

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Hydraulic Calculations

for Project Name: Sample Problem Location: , , Drawing Name: IC0099 LANL TWF Sample Problem Calculation Date: 8/29/2014 Design Remote Area Number: Occupancy Classification: Ordinary Group I Density: 0.150gpm/ft² Area of Application: 1500.00ft2 (Actual 1504.95ft2) Coverage per Sprinkler: 130.00ft² Type of sprinklers calculated: Upright No. of sprinklers calculated: 12 Type of System: Volume of Dry or PreAction System: N/A In-rack Demand: N/A gpm at Node: N/A Hose Streams: 250.0 at Node: 1 Type: Allowance at Source **Total Water Required** (including Hose Streams where applicable): From Water Supply at Node 1: 510.2 @ 67.2 Name of Contractor: WESTERN STATES FIRE PROTECTION Address: 1615 1/2 University Blvd. NE, Albuquerque, NM 87102 Phone Number: 226-668-8168 Name of designer: **BRAD VOKES** Authority Having Jurisdiction: Notes: Left: 58.7 Automatic peaking results Right: N/A

Summary Of Outflowing Devices

Devic	e	Actual Flow (gpm)	Minimum Flow (gpm)	K-Factor (K)	Pressure (psi)	
Sprinkler	101	19.5	19.5	5.6	12.1	
Sprinkler	102	20.8	19.5	5.6	13.7	
Sprinkler	103	21.9	19.5	5.6	15.4	
Sprinkler	104	23.1	19.5	5.6	17.1	
Sprinkler	105	19.8	19.5	5.6	12.5	
Sprinkler	106	21.0	19.5	5.6	14.1	
Sprinkler	107	22.3	19.5	5.6	15.8	
Sprinkler	108	23.5	19.5	5.6	17.6	
Sprinkler	109	20.2	19.5	5.6	13.0	
Sprinkler	110	21.5	19.5	5.6	14.7	
Sprinkler	111	22.7	19.5	5.6	16.5	
Sprinkler	112	23.9	19.5	5.6	18.3	

➡ Most Demanding Sprinkler Data

11 of <u>88</u>

Pipe Information

					-ihe ii	ntorma			
Node 1	Elev 1 (Foot)	K-Factor	Flow added this step (q)	Nominal ID	Fittings & Devices	Length (Foot)	C Factor	Total(Pt)	Notes Fitting/Device (Equivalent Length)
					Equiv.	Fitting (Foot)	Pf Friction	Elev(Pe)	Fixed Pressure Losses, when
Node 2	Elev 2 (Foot)		Total Flow (Q)	Actual ID	Length (Foot)	Total (Foot)	Loss Per Unit (psi)	Friction(Pf)	 applicable, are added directly to (Pf) and shown as a negative value.
101	15'-10¾	5.6	19.5	1	(See Notes)	13'-0	120	12.1	Sprinkler
					Notes)		0.124177		
102	15'-10¾		19.5	1.0		13'-0	0.124111	1.6	
102	15'-10¾	5.6	20.8	1¼	(See Notes)	13'-0	120	13.7	Sprinkler
103	15'-10¾		40.3	1.4			0.124856		_
100	10 10/4		10.0			13'-0		1.6	
103	15'-10¾	5.6	21.9	1½	(See Notes)	13'-0	120	15.4	Sprinkler
104	15'-10¾		62.2	1.6		13'-0	0.131829	1.7	-
104	15'-10¾	5.6	23.1	1½	(See	20'-6	120	17.1	
104	10-1074	5.0	20.1	172	Notes)	16'-0		0.4	Sprinkler
4	14'-10¾		85.3	1.6		36'-6	0.236658	8.6	2T(8'-0)
4	14'-10¾			2		10'-0	120	26.1	_
							0.070090		
6	14'-10¾		85.3	2.1		10'-0	0.070000	0.7	
6	14'-10¾		86.5	21⁄2		10'-0	120	26.8	Flow (q) from Route 2
8	14'-10¾		171.9	2.5		10'-0	0.107719	1.1	_
						70'-0	120	27.9	
8	14'-10¾		88.3	21/2			120	21.0	Flow (q) from Route 3
22	14'-10¾		260.2	2.5		70'-0	0.232013	16.2	_
22	14'-10¾			3	(See	118'-10¾	120	44.2	
					Notes)	30'-0		6.0	
3	1'-0		260.2	3.1		148'-10¾	0.080557	12.0	2E(7'-0), ALV(15'-0), GV(1'-0)
3	1'-0			3	(See	82'-2½	150	62.2	
1	1'-0		260.2	3.0	Notes)	82'-2½	0.061329 -	5.0	Water Supply
				<u> </u>		02-272			
			250.0					67.2	Hose Allowance At Source
1			510.2						 Total(Pt) Route 1
105	15'-10¾	5.6	19.8	1	(See Notes)	13'-0	120	12.5	••••• Route 2 ••••• Sprinkler
106	15'-10¾		19.8	1.0	110100)		0.127451		
100	13-1074		19.0	1.0		13'-0		1.7	

Node 1	Elev 1 (Foot)	K-Factor	Flow added this step (q)	Nominal ID	Fittings & Devices	Length (Foot) Fitting	C Factor Pf Friction	Total(Pt) Elev(Pe)	Notes Fitting/Device (Equivalent Length)
Node 2	Elev 2 (Foot)		Total Flow (Q)	Actual ID	Equiv. Length (Foot)	(Foot) Total (Foot)	Loss Per Unit (psi)	Friction(Pf)	Fixed Pressure Losses, when applicable, are added directly to (Pf) and shown as a negative value.
106	15'-10¾	5.6	21.0	1¼	(See Notes)	13'-0	120	14.1	- Sprinkler
107	15'-10¾		40.8	1.4		13'-0	0.128133	1.7	-
107	15'-10¾	5.6	22.3	1½	(See Notes)	13'-0	120	15.8	Sprinkler
108	15'-10¾		63.1	1.6		13'-0	0.135275	1.8	-
108	15'-10¾	5.6	23.5	1½	(See	20'-6	120	17.6	Sprinkler
6	14'-10¾		86.5	1.6	Notes)	16'-0 36'-6	0.242819	0.4	2T(8'-0)
								26.8	Total(Pt) Route 2
109	15'-10¾	5.6	20.2	1	(See Notes)	13'-0	120	13.0	••••• Route 3 ••••• Sprinkler
110	15'-10¾		20.2	1.0		13'-0	0.132478	1.7	_
110	15'-10¾	5.6	21.5	1¼	(See Notes)	13'-0	120	14.7	- Sprinkler
111	15'-10¾		41.7	1.4	,	13'-0	0.133163	1.7	-
111	15'-10¾	5.6	22.7	1½	(See Notes)	13'-0	120	16.5	Sprinkler
112	15'-10¾		64.4	1.6		13'-0	0.140564 -	1.8	-
112	15'-10¾	5.6	23.9	1½	(See	20'-6	120	18.3	- Sprinkler
8	14'-10¾		88.3	1.6	Notes)	16'-0	0.252274	0.4	2T(8'-0)
				-		36'-6		9.2	Total(Pt) Route 3

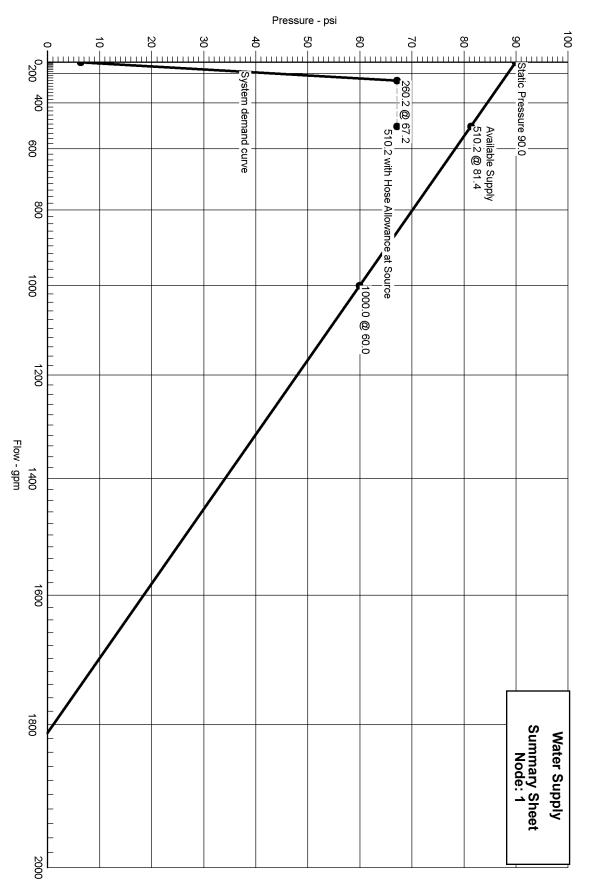
Ding Information

emole	Area Number:									Date
Equivale	nt Pipe Lengths of Valves and Fittings (C=120	only)		C Va	lue Multiplier					
	Actual Inside Diameter	۰ ^{4.87}	= Factor	-	Value Of C		100	130	140	150
(Schedule 40 Steel Pipe Inside Diameter)	- Facior	-	Multiplying F	actor	0.713	1.16	1.33	1.51
	Fittings Legend									
ALV	Alarm Valve	AngV	Angle Valve			b	Bushing			
BalV	Ball Valve	BFP	Backflow Preventer			BV	Butterfly	Valve		
С	Cross Flow Turn 90°	cplg	Coupling			Cr	Cross Ru	un		
CV	Check Valve	DelV	Deluge Valve			DPV	Dry Pipe	Valve		
Е	90° Elbow	EE	45° Elbow			Ee1	111/4° Elb	ow		
Ee2	22½° Elbow	f	Flow Device			fd	Flex Dro	р		
FDC	Fire Department Connection	fE	90° FireLock(TM) El	bow		fEE	45° FireL	.ock(TM)	Elbow	
flg	Flange	FN	Floating Node			fT	FireLock	(TM) Tee		
g	Gauge	GloV	Globe Valve			GV	Gate Val	ve		
Ho	Hose	Hose	Hose			ΗV	Hose Val	lve		
Hyd	Hydrant	LtE	Long Turn Elbow			mecT	Mechani	cal Tee		
Noz	Nozzle	P1	Pump In			P2	Pump Ou	ut		
PIV	Post Indicating Valve	PO	Pipe Outlet			PRV	Pressure	Reducir	ig Valve	
PrV	Pressure Relief Valve	red	Reducer/Adapter			S	Supply			
sCV	Swing Check Valve	Spr	Sprinkler			St	Strainer			
Т	Tee Flow Turn 90°	Tr	Tee Run			U	Union			
WirF	Wirsbo	WMV	Water Meter Valve			Z	Сар			



Job Name: Sample Problem Remote Area Number:

Date: 8/29/2014



ⓑ ◎ M.E.P.CAD, Inc.

AutoSPRINK® VR10 v10.0.56.0

8/29/2014 11:00:34AM

Page 2

Date	Time	User	Software	Computer	Computer S/N	Result
09/02/2014	8:00am	B. Vokes	MEPCAD VR10	HP 8760W	CNU2310PVX	ОК
09/03/2014	6:00am	B. Vokes	MEPCAD VR10	HP 8760W	CNU2310PVX	ОК
10/21/2014	8:00am	B. Vokes	MEPCAD VR10	HP 8760W	CNU2310PVX	ОК
10/23/2014	10:30am	B. Vokes	MEPCAD VR10	HP 8760W	CNU2310PVX	ОК
12/23/2014	6:00am	B. Vokes	MEPCAD VR10	HP 8760W	CNU2310PVX	ОК
12/24/2014	8:00am	B. Vokes	MEPCAD VR10	HP 8760W	CNU2310PVX	ОК
12/29/2014	6:30am	B. Vokes	MEPCAD VR11	HP 8760W	CNU2310PVX	ОК
01/30/2015	3:15pm	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
02/02/2015	8:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
06/01/2015	8:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
06/08/2015	8:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
06/16/2015	8:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
06/18/2015	8:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
06/19/2015	8:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
07/30/2015	7:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
07/31/2015	7:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
08/02/2015	11:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
08/03/2015	7:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
08/06/2015	7:00am	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК
11/15/2016	1:00pm	B. Vokes	MEPCAD VR11	HP 8760W	CNU231OPVX	ОК

Software Verification Log

Attachment B

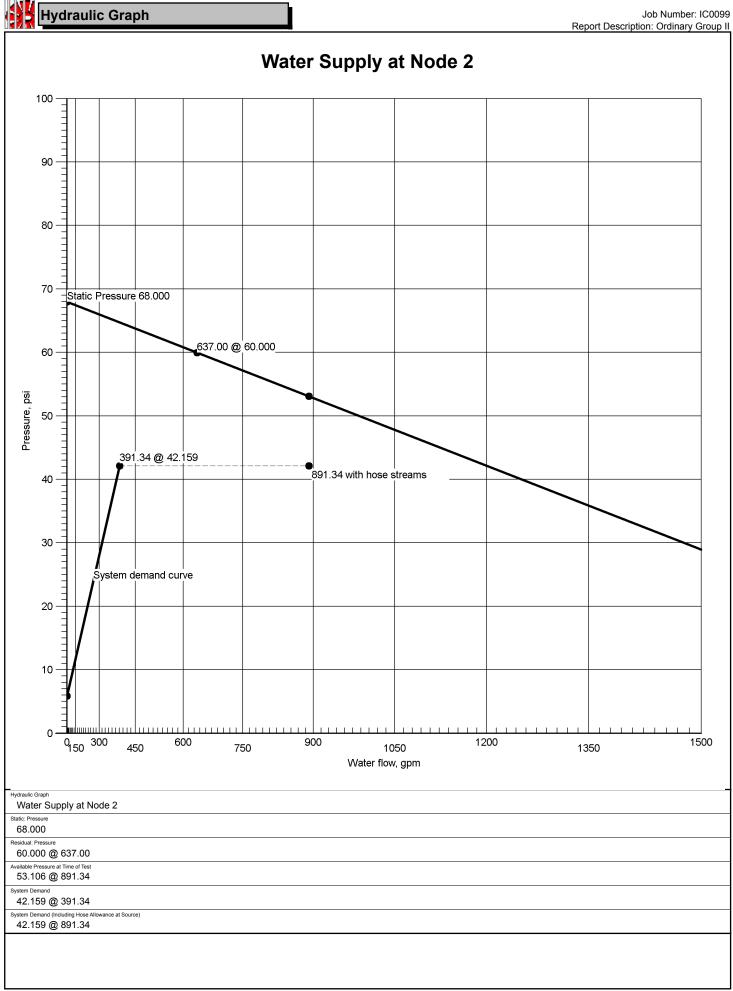
MEPCAD Hydraulic Calculations for Buildings 144, 147, 149, 150, 151, 152, 153 and 154

b b ICO0999 D Name: LANL TWF dress 1 LOS ALAMOS NATIONAL LABS dress 2	Design Engineer Brad Vokes Phone 1-226-668-8168
IC0099 Dame: LANL TWF dress 1 LOS ALAMOS NATIONAL LABS	Phone FAX
LANL TWF dress 1 LOS ALAMOS NATIONAL LABS	
LOS ALAMOS NATIONAL LABS	
	State Certification/License Number
dress 3	LANL FPDO Job Site/Building
atam	Building 144
rsity	Area of Application
0.200gpm/ft² st Demanding Sprinkler Data	1500.00ft² (Actual 1523.66ft²) Hose Streams
5.6 K-Factor 26.00 at 21.556	500.00
verage Per Sprinkler Varies	Number Of Sprinklers Calculated 15
stem Pressure Demand 42.159	System Flow Demand 391.34
al Demand 891.34 @ 42.159	Pressure Result +10.947 (20.6%)
ipplies	Check Point Gauges
<u>Node Name Flow(gpm) Hose Flow(gpm) Static(psi) Residual(psi)</u> 2 Water Supply 637.00 500.00 68.000 60.000	<u>Identifier</u> <u>Pressure(psi)</u> <u>K-Factor(K)</u> Flow(qpm)
0099 LANL TWF Building 144 OPS Rev 1	Water Supply at Node 2 (637.00, 500.00, 68.000, 60.000)
$\mathbf{f}_{\mathbf{r}}$	100 90 90 100 90 100 90 100 100

		inal y						Report [Description	n: Ordinary Group II
Job					Desire Fasies	-				
Job Number IC0099					Design Engine Brad V	okes				
Job Name: LANL TV	VF				State Certificatio	n/License Number				
Address 1 LOS AL/	AMOS NATIONAL LA	BS			AHJ LANL F	PDO				
Address 2					Job Site/Buildin Buildin					
Address 3					Drawing Name	LANL TWF Buildi		v 1		
System					Remote A			v 1		
Most Demanding 5.6 K-Fa	Sprinkler Data Ictor 26.00 at 21.55	6			Occupancy Ordina	ry Group II		Job Suffix		
Hose Allowance A 500.00	at Source				Density 0.200g	pm/ft²		Area of Application 1500.00ft ²	(Actual 15	523.66ft²)
Additional Hose S	upplies	E 1-				inklers Calculated		Coverage Per Sprinkle		,
<u>Node</u>		FIC	w(gpm)			Its: Pressure For Remote Area(s) Adjacent To Most Remote A			
Total Hose Stream 500.00	ns									
System Flow Den 391.34	nand		Total Water Required (Including 891.34	Hose Allowance)						
Maximum Pressu 0.000	re Unbalance In Loops				_					
Maximum Velocit	Above Ground Ween nodes 197 and	270			_					
Maximum Velocit	/ Under Ground									
5.59 bet	ween nodes 95 and 1		Volume capacity of Dry Pipes		_					
Supplies	242 Gallor	IS								
Supplies		Hose Flo	w Static	Residual	Flow	Available	Total Demand	Red	quired	Safety Margin
Node	Name	(gpm)	(psi)	(psi) @	(gpm)	(psi) @	(gpm)	()	psi)	(psi)
2	Water Supply	500.00	68.000	60.000	637.00	53.106	891.34	42	.159	10.947
<u> </u>										
Contractor	Contractor Numb	er			Contact Na				Contact Title	
Name of Contrac					Phone	D VOKES			DESIG Extension	NER
WESTE Address 1	RN STATES FIRE PR	OTECTION			226-0	668-8168				
5200 PA	SADENA AVE NE, SI	JITE A			505-	384-1863				
Address 2						D.VOKES@WSFF	US			
Address 3 ALBUQU	JERQUE, NM 87113				Web-Site					

Hydraulic Summary

Job Number: IC0099



Summary Of Outflowing Devices

		-				Report Descriptior	1: Ordinary Group
Device	e	Actual Flow (gpm)	Minimum Flow (gpm)	K-Factor (K)	Pressure (psi)		Coverage (Foot)
Sprinkler	439	26.04	26.00	5.6	21.616		130.00ft ²
🔿 Sprinkler	448	26.00	26.00	5.6	21.556		130.00ft ²
Sprinkler	539	25.63	24.00	5.6	20.950		120.00sqft
Sprinkler	548	25.42	24.00	5.6	20.598		120.00sqft
Sprinkler	555	26.39	26.00	5.6	22.205		130.00ft ²
Sprinkler	556	26.19	26.00	5.6	21.865		130.00ft ²
Sprinkler	557	26.16	26.00	5.6	21.814		130.00ft ²
Sprinkler	559	26.04	19.20	5.6	21.623		96.00sqft
Sprinkler	561	26.26	24.00	5.6	21.991		120.00sqft
Sprinkler	562	26.20	24.00	5.6	21.897		120.00sqft
Sprinkler	564	26.47	24.00	5.6	22.340		120.00sqft
Sprinkler	567	25.93	19.20	5.6	21.436		96.00sqft
Sprinkler	571	25.87	24.00	5.6	21.346		120.00sqft
Sprinkler	572	26.22	24.00	5.6	21.925		120.00sqf
Sprinkler	574	26.53	24.00	5.6	22.444		120.00sqf

➡ Most Demanding Sprinkler Data

Pipe Type	Diameter	Flow	Velocity	нмс	Friction Loss	Length	Pres	sure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length		nmary
Upstream						Total Length		
••••• Route 1 •								
BL	1.3800	26.00	5.58	120	0.055609	5'-10½		
448	9'-01/2	26.00	5.6	21.556	Sprinkler,		1	-1.912
308	13'-5½	47.74	1.50	20.471	E(3'-0), mecT(6'-0) 0.023897	14'-10½		0.405
CM 308	2.0670 13'-5½	<u>47.71</u> 21.71	4.56	<u>120</u> 20.471	Flow (q) from Route 6	6-11		0.165 0.000
307	13'-5½	21.71		20.636	1 low (q) from Route o	6'-11	1	0.000
CM	2.0670	73.74	7.05	120	0.053486	51'-6		3.424
307	13'-5½	26.04	7.05	20.636	Flow (q) from Route 2			0.438
295	12'-5½	20.04		20.030	fE(3'-6), mecT(9'-0)	64'-0	1	0.430
CM	4.0260	310.90	7.84	120	0.029803			0.150
295	12'-5½	237.15	7.04	24.497	Flow (q) from Route 3		Pr	0.150
233	12'-5½	237.13		24.647		5'-0	1	
CM	4.0260	391.34	9.86	120	0.045618	14'-10½		1 400
278	12'-5½	80.44	9.00	24.647	Flow (q) from Route 7			0.000
197	12'-5½	00.44		26.055	fT(16'-0)	30'-10½		0.000
CM	6.0650	391.34	4.35	120	0.006201	14'-3½		6.659
197	12'-5½	391.34	4.55	26.055	0.000201			7.352
106	-4'-6			40.067	fE(10'-0), ALV, BFP(-6.378),	45'-3½		7.552
100				TU.007	E(14'-0), EE(7'-0)	+0-0/2	FV.	
UG	5.3490	391.34	5.59	150	0.007567	122'-2	Df	1.216
106	-4'-6	591.34	0.09	40.067	0.001001			0.000
95	-4-6 -4'-6			41.282	E(11'-5½), PIV(2'-5½), T(24'-7)	160'-8		0.000
95 UG	6.9780	391.34	3.28	150	0.002073			0.866
95	<u> </u>	391.34	3.20	41.282	0.002075		Pf	0.000
95 1	-4 -0 -4'-6			41.282 42.148	3PIV(3'-1½)	417'-9		
UG		204.24	2.20		0.002095			0.011
1	<u>6.9630</u> -4'-6	391.34	3.30	<u>150</u> 42.148	0.002095	5-1	PT	0.011
2	-4-0 -4'-6				Water Supply	5'-1	1	
2	-4 -0	500.00		42.159	Hose Allowance At Source	5-1	PV	
		500.00			Hose Allowance At Source			
2		891.34						
••••• Route 2 •								
BL	1.3800	26.04	5.58	120	0.055750	7' 0	Df	0.933
439	9'-01/2	26.04	5.6	21.616	Sprinkler,			-1.912
307	13'-5½	20.04	5.0	20.636	E(3'-0), mecT(6'-0)	16'-9		-1.912
••••• Route 3 •				20.000		10 0	I V	
BL	1.3800	26.16	5.61	120	0.056224	A' 1	Df	0.566
557	9'-01/2	26.16	5.6	21.814	Sprinkler,		1	-1.766
345	13'-1½	20.10	0.0	20.614	mecT(6'-0)	10'-1	1	-1.700
<u>CM</u>	2.0670	27.02	2.58	120	0.008348			0.035
345	13'-1½	0.87	2.30	20.614	Flow (q) from Route 16			-0.012
361	13'-2	0.07		20.637		4'-2		-0.012
CM	2.0670	22.60	2.16	120	0.006001			0.056
361	13'-2	22.00	2.10	20.637	0.000001			0.030
359	13-2 13'-1½			20.837 20.705		0' 4	Pe Pv	0.011
<u>359</u> CM		48.79	4.66	120	0.024909			0.349
359	2.0670 13'-1½	26.19	4.00	20.705	Flow (q) from Route 4	14-0		0.349
359 357	13-1/2	20.19		20.705 21.053		14'-0		0.000
		75.18	7.19	120	0.055426			2.555
CM 357	2.0670		1.19		Flow (q) from Route 5			2.555 0.292
357 350	13'-1½ 12'-5½	26.39		21.053 23.900	fE(3'-6), mecT(9'-0)	46'-1		0.292
 CM	4.0260	237.15	5.98	120	0.018060	19'-5½		0 507
			5.98	23.900	Flow (q) from Route 8	19'-5½ 13'-7		0.597
350 295	12'-5½ 12'-5½	161.97		23.900 24.497	2fE(6'-9 ¹ / ₂)	13-7 33'-0½		
295	12'-5½			27.731	LIL(V-072)	33-0/2	IL.A.	
		26.40	E 00	120	0.056344	01.444	P (0.500
BL	1.3800	26.19	5.62	120	Sprinkler,	3'-11½		
556 350	9'-2 13'-1½	26.19	5.6	21.865	mecT(6'-0)			-1.722
359				20.705		9'-11½	PV	
••••• Route 5 •		00.00	E 00	100	0.057156	0.444	-	0
BL	1.3800	26.39	5.66	120		3'-11½	1	
555 357	9'-2 13'-1½	26.39	5.6	22.205 21.053	Sprinkler, mecT(6'-0)	6'-0 9'-11½		-1.722
357				21.000		9-11/2	F V	
	1.3800	25.42	5.45	120	0.053318	10' 10	Df	1.697
	9'-0½	25.42	5.6	20.598	Sprinkler,			-1.912
BL		20.42	5.0	20.382	3E(3'-0), T(6'-0), mecT(6'-0)	31'-10	1	-1.314
BL 548					$O_{-}(O_{-}O_{i}), I(O_{-}O_{i}), IIICOI(O_{-}O_{i})$	1 31-10	ILL A	
BL 548 310	13'-5½	21 71	2.00		0.005568	4 = 1 4 4	Df	0 000
BL 548 310 CM	13'-5½ 2.0670	21.71	2.08	120	0.005568	15'-11	1	0.089
BL 548 310	13'-5½	21.71	2.08		0.005568	15'-11	Ре	0.089

Pipe Type	Diameter	Flow	Velocity	HWC	Friction Loss	Length	Press	sure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length	Sumr	
Upstream						Total Length		
L	1.3800	25.63	5.50	120	0.054161	9'-10		
539	9'-01⁄2	25.63	5.6	20.950	Sprinkler,			-1.912
310	13'-5½			20.382	3E(3'-0), mecT(6'-0)	24'-10		
М	2.0670	29.34	2.81	120	0.009721		Pf (0.213
310	13'-5½			20.382		12'-6	Pe	0.438
313	12'-5½			21.033	fE(3'-6), mecT(9'-0)	21'-11		
Μ	4.0260	80.44	2.03	120	0.002444	10'-3	Pf (0.025
313	12'-5½	51.10		21.033	Flow (q) from Route 14		Pe (0.000
269	12'-5½			21.058		10'-3	Ρv	
M	4.0260	50.58	1.27	120	0.001036	8'-6½	Pf (0.018
269	12'-5½			21.058		9'-0		-0.000
218	12'-5½			21.076	mecT(9'-0)	17'-6½		
M	4.0260	24.34	0.61	120	0.000268	9'-8½		0.007
218	12'-5½	24.04	0.01	21.076	mecT(9'-0)	18'-0		
157	12'-5½			21.084	mecT(9'-0)	27'-8½		0.000
		24.34	0.00	120	0.006880	72'-8		0.582
M	2.0670	24.34	2.33		0.000880			
157	12'-5½			21.084				-0.897
42	14'-6½			20.769	fT(8'-6), fE(3'-6)	84'-8		
M	2.0670	50.58	4.84	120	0.026628	8'-6½		0.228
42	14'-6½	26.24		20.769	Flow (q) from Route 20			0.154
252	14'-2			21.151		8'-6½		
М	2.0670	80.44	7.69	120	0.062819	27'-10		2.753
252	14'-2	29.86		21.151	Flow (q) from Route 19	16'-0		0.743
278	12'-5½			24.647	2fE(3'-6), mecT(9'-0)	43'-10		
••••• Route 8 •								
L	1.3800	25.87	5.55	120	0.055108	4'-5½	Df	1.239
571	8'-11½	25.87	5.6	21.346	Sprinkler,			-1.508
398		20.07	0.0	21.077	4E(3'-0), mecT(6'-0)	22'-5½		-1.500
	12'-5½	50.05	5.00		0.032519			0.400
M	2.0670	56.35	5.39	120		12'-5½		0.406
398	12'-5½	30.48		21.077	Flow (q) from Route 10			-0.001
397	12'-5½			21.482		12'-5½		
M	2.0670	82.88	7.92	120	0.066390	29'-5		
397	12'-5½	26.53		21.482	Flow (q) from Route 13	6'-0	Pe ·	-0.002
392	12'-5½			23.831	mecT(6'-0)	35'-5	Ρv	
М	4.0260	82.88	2.09	120	0.002583	10'-0	Pf (0.026
392	12'-5½			23.831			Pe	
376	12'-5½			23.857		10'-0		
M	4.0260	161.97	4.08	120	0.008921	4'-10		0.043
376	12'-5½	79.09	4.00	23.857	Flow (q) from Route 9		Pe	0.040
350	12'-5½	13.03		23.900		4'-10		
••••• Route 9 •				23.900		4-10	FV	
				(00	0.050.100			
L	1.3800	26.20	5.62	120	0.056422	3'-10½		0.558
562	8'-11½	26.20	5.6	21.897	Sprinkler,			-1.687
369	12'-10½			20.768	mecT(6'-0)	9'-10½	Pv	
Μ	2.0670	26.36	2.52	120	0.007976	12'-0	Pf (0.096
369	12'-10½	0.16		20.768	Flow (q) from Route 18		Pe ·	-0.002
371	12'-10½			20.862		12'-0	Pv	
M	2.0670	52.62	5.03	120	0.028650	12'-5½	Pf (0 357
371	12'-10½	26.26	0.00	20.862	Flow (g) from Route 11			-0.002
372	12'-101/2			21.217		12'-5½		
:M	2.0670	79.09	7.56	120	0.060881	29'-7		2.459
372		26.47	7.00		Flow (g) from Route 12			
	12'-10½	20.47		21.217		10'-9½		0.101
376	12'-5½			23.857	fEE(1'-9½), mecT(9'-0)	40'-4½	PV	
••••• Route 10						1		
L	1.3800	26.22	5.62	120	0.056487	3'-5½		
572	8'-11½	26.22	5.6	21.925	Sprinkler,	6'-0	Pe	-1.507
400	12'-5½			20.953	mecT(6'-0)	9'-5½	Pv	
М	2.0670	30.48	2.91	120	0.010432	12'-0		0.125
400	12'-5½	4.26		20.953	Flow (q) from Route 17	•		-0.001
398	12'-5½			21.077	· • ·	12'-0		
••••• Route 11						0		
	1.3800	26.26	5.63	120	0.056645	3'-11	Df (0.561
L								
561	8'-11½	26.26	5.6	21.991	Sprinkler,			-1.689
371	12'-10½			20.862	mecT(6'-0)	9'-11	PV	
••••• Route 12	••••							
L	1.3800	26.47	5.68	120	0.057476	3'-11	Pf (0.569
564	8'-11½	26.47	5.6	22.340	Sprinkler,	6'-0	Pe	-1.691
372	12'-10½			21.217	mecT(6'-0)	9'-11		
••••• Route 13					. /			
	1.3800	26.53	5.69	120	0.057723	0 i C	Df	0.547
L574	8'-11½	26.53	5.6	22.444	Sprinkler,			0.547 -1.508
J 1 T		20.00	5.0		•	9'-6		-1.500
397	12'-5½			21.482	mecT(6'-0)			

Pipe Type Downstream	Diameter Elevation	Flow Discharge	Velocity K-Factor	HWC Pt	Pn	Friction Lo Fittings	SS		Length Eq. Length		sure mary
Upstream	4 0000	05.00		100		0.055323			Total Length	-	4 000
BL	1.3800 8'-11½	25.93	<u>5.56</u> 5.6	<u>120</u> 21.436		Sprinkler,				1	1.088
		25.93	0.0				aT/6' 0)			-	-1.511
387	12'-5½	05.00	0.05	21.014		E(3'-0), me 0.000301	01(0-0)		19'-8		0.004
CM	4.0260	25.93	0.65	120		0.000301			12'-5½		
387	12'-5½			21.014					401 51/	-	-0.000
349	12'-5½	54.40	1.00	21.018		0.001056			12'-5½		0.045
CM	4.0260	51.10	1.29	120			m Route 15		14'-3½		
349	12'-5½	25.18		21.018		Flow (q) fro	m Route 15			-	0.000
313	12'-5½			21.033					14'-3½	Pv	
••••• Route 1						0.055300					
BL	1.3800	26.04	5.59	120		0.055769					0.757
559	9'-0½	26.04	5.6	21.623		Sprinkler,	- T(0) 0				-1.766
346	13'-1½			20.614		E(3'-0), me	CI(6'-0)		13'-7	_	
CM	2.0670	25.18	2.41	120		0.007324				1	0.112
346	13'-1½			20.614							0.292
349	12'-5½			21.018		fEE(1'-9½),	, mecT(6'-0)		15'-3½	Pv	
••••• Route 1											
СМ	2.0670	0.87	0.08	120		0.000014			8'-11½		0.000
346	13'-1½			20.614						Pe	
345	13'-1½			20.614					8'-11½	Ρv	
🕶 • • • • Route 1	7••••										
СМ	2.0670	4.42	0.42	120		0.000293					0.004
361	13'-2			20.637		fT(8'-6)				-	0.127
367	12'-10½			20.768					13'-4		
СМ	2.0670	4.26	0.41	120		0.000274			12'-4½		
367	12'-10½			20.768						-	0.180
400	12'-5½			20.953		fE(3'-6)			15'-10½	Ρv	
🕶 • • • • Route 1	8 • • • •										
СМ	2.0670	0.16	0.02	120		0.000001					0.000
367	12'-10½			20.768		fT(8'-6)					-0.000
369	12'-10½			20.768					10'-10½	Pv	
••••• Route 1	9 • • • •										
СМ	2.0670	29.86	2.85	120		0.010043			62'-2½	Pf	0.836
269	12'-5½			21.058		mecT(9'-0)					-0.743
252	14'-2			21.151		fE(3'-6), fT((8'-6)		83'-21⁄2	Ρv	
Route 2	0 • • • • •										
СМ	2.0670	26.24	2.51	120		0.007909			62'-7	Pf	0.590
218	12'-5½			21.076					12'-0	Pe	-0.897
42	14'-6½			20.769		fE(3'-6), fT((8'-6)		74'-7	Pv	
	engths of Valves and	l Fittings (C=120 on	ly)		C Valu	e Multiplier					
			4.87			010	400	400	4.40		450
(Actual Inside)	actor	Value		100	130	140		150
I So	chedule 40 Steel Pig	be Inside Diameter	1		Multip	lying Factor	0.713	1.16	1.33	1	1.51

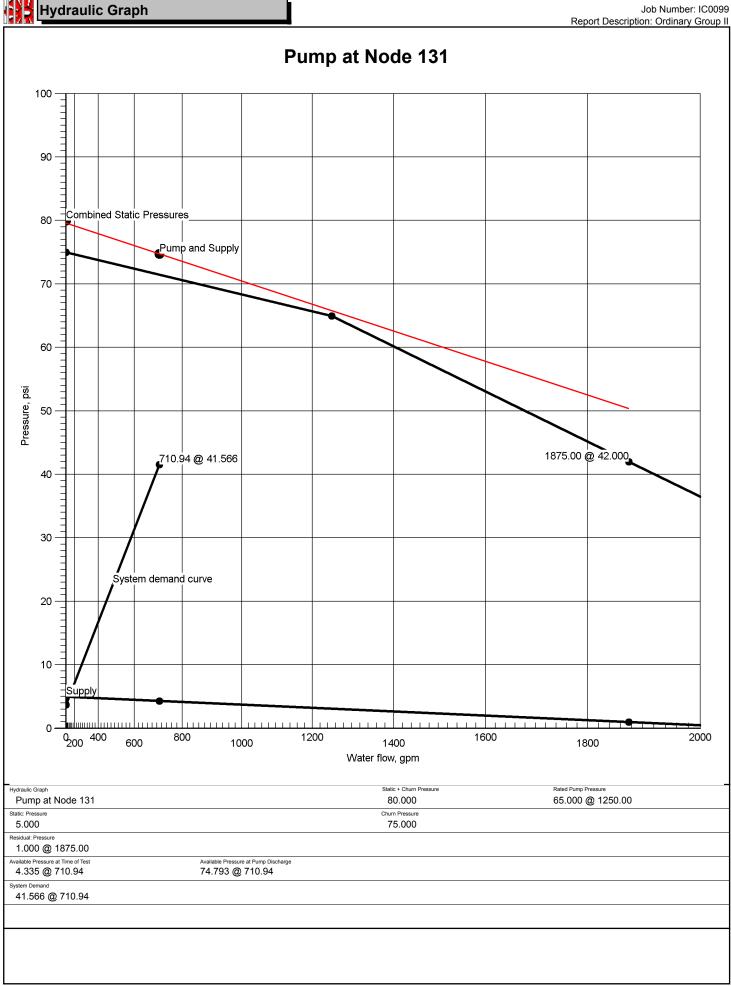


Job Number: IC0099

ipe Type Diamet	er Flow	Velocity HWC		Friction Loss		Length	Pressure
Downstream Elevati Jpstream	on Discharge	K-Factor Pt	Pn	Fittings		Eq. Length Total Length	Summary
Pipe Type Legend		Units Legen	d			Fittings Legen	d
 Arm-Over Branch Line Cross Main Drop Dynamic Feed Main Feed Riser Miscellaneous Outrigger Riser Nipple Sprig Stand Pipe Underground 	Pt Total p Pn Norma Pf Pressu Pe Pressu	ot h-Williams Constant pressure at a point in a pi al pressure at a point in a ure loss due to friction be ure due to elevation differ ty pressure at a point in a	pipe tween points rence betwee		ALV AngV b BaIV BFP BV C cplg Cr CV DPV E EE Ee1 Ee2 f fd FDC fE fEE flg FN fT g GloV GV Ho Hose HV Hyd LtE mecT Noz P1 P2 PIV PO PRV PRV PO PRV PV red S SCV Spr St T Tr U WirF WMV Z	Alarm Valve Angle Valve Bushing Ball Valve Backflow Prevente Butterfly Valve Cross Flow Turn 9 Coupling Cross Run Check Valve Deluge Valve Dry Pipe Valve 90° Elbow 45° Elbow 11¼° Elbow 22½° Elbow Flow Device Flex Drop Fire Department C 90° FireLock(TM) 1 45° FireLock(TM) 1 45° FireLock(TM) 1 Flange Floating Node FireLock(TM) 1 Elange Globe Valve Gate Valve Hose Hose Hose Hose Valve Hose Hose Valve Hose Hose Hose Valve Hose Hose Hose Valve Hose Hose Hose Valve Hose Hose Hose Hose Hose Hose Hose Hos	ornection Elbow Elbow g Valve lve

Hydraulic Overview							
b Number				Design Engineer			
C0099 Name:				Brad Vokes	F	AX	
LANL TWF				1-226-668-8168			
dress 1 LOS ALAMOS NATIONAL LABS				State Certification/License Number			
dress 2				AHJ LANL FPDO			
dress 3				Job Site/Building			
stem				Building 147			
nsity				Area of Application			
D.200gpm/ft ² st Demanding Sprinkler Data				610.00ft ² (Actual 617 Hose Streams	′.65ft²)		
5.6 K-Factor 23.47 at 17.568				500.00			
verage Per Sprinkler Varies				Number Of Sprinklers Calculated			
				System Flow Demand 710.94			
al Demand 710.94							
pplies				Check Point Gauges			
	Hose Flow(gpm)	Static(psi)	Residual(psi)	Identifier	Pressure(psi)	K-Factor(K)	Flow(gpm)
62 Tank Supply 1875.00		5.000	1.000	_			
131 1250.00	Pump	75.000	65.000				
Pumps: Static = Churn (Pressure @ Zero Flow)							
Pumps: Static = Churn (Pressure @ Zero Flow) 0099 LANL TWF Rev 3				Tank Supply at Node 6	2 (1875.00, 0.00, 5.00	00, 1.000)	

(ydraulic Sumr	mary							Re		bb Number: IC0099 : Ordinary Group II	
Job									1.0			
Job Number IC0099						Design Enginee Brad Vo						
Job Name: LANL TV	WE					State Certification	n/License Number					
Address 1	AMOS NATIONAL LAI	BS				AHJ LANL F	PDO					
Address 2						Job Site/Buildin Building						
Address 3						Drawing Name	-					
System						Remote A	LANL TWF Rev	/ 3				
Most Demanding	Sprinkler Data actor 23.47 at 17.568	<u> </u>			_	Occupancy Job Suffix Job Suffix						
Hose Allowance A)				Density A			Area of Appli			
Additional Hose S	Supplies					0.200gpm/ft² 610.00ft² (Actual 617.65ft²) Number Of Sprinklers Calculated Coverage Per Sprinkler					65ft²)	
Node			<u>((gpm)</u>			8			Var			
Hydrant	At Node 44	50	0.00			AutoPeak Resu	ts: Pressure For Remote Ar	ea(s) Adjacent To Most Rem	ote Area			
Total Hose Stream 500.00 System Flow Den 710.94	mand	1	otal Water Required (Including H 710.94	iose Allowance)		-						
Maximum Velocity 20.17 be	y Above Ground etween nodes 985 and	951										
Maximum Velocity 7.14 bet	y Under Ground ween nodes 41 and 4	4										
Volume capacity of			/olume capacity of Dry Pipes			-						
Supplies												
		Hose Flow	Static	Residual		Flow	Available	Total Dema	nd	Required	Safety Margin	
Node	Name	(gpm)	(psi)	(psi)		(gpm)	(psi)	(gpiii)		(psi)	(psi)	
62 131	Tank Supply	Pump	5.000 75.000	1.000 65.000		1875.00 1250.00	4.335 74.793	710.94		0.000 41.566	33.227 33.227	
Pumps: Sta	atic = Churn (Pressure @ Zer	o Flow)										
Contractor												
	Contractor Number	er				Contact Nar				Contact Title DESIGN	JER	
Name of Contract		OTECTION				Phone	68-8168			Extension		
Address 1 5200 PA	SADENA AVE NE, SU	JITEA			-	FAX 505-8	84-1863					
Address 2	, 00					E-mail						
Address 3						Web-Site	D.VOKES@WSI	-4.05				
ALBUQU	JERQUE, NM 87113											





Summary Of Outflowing Devices

Job Number: IC0099 Report Description: Ordinary Group II

Devic	e	Actual Flow (gpm)	Minimum Flow (gpm)	K-Factor (K)	Pressure (psi)	Coverage (Foot)
Hydrant	44	500.00	500.00	267.26	37.964	
Sprinkler	1347	25.97	20.00	5.6	21.502	100.00ft ²
Sprinkler	1348	26.37	16.80	5.6	22.169	84.00sqft
Sprinkler	1349	27.15	16.80	5.6	23.500	84.00sqft
Sprinkler	1350	28.02	16.80	5.6	25.036	84.00sqft
Sprinkler	1352	25.07	16.80	5.6	20.042	84.00sqft
Sprinkler	1353	25.92	16.80	5.6	21.426	84.00sqft
Sprinkler	1354	28.98	16.80	5.6	26.775	84.00sqft
Sprinkler	1697	23.47	23.47	5.6	17.568	117.35sqf

➡ Most Demanding Sprinkler Data

Pipe Type	Diameter	Flow	Velocity	нис	Friction Loss	Length	Pres	sure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length Total Length		nmary
UpstreamRoute 1.						Total Length	ļ	
	1.0490	23.47	8.71	120	0.174982	11'-8½	Df	1 224
1697	9'-10	23.47	5.6	17.568	Sprinkler,			-0.243
824	10'-5	20.47	0.0	21.559	2E(2'-0), PO(8'-6)	24'-2½		0.240
о <u>г</u>	1.6100	49.44	7.79	120	0.086188			0.610
824	10'-5	25.97	1.15	21.559	Flow (q) from Route 2		Pe	0.010
1348	10-5	20.01		22.169		7'-1		
CM	1.6100	75.81	11.95	120	0.190051		_	1.330
1348	10'-5	26.37	5.6	22.169	Sprinkler		PI	1.550
		20.37	5.0		Sphinkler	7' 0		
1349	10'-5	100.05	40.00	23.500	0.224000	7'-0		0.000
CM	1.6100	102.95	16.22	120	0.334809			3.283
1349	10'-5	27.15	5.6	23.500	Sprinkler,			0.000
829	10'-5			26.783	mecT(5'-0)	9'-9½	_	
CM	2.0670	130.97	12.52	120	0.154787	10'-3		1.589
829	10'-5	28.02		26.783	Flow (q) from Route 4			0.262
951	9'-9½			28.634		10'-3		
M	2.0670	210.94	20.17	120	0.373807			7.404
951	9'-91⁄2	50.99		28.634	Flow (q) from Route 3	13'-6	Pe	0.092
985	9'-7			36.129	fE(3'-6), PO(10'-0)	19'-9½	Ρv	
CM	4.0260	210.94	5.32	120	0.014542	14'-9½		0.733
985	9'-7			36.129				3.395
119	1'-9			40.257	ALV, PIV(2'-0), 2fE(6'-9½), f(-0.000), T(20'-0)	50'-5		
JG	4.3000	210.94	4.66	120	0.010553	 ∩_∩	Pf	0.582
119	1'-9	L 10.07	1.00	40.257		55'-1½		
74	1'-9			40.843	T(27'-6½), C(27'-6½)	55'-1½		2.000
	7.9810	710.94	4.56	120	0.004915	7'-1		0.723
⁻ M 74	<u>7.9810</u> 1'-9	500.00	4.00	40.843	Flow (q) from Route 6			0.723
131	1-9 1'-9	500.00		41.566	2T(35'-0), LtE(13'-0), BV(12'-0), CV(45'-0)	140-0		0.000
			Valacity		01(40 0)		-	
2000 Pump		710.94	Velocity	41.566	Rating: 65.000 @ 1250.00	_		
131			4.50					
129		Q=710.94	4.56	-29.913	Churn Pressure: 75.000			
-M	7.9810	710.94	4.56	120	0.004915			0.285
129	1'-9			-29.913				-1.409
124	5'-0			-31.037	GV(4'-0), LtE(13'-0), T(35'-0)	58'-0		
M	11.9380	710.94	2.04	120	0.000692			0.194
124 62	5'-0 0'-6			-31.037 -28.892	sCV(65'-0), GV(6'-0), 7LtE(18'-0),	197'-0 280'-8		1.951
		0.00			S Hose Allowance At Source			
		= 40.04				-		
62		710.94						
••••• Route 2 •					0.000100			
CM	1.6100	25.97	4.09	120	0.026188	2'-2		0.057
1347	10'-5	25.97	5.6	21.502	Sprinkler		Pe	
824	10'-5			21.559		2'-2	Pv	
• • • • • Route 3 •	• • • • •							
BL	1.0490	25.07	9.31	120	0.197661	7'-0	Pf	1.384
1352	9'-91⁄2	25.07	5.6	20.042	Sprinkler		Pe	
1353	9'-9½			21.426		7'-0	Ρv	
BL	1.0490	50.99	18.93	120	0.735102	4'-9½	Pf	7.208
1353	9'-9½	25.92	5.6	21.426	Sprinkler,	5'-0	Pe	0.000
951	9'-91⁄2			28.634	mecT(5'-0)	9'-9½		
••••• Route 4 •								
BL	1.0490	28.02	10.40	120	0.242827	2'-21%	Pf	1.747
1350	10'-5	28.02	5.6	25.036	Sprinkler,			0.000
829	10-5		0.0	26.783	mecT(5'-0)	7'-2½		2.000
••••• Route 5 •						. 2/2		
L	1.0490	28.98	10.76	120	0.258391	01.01/	Df	1.859
					Sprinkler,			0.000
1354	9'-9½	28.98	5.6	26.775	mecT(5'-0)	5'-0 7'-2½		0.000
951	9'-9½			28.634		1-2/2	FV	
••••• Route 6 •		500.00	7.44	150	0.044047			4.65
JG	5.3480	500.00	7.14	150	0.011917			1.081
44	2'-6	500.00		37.964	Hydrant,			3.035
41	-4'-6			42.079	E(14'-0), CV(32'-0), T(30'-0)	90'-8		
IG	6.9630	500.00	4.21	150	0.003296	73'-5	Pf	0.301
41	-4'-6			42.079		18'-0	Pe	
52	-4'-6			42.381	2EE(9'-0)	91'-5		
JG	6.9630	289.40	2.44	150	0.001199			0.011
52	-4'-6			42.381		4'-0		
	-4'-6			42.391	PIV(4'-0)	8'-11	1	
53				H/ UM				

ipe Type Downstream Upstream	Diameter Elevation	Flow Discharge	Velocity K-Factor	HWC Pt	Pn	Friction Los Fittings	SS		Length Eq. Length Total Length		ssure nmary
G	6.4700	289.40	2.82	120		0.002590				Pf	0.003
53	-4'-6	200.10	2.02	42.391					10	Pe	0.000
54	-4'-6			42.394					1'-0	Ρv	
G	6.9630	289.40	2.44	150		0.001199			223'-3	Pf	0.316
54	-4'-6			42.394					40'-0	Pe	
69	-4'-6			42.709		4EE(9'-0), P	PIV(4'-0)		263'-3	Ρv	
IG	6.4700	289.40	2.82	120		0.002590			1'-0	Pf	0.003
69	-4'-6			42.709						Pe	
70	-4'-6			42.712					1'-0	Ρv	
G	6.9630	289.40	2.44	150		0.001199			3'-11	Pf	0.005
70	-4'-6			42.712						Pe	
71	-4'-6			42.717					3'-11	Ρv	
IG	6.9630	500.00	4.21	150		0.003296					0.029
71	-4'-6	210.60		42.717		Flow (q) fror	m Route 7		4'-0	Pe	
72	-4'-6			42.746		PIV(4'-0)			8'-9½	Ρv	
G	6.4700	500.00	4.88	120		0.007123			1'-0	Pf	0.007
72	-4'-6			42.746						Pe	
73	-4'-6			42.753					1'-0		
IG	6.9630	500.00	4.21	150		0.003296			165'-8	Pf	0.751
73	-4'-6			42.753							0.000
75	-4'-6			43.503		EE(9'-0), T(3	35'-0), E(18'-0)		227'-8	Pv	
M	7.9810	500.00	3.21	120		0.002563					0.049
75	-4'-6			43.503							-2.71
74	1'-9			40.843		LtE(13'-0)			19'-3		
••••• Route 7 •										1	
IG	6.9630	210.60	1.77	150		0.000666			63'-0	Pf	0.045
24	-4'-6	210.00	1.1.1	42.526					4'-0		0.010
25	-4'-6			42.571		PIV(4'-0)			67'-0		
IG	6.4700	210.60	2.06	120		0.001439					0.001
25	-4'-6	210.00	2.00	42.571		0.001100			10	Pe	0.001
26	-4'-6			42.572					1'-0		
1G	6.9630	210.60	1.77	150		0.000666					0.106
26	-4'-6	210.00	1.77	42.572		0.000000			39'-0		0.100
61	-4'-6			42.678		T(35'-0), PI\	/(4'-0)		158'-6		
JG	6.4700	210.60	2.06	120		0.001439	/(+ 0)				0.001
61	-4'-6	210.00	2.00	42.678		0.001400			1-0	Pr	0.001
63	-4'-6			42.679					1'-0		
JG	6.9630	210.60	1.77	150		0.000666					0.038
63	-4'-6	210.00	1.77	42.679		0.000000			35'-0	1	0.036
71	-4'-6			42.079		T(35'-0)			56'-6		
••••• Route 8 •				42.717		1(33-0)			50-0	PV	
		010.00	2.00	100		0.001439			41.0	D (0.001
IG	6.4700	210.60	2.06	120		0.001439			1-0		0.001
51	-4'-6			42.410					41.0	Pe	
50	-4'-6	010.00	4 77	42.411		0.000000			1'-0		0.070
JG	6.9630	210.60	1.77	150		0.000666			94'-5½		0.072
50	-4'-6			42.411					13'-0		
18	-4'-6	040.00	0.00	42.483		EE(9'-0), PI	v(4-U)		107'-5½		0.00
IG	6.4700	210.60	2.06	120		0.001439			1'-0		0.001
18	-4'-6			42.483						Pe	
19	-4'-6			42.484		0.000000			1'-0		
G	6.9630	210.60	1.77	150		0.000666					0.041
19	-4'-6			42.484		DN (111 A)			4'-0		
22	-4'-6			42.525		PIV(4'-0)			61'-0	_	
G	6.4700	210.60	2.06	120		0.001439			1'-0		0.001
22	-4'-6			42.525						Pe	
24	-4'-6			42.526					1'-0	Ρv	
••••• Route 9 •	••••										
G	6.9630	210.60	1.77	150		0.000666					0.029
52	-4'-6			42.381		T(35'-0)			39'-0		
51	-4'-6			42.410		PIV(4'-0)			43'-8	Ρv	
quivalent Pipe Ler	ngths of Valves and	Fittings (C=120 or	ıly)		C Valu	e Multiplier					
/	Actual Inside	Diameter	۱ ^{4.87}		Value	Of C	100	130	140		150
	hedule 40 Steel Pip		—) = Fa	actor		lying Factor	0.713	1.16	1.33		1.51
V SCI	ieuuie 40 Steel Pip	e mane Diameter	,		<u>internet</u>	iying i actor	0.715	1.10	1.00		1.01

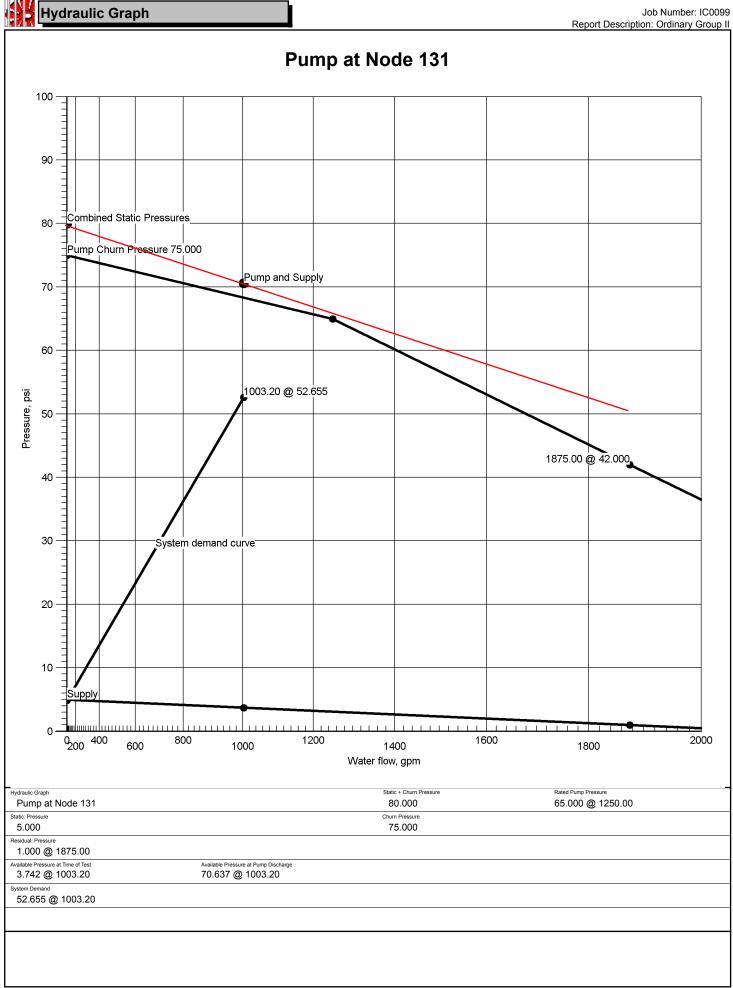


Job Number: IC0099

		Flow Discharge	Velocity K-Factor	HWC Pt	Pn	Friction Loss Fittings		Length Eq. Length Total Length	Pressure Summary
Pipe Type Legend			Ur	its Legend				Fittings Legen	d
Arm-Over BL Branch Line Cross Main DN Drain DR Drop DY Dynamic Feed Main Feed Riser MS Miscellaneous DR Outrigger RN Riser Nipple SP Sprig ST Stand Pipe JG Underground	Diamet Elevati Flow Discha Velocity Pressu Length Frictior HWC Pt Pn Pf Pe Pv	on Foo gpm rge gpm y fps re psi Foo I Loss psi// Haz Tota Nori Pres	t Foot en-Williams Cons al pressure at a po mal pressure at a ssure loss due to	pint in a pipe point in a pi friction betw ation differer	ipe een points nce betweer	n indicated points	ALV AngV b BalV BFP BV C cplg Cr CV DPV E EE Ee1 Ee2 f f f f DPV E EE Ee1 Ee2 f f f f CV DPV E EE Ee1 Ee2 f f f SloV GV Ho BV C V DPV E E E Str T T T V V DPV E E Str Str Str Str Str Str Str Str Str Str	Alarm Valve Angle Valve Bushing Ball Valve Backflow Prevente Butterfly Valve Cross Flow Turn 9 Coupling Cross Run Check Valve Deluge Valve Dry Pipe Valve 90° Elbow 45° Elbow 11¼° Elbow 22½° Elbow Flow Device Flex Drop Fire Department C 90° FireLock(TM) 1 Flange Floating Node FireLock(TM) 1 Flange Floating Node FireLock(TM) 1 Flange Globe Valve Gate Valve Hose Hose Hose Hose Hose Valve Hose Hose Valve Hose Valve Hose Hose Valve Hose Valve Vater Meter Valve Cap	onnection Elbow Elbow

Hydraulic Overview	Report Description: O	Number: IC(Indinary Gro
ob Number		
IC0099	Besign Engineer Brad Vokes	
^{bb} Name: LANL TWF	Phone FAX 1-226-668-8168	
dress 1 LOS ALAMOS NATIONAL LABS	State Certification/License Number	
dress 2	LHA LTA LTA LTA LTA LTA LTA LTA LTA LTA LT	
idress 3	LANL FPDO Job Site/Building	
	Building 149	
rstem nsily	Area of Application	
0.200gpm/ft ²	1950.00ft ² (Actual 1966.05ft ²)	
st Demanding Sprinkler Data 5.6 K-Factor 18.43 at 10.829	Hose Streams 500.00	
verage Per Sprinkler Varies	Number Of Sprinklers Calculated	
Valles	System Flow Demand	
al Demand	1003.20	
1003.20		
pplies	Check Point Gauges	
Name Flow(qpm) Hose Flow(qpm) Static(psi) 62 Tank Supply 1875.00 5.000	Residual(psi) Identifier Pressure(psi) K-Factor(K) 1.000	Flow(gpm)
131 1250.00 Pump 75.000	65.000	
Pumns: Static = Chura (Prassure @ Zero Flow)		
	Tank Supply at Node 62 (1875.00, 0.00, 5.000, 1.000)	
	Tank Supply at Node 62 (1875.00, 0.00, 5.000, 1.000)	
0099 LANL TWF Rev 3	10 7 - Static Pressure 5.000	
	10 7 Static Pressure 5.000 4	
0099 LANL TWF Rev 3	10 7 - Static Pressure 5.000	
2099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 2	
D099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 2	
D099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 2	
2099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 2	
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 -2 System demand curve -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 -2 -2 -3 -5 -5 -11 -11 -11 -11 -11 -11	
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 -2 System demand curve -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 -2 -2 System demand curve -5 -11 -14 -1003.20 @ -14.240	
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 -2 -3 -5 -11 -14 -14 -17 -14 -17 -14 -17 -14 -1 -7 -14 -1 -14 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	
	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 -2 -3 -5 -11 -14 -14 -17 -20 -20 -20 -20 -20 -20 -20 -20	400
	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 -2 -3 -5 -11 -14 -14 -17 -14 -17 -14 -17 -14 -1 -7 -14 -1 -14 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	400

H)	ydraulic Sumr	mary							Jo Report Descriptior	ob Number: IC009 n: Ordinary Group	
Job											
Job Number IC0099						Design Enginee Brad Vo					
Job Name: LANL TW	VF					State Certificatio	n/License Number				
Address 1 LOS ALA	AMOS NATIONAL LA	BS				AHJ LANL F	PDO				
Address 2						Job Site/Buildin Buildin					
Address 3						Drawing Name	-				
System						IC0099 LANL TWF Rev 3 Remote Area(s)					
Most Demanding S	Sprinkler Data ICtor 18.43 at 10.829	9				Occupancy Job Suffix Ordinary Group II			bb Suffix		
Hose Allowance At						Density Area of Appli			rea of Application	00.05(2)	
Additional Hose Su	upplies					0.200g	DM/ft ²		1950.00ft ² (Actual 19 overage Per Sprinkler	66.05tt²)	
Node			w(gpm)			22			Varies		
Hydrant A	At Node 44	5	00.00			Autoreak Resu	Its: Pressure For Remote Area(S) Aujacent 10 Most Remote Art	za		
Total Hose Stream	ns					-					
500.00 System Flow Dema	nand		Total Water Required (Including	Hose Allowance)		-					
1003.20			1003.20			_					
Maximum Velocity 9.79 betv Volume capacity of	etween nodes 766 and ^{, Under Ground} ween nodes 73 and 7		Volume capacity of Dry Pipes	41 Gallons		-					
Supplies				1			1			1	
Node	Name	Hose Flo (gpm)	w Static (psi)	Residual (psi)	@	Flow (gpm)	Available (psi) @	Total Demand (gpm)	Required (psi)	Safety Margin (psi)	
62	Tank Supply		5.000	1.000		875.00	3.742	1003.20	0.000	17.982	
131		Pump	75.000	65.000	1	250.00	70.637	1003.20	52.655	17.982	
Pumps: Stat	utic = Churn (Pressure @ Ze	ro Flow)									
Contractor											
	Contractor Number	er				Contact Nar BRAI	D VOKES		Contact Title DESIGI	NER	
	RN STATES FIRE PR						68-8168		Extension		
Address 1 5200 PAS	SADENA AVE NE, SU	JITE A				FAX 505-8	384-1863				
Address 2	· - ·					E-mail		2119			
Address 3						BRAI Web-Site	D.VOKES@WSFF	.00			
ALBUQU	JERQUE, NM 87113										





Summary Of Outflowing Devices

					· · ·	ort Description: Ordinary Gro
Device	•	Actual Flow (gpm)	Minimum Flow (gpm)	K-Factor (K)	Pressure (psi)	Coverage (Foot)
Hydrant	44	500.00	500.00	267.26	45.887	
Sprinkler	1649	19.72	18.43	5.6	12.403	92.15sqft
Sprinkler	1674	19.89	18.43	5.6	12.614	92.15sqft
Sprinkler	1675	20.45	18.43	5.6	13.341	92.15sqft
Sprinkler	1676	21.61	18.43	5.6	14.893	92.15sqft
Sprinkler	1677	23.51	18.43	5.6	17.622	92.15sqft
Sprinkler	1678	26.25	18.43	5.6	21.970	92.15sqft
Sprinkler	1679	31.56	18.43	5.6	31.752	92.15sqft
Sprinkler	1681	17.96	14.82	5.6	10.291	74.10sqft
Sprinkler	1682	18.07	14.82	5.6	10.414	74.10sqft
🖈 Sprinkler	1683	18.43	18.43	5.6	10.829	92.15sqft
Sprinkler	1684	19.34	18.43	5.6	11.926	92.15sqft
Sprinkler	1685	21.10	18.43	5.6	14.192	92.15sqft
Sprinkler	1686	23.62	18.43	5.6	17.789	92.15sqft
Sprinkler	1687	26.98	18.43	5.6	23.208	92.15sqft
Sprinkler	1688	33.14	14.82	5.6	35.016	74.10sqft
Sprinkler	1690	19.55	18.43	5.6	12.184	92.15sqft
Sprinkler	1691	19.71	18.43	5.6	12.393	92.15sqft
Sprinkler	1692	20.27	18.43	5.6	13.108	92.15sqft
Sprinkler	1693	21.42	18.43	5.6	14.635	92.15sqft
Sprinkler	1694	23.31	18.43	5.6	17.320	92.15sqft
Sprinkler	1695	26.03	18.43	5.6	21.598	92.15sqft
Sprinkler	1696	31.29	18.43	5.6	31.224	92.15sqft

➡ Most Demanding Sprinkler Data

Pipe Type	Diameter	Flow	Velocity	нмс	Friction Loss	Length	Pressure	
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length	1	nmary
Upstream						Total Length		
••••• Route 1 •					0.44440			
M	1.6100	54.46	8.58	100	0.144442 Sprinkler	7'-6		1.083
1683 1684	13'-0½ 13'-0	18.43	5.6	10.829 11.926	Sprinkler	7' 6	1	0.014
M	1.6100	72.90	11.63	100	0.253413	7'-6 8'-10½		2 240
1684	13'-0	<u>73.80</u> 19.34	5.6	11.926	Sprinkler	0-10/2		0.017
1685	12'-11½	19.04	5.0	14.192	ophilker	8'-10½	1	0.017
M	1.6100	94.90	14.96	100	0.403486	8'-101/2		3.581
1685	12'-11½	21.10	5.6	14.192	Sprinkler	0 10/2		0.017
1686	12'-11			17.789		8'-10½	-	
M	1.6100	118.52	18.68	100	0.608692	8'-10½		5.402
1686	12'-11	23.62	5.6	17.789	Sprinkler			0.017
1687	12'-10½			23.208		8'-10½	Ρv	
Μ	1.6100	145.50	22.93	100	0.889550	9'-8	Pf	14.316
1687	12'-10½	26.98	5.6	23.208	Sprinkler,	6'-5	Pe	0.733
781	11'-2½			38.258	LtE(1'-5), mecT(5'-0)	16'-1		
M	4.0260	340.22	8.57	100	0.049334	10'-4		0.510
781	11'-2½	194.72		38.258	Flow (q) from Route 2		1	0.008
766	11'-2			38.776		10'-4		
M	4.0260	503.20	12.68	100	0.101772		Pf	
766	11'-2	162.99		38.776	Flow (q) from Route 3	26'-9½	1	4.217
113	1'-5½			46.715	2fE(4'-10), DPV, CV(15'-8),	36'-7	Pv	
<u> </u>	6 4000	502.00	E 00	120	PIV(1'-5) 0.007599		P (0.404
G 113	<u>6.4000</u> 1'-5½	503.20	5.02	<u>120</u> 46.715	0.007099			0.464 2.576
39	-4'-6			40.715 49.755	3E(18'-2½)	61'-0		2.070
G	5.3480	503.20	7.19	150	0.012059			0.591
39	-4'-6	505.20	7.15	49.755	0.012000	30'-0		0.591
37	-4'-6			50.346	T(30'-0)	49'-0		
G	6.9630	585.44	4.93	150	0.004414			0.361
37	-4'-6	82.23	1.00	50.346	Flow (q) from Route 9			-0.000
61	-4'-6			50.707	PIV(4'-0)	81'-11	1	
G	6.4700	585.44	5.71	120	0.009536			0.010
61	-4'-6		-	50.707			Pe	
63	-4'-6			50.717		1'-0	Ρv	
IG	6.9630	585.44	4.93	150	0.004414	21'-6	Pf	0.249
63	-4'-6			50.717		35'-0	Pe	
71	-4'-6			50.966	T(35'-0)	56'-6	Ρv	
IG	6.9630	1003.20	8.45	150	0.011954			0.105
71	-4'-6	417.77		50.966	Flow (q) from Route 8	4'-0		
72	-4'-6			51.071	PIV(4'-0)	8'-9½		
JG	6.4700	1003.20	9.79	120	0.025830	1'-0	Pf	0.026
72	-4'-6			51.071			Pe	
73	-4'-6			51.097		1'-0		
G	6.9630	1003.20	8.45	150	0.011954			2.722
73	-4'-6			51.097				0.000
75	-4'-6	1000.00	0.10	53.819	EE(9'-0), T(35'-0), E(18'-0)	227'-8	_	4
M	7.9810	1003.20	6.43	120	0.009294			1.546
75	-4'-6			53.819			1	-2.710
131	1'-9			52.655	2LtE(13'-0), 2T(35'-0), BV(12'-0),	166'-4	PV	
			Mel''		CV(45'-0)		-	
'ump 131		1003.20	Velocity	52.655	Rating: 65.000 @ 1250.00			
129		Q=1003.20	6.43	-15.688	Churn Pressure: 75.000			
M	7.9810	1003.20	6.43	120	0.009294	6' 0	Df	0.539
129	1'-9	1003.20	0.40	-15.688	0.000207			-1.409
129	5'-0			-16.558	GV(4'-0), LtE(13'-0), T(35'-0)	58'-0		1.409
M	11.9380	1003.20	2.88	120	0.001308		_	0.367
124	5'-0		_ ,	-16.558				1.951
62	0'-6			-14.240	sCV(65'-0), GV(6'-0), 7LtE(18'-0),	280'-8		
	-			-	S		.	
		0.00			Hose Allowance At Source			
62		1003.20				1		
••••• Route 2 •	••••						1	
M	1.6100	19.55	3.08	100	0.021697	8'-10½	Pf	0.193
1690	12'-2	19.55	5.6	12.184	Sprinkler			0.016
1691	12'-2		-	12.393	-	8'-10½		
M	1.6100	39.26	6.19	100	0.078836	8'-10½		0.700
1691	12'-2	19.71	5.6	12.393	Sprinkler			0.016
1692	12'-1½			13.108		8'-10½		-

Pipe Type	Diameter	Flow	Velocity	HWC	Friction Loss	Length		ssure	
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length		Summary	
Upstream						Total Length			
M	1.6100	59.54	9.38	100	0.170308	8'-10½			
1692	12'-1½	20.27	5.6	13.108	Sprinkler	01.401/		0.016	
1693 M	12'-1	80.96	12.76	<u>14.635</u> 100	0.300738	8'-10½ 8'-10½		0.000	
1693	<u>1.6100</u> 12'-1	21.42	5.6	14.635	Sprinkler	8-10/2		2.669	
1694	12'-0½	21.42	5.0	17.320	Spillikei	8'-10½		0.010	
CM	1.6100	104.26	16.43	100	0.480232	8'-10½		4 262	
1694	12'-01/2	23.31	5.6	17.320	Sprinkler	0-10/2		0.016	
1695	12'-0	20.01	5.0	21.598	oprinder	8'-10½		0.010	
CM	1.6100	130.29	20.53	100	0.725238			9.951	
1695	12'-0	26.03	5.6	21.598	Sprinkler,			0.014	
796	11'-11½	20.00	0.0	31.562	T(5'-8½)	13'-8½	-	0.014	
CM	1.6100	161.58	25.46	100	1.079996			6.217	
796	11'-11½	31.29	20.40	31.562	Flow (q) from Route 5			0.332	
795	11'-2½	01120		38.111	mecT(5'-0)	5'-9		0.002	
CM	4.0260	161.58	4.07	100	0.012443			0.104	
795	11'-2½	101.00	1.07	38.111				0.006	
782	11'-2½			38.221		8'-4	-		
CM	4.0260	194.72	4.91	100	0.017572			0.035	
782	11'-2½	33.14		38.221	Flow (q) from Route 7			0.002	
781	11'-2½			38.258		2'-0			
••••• Route 3 •									
	1.6100	19.72	3.11	100	0.022057	8'-10½	Pf	0 196	
1649	12'-2	19.72	5.6	12.403	Sprinkler	0-10/2		0.016	
1674	12'-1½			12.614	- 1	8'-10½		2.010	
CM	1.6100	39.61	6.24	100	0.080141	8'-101/2		0 711	
1674	12'-1½	19.89	5.6	12.614	Sprinkler	- 0 10/2		0.016	
1675	12'-1			13.341		8'-10½			
CM	1.6100	60.07	9.47	100	0.173120	8'-101/2		1 536	
1675	12'-1	20.45	5.6	13.341	Sprinkler			0.016	
1676	12'-0½			14.893		8'-10½			
СМ	1.6100	81.68	12.87	100	0.305687	8'-10½		2.713	
1676	12'-01/2	21.61	5.6	14.893	Sprinkler			0.016	
1677	12'-0½			17.622		8'-10½			
CM	1.6100	105.18	16.58	100	0.488098	8'-101/2		4 332	
1677	12'-01/2	23.51	5.6	17.622	Sprinkler	- 0 10/2		0.016	
1678	12'-0			21.970		8'-10½			
СМ	1.6100	131.43	20.71	100	0.737051			10.11	
1678	12'-0	26.25	5.6	21.970	Sprinkler,			0.014	
763	11'-11½			32.096	T(5'-8½)	13'-8½			
CM	1.6100	162.99	25.69	100	1.097452			6.339	
763	11'-11½	31.56		32.096	Flow (q) from Route 6			0.340	
766	11'-2			38.776	mecT(5'-0)	5'-9½	-		
••••• Route 4 •									
СМ	1.6100	17.96	2.83	100	0.018560	6'-0	Pf	0.111	
1681	13'-1	17.96	5.6	10.291	Sprinkler			0.011	
1682	13'-0½			10.414		6'-0			
CM	1.6100	36.04	5.68	100	0.067275			0.404	
1682	13'-0½	18.07	5.6	10.414	Sprinkler			0.011	
1683	13'-0½			10.829	·	6'-0			
••••• Route 5 •				-					
	1.6100	31.29	4.93	100	0.051814	0'-10½	Pf	0.340	
1696	11'-11½	31.29	5.6	31.224	Sprinkler,		1	-0.002	
796	11'-11½			31.562	T(5'-8½)	6'-7			
••••• Route 6 •									
CM	1.6100	31.56	4.97	100	0.052625	0'-10½	Pf	0.345	
1679	11'-11½	31.56	5.6	31.752	Sprinkler,		1	-0.002	
763	11'-11½			32.096	T(5'-8½)	6'-7			
••••• Route 7 •									
BL	1.0490	33.14	12.30	100	0.464044	1'_81⁄_	Pf	2.456	
1688	12'-11	33.14	5.6	35.016	Sprinkler,			0.749	
782	11'-2½		0.0	38.221	mecT(3'-7)	5'-3½		0.7 10	
••••• Route 8 •						0 072			
JG	5.3480	500.00	7.14	150	0.011917	1/1 0	Df	1.081	
44	2'-6	500.00	1.14	45.887	Hydrant,			3.035	
44	-4'-6	000.00		50.002	E(14'-0), CV(32'-0), T(30'-0)	90'-8		0.000	
JG	6.9630	500.00	4.21	150	0.003296		_	0.301	
41	-4'-6	500.00	4.21	50.002	0.000200			0.301	
52	-4-0 -4'-6			50.303	2EE(9'-0)	91'-5			
<u>52</u> JG	6.9630	417.77	3.52	150	0.002364			0.021	
52	<u> </u>	41/.//	3.52	50.303	0.002007	4'-11		0.021	
UL	- - -0			30.303	PIV(4'-0)	4-0	re		

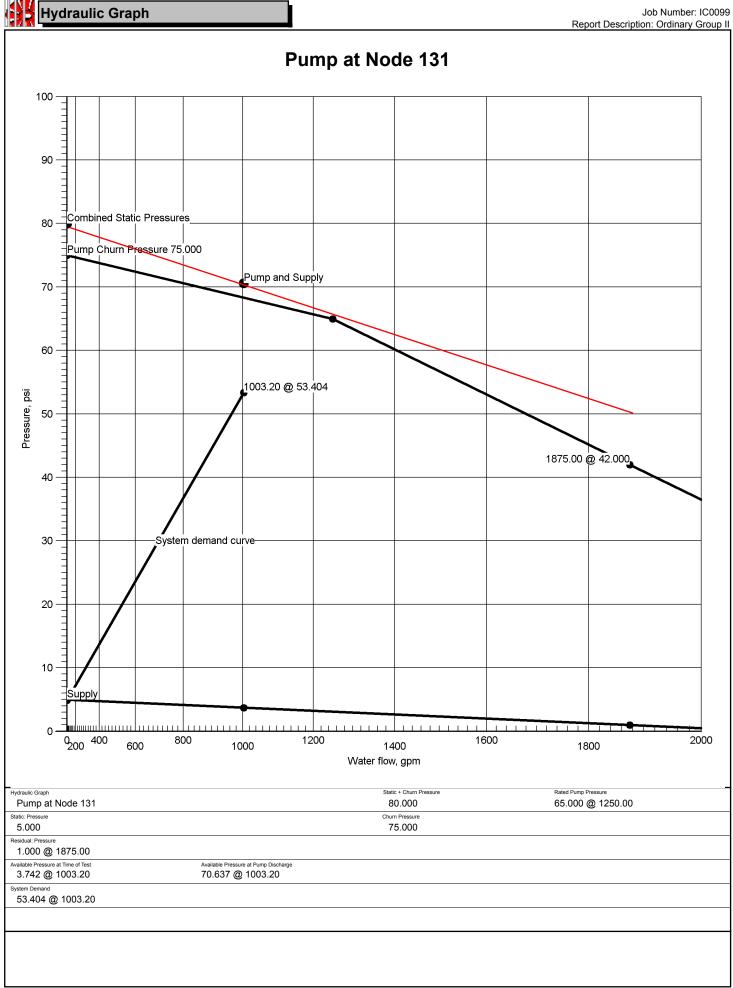
essure Immary		Length Eq. Length Total Length		3	Friction Loss Fittings	Pn	HWC Pt	Velocity K-Factor	Flow Discharge	Diameter Elevation	Pipe Type Downstream Upstream
0.005	Pf				0.005108		120	4.08	417.77	6.4700	JG
	Pe						50.324			-4'-6	53
,	Pv	1'-0					50.329			-4'-6	54
0.622					0.002364		150	3.52	417.77	6.9630	JG
•	Pe	40'-0					50.329			-4'-6	54
,	Pv	263'-3		V(4'-0)	4EE(9'-0), Pl		50.952			-4'-6	69
0.005	Pf	1'-0			0.005108		120	4.08	417.77	6.4700	JG
•	Pe						50.952			-4'-6	69
,	Pv	1'-0					50.957			-4'-6	70
0.009	Pf	3'-11			0.002364		150	3.52	417.77	6.9630	JG
•	Pe						50.957			-4'-6	70
,	Pv	3'-11					50.966			-4'-6	71
										• • • •	••••• Route 9 •
0.008					0.000117		150	0.69	82.23	6.9630	JG
÷	Pe	4'-0					50.329			-4'-6	24
,	Ρv	67'-0			PIV(4'-0)		50.337			-4'-6	25
0.000	Pf	1'-0			0.000253		120	0.80	82.23	6.4700	JG
•	Pe						50.337			-4'-6	25
,	Pv	1'-0					50.337			-4'-6	26
0.009	Pf	41'-7			0.000117		150	0.69	82.23	6.9630	JG
e 0.000	Pe	35'-0					50.337			-4'-6	26
,	Pv	76'-7			T(35'-0)		50.346			-4'-6	37
										• • • • •	••••• Route 10
0.000	Pf	1'-0			0.000253		120	0.80	82.23	6.4700	JG
•	Pe						50.308			-4'-6	51
,	Pv	1'-0					50.309			-4'-6	50
0.013	Pf	94'-5½			0.000117		150	0.69	82.23	6.9630	JG
)	Pe	13'-0					50.309			-4'-6	50
,	Ρv	107'-5½		(4'-0)	EE(9'-0), PIV		50.321			-4'-6	18
0.000	Pf	1'-0			0.000253		120	0.80	82.23	6.4700	JG
•	Pe						50.321			-4'-6	18
,	Ρv	1'-0					50.321			-4'-6	19
		57'-0			0.000117		150	0.69	82.23	6.9630	JG
•	Pe	4'-0					50.321			-4'-6	19
	Ρv	61'-0			PIV(4'-0)		50.329			-4'-6	22
0.000	Pf	1'-0			0.000253		120	0.80	82.23	6.4700	JG
	Pe						50.329			-4'-6	22
,	Ρv	1'-0					50.329			-4'-6	24
										• • • •	••••• Route 11
0.005	Pf	4'-8			0.000117		150	0.69	82.23	6.9630	JG
	-	39'-0			T(35'-0)		50.303			-4'-6	52
	Pv	43'-8			PIV(4'-0)		50.308			-4'-6	51
					e Multiplier	C Valu		ly)	Fittings (C=120 on	gths of Valves and	Equivalent Pipe Lei
150		140	130	100	Of C	Value		۱ ^{4.87} –	Diameter	Actual Inside [(
1.51		1.33	1.16	0.713	lying Factor	Multin	actor	—) = Fi	Incida Diamatar	edule 40 Steel Pipe	



Hydraulic A					R	eport Description:	-
	iameter Flow levation Discharg	Velocity e K-Factor	HWC Pt Pn	Friction Loss Fittings		Length Eq. Length Total Length	Pressure Summary
Pipe Type Legend		l	Jnits Legend			Fittings Legen	d
O Arm-Over L Branch Line M Cross Main N Drain R Drop Y Dynamic M Feed Main R Feed Riser IS Miscellaneous 8 Outrigger N Riser Nipple P Sprig T Stand Pipe IG Underground	Diameter Elevation Flow Discharge Velocity Pressure Length Friction Loss HWC Pt Pn Pf Pe Pv	Inch Foot gpm gpm fps psi Foot psi/Foot Hazen-Williams Co Total pressure at a Normal pressure at Pressure loss due t	nstant point in a pipe a point in a pipe o friction between po evation difference be	ints ween indicated points	AngV b BalV BFP BV C cplg Cr CV DelV DPV E E E E e 1 f f f FDC f E E e 2 f f f FDC f F BV C CV DPV E E E e 2 f f f FDC f F P V DPV E E E e 2 f f f FDC f F P V DPV E E E e 2 f f f FDC F F P V DPV E E E e 2 f f FDC F F P V DPV E E E f f S N T T S S CV DPV E E E f f S N T T S S CV DPV E E E E f S N T P V V P V V P V V P V V P V V P V V P V V V V V V V V V V V V V	Alarm Valve Angle Valve Bushing Ball Valve Backflow Prevente Butterfly Valve Cross Flow Turn 9 Coupling Cross Run Check Valve Deluge Valve 90° Elbow 45° Elbow 11/2° Elbow 22/2° Elbow Flow Device Flex Drop Fire Department C 90° FireLock(TM) I Flange Floating Node FireLock(TM) Tee Gauge Globe Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Calve Hose Nozzle Pump In Pump Out Post Indicating Val Pipe Outlet Pressure Reducing Pressure Relief Va Reducer/Adapter Supply Swing Check Valve Sprinkler Strainer Tee Flow Turn 90° Tee Run Union Wirsbo Water Meter Valve Cap	onnection Elbow Elbow

	Report Description: Ordin	
Number C0099	Design Engineer Brad Vokes	
Name:	Phone FAX	
LANL TWF	1-226-668-8168 State Certification/License Number	
LOS ALAMOS NATIONAL LABS	AHJ	
	LANL FPDO	
Iress 3	Job StlerBuilding Building 150	
stem		
^{usity} J.200gpm/ft²	Area of Application 1950.00ft ² (Actual 1966.05ft ²)	
st Demanding Sprinkler Data 5.6 K-Factor 18.43 at 10.829	Hose Streams 500.00	
erage Per Sprinkler Varles	Number Of Sprinklers Calculated	
vuico	System Flow Demand	
al Demand	1003.20	
1003.20	Charle Daint Courses	
pplies lode Name Flow(gpm) Hose Flow(gpm) Static	Check Point Gauges si) Residual(psi) Identifier Pressure(psi) K-Factor(K) Floc	ow(gpm)
62 Tank Supply 1875.00 5.00		- MANU
131 1250.00 Pump 75.0	0 65.000	
Pumps: Static = Churn (Pressure @ Zero Flow) 20099 LANL TWF Rev 3	Tank Supply at Node 62 (1875.00, 0.00, 5.000, 1.000)	

Hy	ydraulic Sumr	mary							Jo Report Descriptior	ob Number: IC009 n: Ordinary Group	
Job									· · ·	· · ·	
Job Number IC0099						Design Enginee Brad Vo					
Job Name: LANL TV	VF					State Certification	n/License Number				
Address 1	AMOS NATIONAL LA	BS				AHJ LANL F	PDO				
Address 2						Job Site/Buildin	9				
Address 3						Drawing Name	-				
System						IC0099 LANL TWF Rev 3 Remote Area(s)					
Most Demanding S		0			_	Occupancy	b Suffix				
Hose Allowance Al	ictor 18.43 at 10.829	9				Density	y Group II		ea of Application		
Additional Hose St	upplies					0.200gp Number Of Spri	Dm/ft ²		1950.00ft ² (Actual 19 overage Per Sprinkler	66.05ft ²)	
Node			w(gpm)			22			Varies		
Hydrant	At Node 44	5	00.00			Autoreak Resu	IS. FIESSUR FOI REINOLE AREA	s) Adjacent To Most Remote Are	ia		
Total Hose Stream	ns										
500.00 System Flow Dem	nand		Total Water Required (Including I	Hose Allowance)							
1003.20			1003.20								
Maximum Velocity 9.79 betv Volume capacity o	etween nodes 647 and ^{, Under Ground} ween nodes 73 and 7		Volume capacity of Dry Pipes	41 Gallons							
Supplies											
Node	Name	Hose Flo (gpm)	w Static (psi)	Residual (psi)	(a)	Flow (gpm)	Available (psi) @	Total Demand (gpm)	Required (psi)	Safety Margin (psi)	
62	Tank Supply		5.000	1.000		875.00	3.742	1003.20	0.000	17.233	
131		Pump	75.000	65.000	1	250.00	70.637	1003.20	53.404	17.233	
Pumps: Sta	ttic = Churn (Pressure @ Ze	ro Flow)									
Contractor											
	Contractor Number	er				Contact Nar			Contact Title		
Name of Contracto						Phone	O VOKES		DESIGI Extension		
Address 1	RN STATES FIRE PR					FAX	68-8168				
5200 PAS	SADENA AVE NE, SU	JITE A				505-8 E-mail	84-1863				
						BRAD	D.VOKES@WSFF	2.US			
Address 3 ALBUQU	JERQUE, NM 87113					Web-Site					





Summary Of Outflowing Devices

						ort Description: Ordinary Gro
Device		Actual Flow (gpm)	Minimum Flow (gpm)	K-Factor (K)	Pressure (psi)	Coverage (Foot)
Hydrant	44	500.00	500.00	267.26	46.571	
Sprinkler	1583	19.72	18.43	5.6	12.403	92.15sqft
Sprinkler	1584	19.89	18.43	5.6	12.614	92.15sqft
Sprinkler	1585	20.45	18.43	5.6	13.341	92.15sqft
Sprinkler	1586	21.61	18.43	5.6	14.893	92.15sqft
Sprinkler	1587	23.51	18.43	5.6	17.622	92.15sqft
Sprinkler	1588	26.25	18.43	5.6	21.970	92.15sqft
Sprinkler	1589	31.56	18.43	5.6	31.752	92.15sqft
Sprinkler	1591	17.96	14.82	5.6	10.291	74.10sqft
Sprinkler	1592	18.07	14.82	5.6	10.414	74.10sqft
🔷 Sprinkler	1593	18.43	18.43	5.6	10.829	92.15sqft
Sprinkler	1594	19.34	18.43	5.6	11.926	92.15sqft
Sprinkler	1595	21.10	18.43	5.6	14.192	92.15sqft
Sprinkler	1596	23.62	18.43	5.6	17.789	92.15sqft
Sprinkler	1597	26.98	18.43	5.6	23.208	92.15sqft
Sprinkler	1598	33.14	14.82	5.6	35.016	74.10sqft
Sprinkler	1600	19.55	18.43	5.6	12.184	92.15sqft
Sprinkler	1601	19.71	18.43	5.6	12.393	92.15sqft
Sprinkler	1605	20.27	18.43	5.6	13.108	92.15sqft
Sprinkler	1606	21.42	18.43	5.6	14.635	92.15sqft
Sprinkler	1607	23.31	18.43	5.6	17.320	92.15sqft
Sprinkler	1608	26.03	18.43	5.6	21.598	92.15sqft
Sprinkler	1609	31.29	18.43	5.6	31.224	92.15sqft

➡ Most Demanding Sprinkler Data

Pipe Type	Diameter	Flow	Velocity	HWC	Friction Loss	Length	Pre	ssure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length	1	nmary
Upstream						Total Length		
••••• Route 1 •					0.44440			
M	1.6100	54.46	8.58	100	0.144442 Sprinkler	7'-6		1.083
1593 1594	13'-0½ 13'-0	18.43	5.6	10.829 11.926	Sprinkler	7' 6	1	0.014
N	1.6100	72.90	11.63	100	0.253413	7'-6 8'-10½		2.240
1594	13'-0	<u>73.80</u> 19.34	5.6	11.926	Sprinkler	0-10/2		0.017
1595	12'-11½	13.54	5.0	14.192	ophilidei	8'-10½	1	0.017
M	1.6100	94.90	14.96	100	0.403486	8'-101/2		3.581
1595	12'-11½	21.10	5.6	14.192	Sprinkler			0.017
1596	12'-11			17.789	·	8'-10½	-	
М	1.6100	118.52	18.68	100	0.608692	8'-10½	Pf	5.402
1596	12'-11	23.62	5.6	17.789	Sprinkler			0.017
1597	12'-10½			23.208		8'-10½	Ρv	
Μ	1.6100	145.50	22.93	100	0.889550	9'-8	Pf	14.316
1597	12'-10½	26.98	5.6	23.208	Sprinkler,	6'-5	Pe	0.733
61	11'-2½			38.258	LtE(1'-5), mecT(5'-0)	16'-1		
Μ	4.0260	340.22	8.57	100	0.049334	10'-4	Pf	0.510
661	11'-2½	194.72		38.258	Flow (q) from Route 2		Pe	0.008
647	11'-2			38.776		10'-4		
M	4.0260	503.20	12.68	100	0.101772		Pf	
647	11'-2	162.99		38.776	Flow (q) from Route 3		1	4.217
112	1'-5½			46.715	2fE(4'-10), DPV, CV(15'-8),	36'-7	Pv	
				105	PIV(1'-5)			0.1-
G	6.4000	503.20	5.02	120	0.007599			0.464
112	1'-5½			46.715	25(10) 21()			2.576
11	-4'-6	500.00	7.40	49.755	<u>3E(18'-2½)</u>	61'-0	_	1 0 5 5
G	5.3480	503.20	7.19	150	0.012059			1.255
11 27	-4'-6 -4'-6			49.755 51.010	E(14'-0)	14'-0 104'-1		
		504.00	4.75	150	0.004119			0.463
G 27	<u>6.9630</u> -4'-6	<u>564.00</u> 60.79	4.75	51.010	Flow (q) from Route 9		PT	0.463
51	-4-0 -4'-6	00.79		51.473	PIV(4'-0)	112'-6	1	
G	6.4700	564.00	5.50	120	0.008900			0.009
61	-4'-6	564.00	5.50	51.473	0.000900		PT	0.009
63	-4'-6			51.482		1'-0		
IG	6.9630	564.00	4.75	150	0.004119			0.233
63	-4'-6	504.00	4.75	51.482	0.001110	35'-0		0.200
71	-4'-6			51.715	T(35'-0)	56'-6		
G	6.9630	1003.20	8.45	150	0.011954		_	0.105
71	-4'-6	439.21	0.10	51.715	Flow (q) from Route 8		Pe	000
72	-4'-6			51.820	PIV(4'-0)	8'-91/2		
G	6.4700	1003.20	9.79	120	0.025830	1'-0	Pf	0.026
72	-4'-6			51.820			Pe	
73	-4'-6			51.846		1'-0	Ρv	
G	6.9630	1003.20	8.45	150	0.011954	165'-8	Pf	2.722
73	-4'-6			51.846		62'-0	Pe	0.000
75	-4'-6			54.567	EE(9'-0), T(35'-0), E(18'-0)	227'-8	Ρv	
Μ	7.9810	1003.20	6.43	120	0.009294	13'-4	Pf	1.546
75	-4'-6			54.567			1	-2.710
131	1'-9			53.404	2LtE(13'-0), 2T(35'-0), BV(12'-0),	166'-4	Ρv	
					CV(45'-0)			
ump			Velocity			_		
131		1003.20	0.45	53.404	Rating: 65.000 @ 1250.00			
129		Q=1003.20	6.43	-14.939	Churn Pressure: 75.000			0
M	7.9810	1003.20	6.43	120	0.009294			0.539
129	1'-9			-14.939			-	-1.409
124	5'-0	4000.00	0.00	-15.809	GV(4'-0), LtE(13'-0), T(35'-0) 0.001308	58'-0		0.007
M	11.9380	1003.20	2.88	120	0.001300			0.367
124 62	5'-0 0'-6			-15.809		197-0 280'-8		1.951
02	0-0			-13.491	sCV(65'-0), GV(6'-0), 7LtE(18'-0), S	280-8	PV	
		0.00			Hose Allowance At Source		-	
62		1003.20				-		
••••• Route 2 •	••••							
M	1.6100	19.55	3.08	100	0.021697	8'-101%	Pf	0.193
1600	12'-2	19.55	5.6	12.184	Sprinkler			0.016
1601	12'-2			12.393		8'-10½		2.010
M	1.6100	39.26	6.19	100	0.078836	8'-101/2		0.700
1601	12'-2	19.71	5.6	12.393	Sprinkler			0.016
1605	12'-1½		-	13.108		8'-10½		

Pipe Type	Diameter	Flow	Velocity	HWC	Friction Loss	Length	Pres	sure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length		nmary
Upstream						Total Length		
M	1.6100	59.54	9.38	100	0.170308	8'-10½		
1605	12'-1½	20.27	5.6	13.108	Sprinkler			0.016
1606	12'-1			14.635	0.000700	8'-10½		
M	1.6100	80.96	12.76	100	0.300738	8'-10½		
1606	12'-1	21.42	5.6	14.635	Sprinkler			0.016
1607	12'-0½			17.320		8'-10½		
CM	1.6100	104.26	16.43	100	0.480232	8'-10½		
1607	12'-0½	23.31	5.6	17.320	Sprinkler			0.016
1608	12'-0			21.598		8'-10½		
CM	1.6100	130.29	20.53	100	0.725238			9.951
1608	12'-0	26.03	5.6	21.598	Sprinkler,			0.014
676	11'-11½			31.562	T(5'-8½)	13'-8½		
CM	1.6100	161.58	25.46	100	1.079996			6.217
676	11'-11½	31.29		31.562	Flow (q) from Route 5			0.332
675	11'-2½			38.111	mecT(5'-0)	5'-9		
CM	4.0260	161.58	4.07	100	0.012443	8'-4	Pf	0.104
675	11'-2½			38.111			Ре	0.006
662	11'-2½			38.221		8'-4	Ρv	
CM	4.0260	194.72	4.91	100	0.017572	2'-0	Pf	0.035
662	11'-2½	33.14		38.221	Flow (q) from Route 7			0.002
661	11'-2½			38.258		2'-0		
••••• Route 3 •								
	1.6100	19.72	3.11	100	0.022057	8'-10½	Pf	0 196
1583	12'-2	19.72	5.6	12.403	Sprinkler	0-10/2		0.190
1584	12'-1½	10.72	0.0	12.614		8'-10½		0.010
CM	1.6100	39.61	6.24	12.014	0.080141	8'-101/2		0 744
1584	<u>1.6100</u> 12'-1½	<u> </u>	<u> </u>	12.614	Sprinkler	δ-10/2		0.711
		19.09	5.0		Sphinkler	01.401/		0.016
1585	12'-1			13.341	0.170100	8'-10½	_	. = = = =
CM	1.6100	60.07	9.47	100	0.173120	8'-10½		
1585	12'-1	20.45	5.6	13.341	Sprinkler			0.016
1586	12'-0½			14.893		8'-10½		
CM	1.6100	81.68	12.87	100	0.305687	8'-10½		2.713
1586	12'-0½	21.61	5.6	14.893	Sprinkler		Pe	0.016
1587	12'-0½			17.622		8'-10½		
CM	1.6100	105.18	16.58	100	0.488098	8'-10½		
1587	12'-0½	23.51	5.6	17.622	Sprinkler		Ре	0.016
1588	12'-0			21.970		8'-10½	Ρv	
CM	1.6100	131.43	20.71	100	0.737051			10.11
1588	12'-0	26.25	5.6	21.970	Sprinkler,	5'-8½	Pe	0.014
644	11'-11½			32.096	T(5'-81⁄2)	13'-8½		
СМ	1.6100	162.99	25.69	100	1.097452	0'-9½	Pf	6.339
644	11'-11½	31.56		32.096	Flow (q) from Route 6	5'-0	Ре	0.340
647	11'-2			38.776	mecT(5'-0)	5'-9½	Pv	
••••• Route 4 •								
CM	1.6100	17.96	2.83	100	0.018560	6'-0	Df	0.111
1591	13'-1	17.96	5.6	10.291	Sprinkler			0.011
1592	13'-0½		0.0	10.414		6'-0		0.011
CM	1.6100	36.04	5.68	100	0.067275			0.404
1592	13'-0½	18.07	5.6	10.414	Sprinkler	0-0		0.404
1592		10.07	5.0		Opinikier	61.0		0.011
	13'-0½			10.829		6'-0	۳V	
• • • • • Route 5 •		04.00	4.00	100	0.051914			0.015
	1.6100	31.29	4.93	100	0.051814	0'-10½	1	
1609	11'-11½	31.29	5.6	31.224	Sprinkler,			-0.002
676	11'-11½			31.562	T(5'-8½)	6'-7	Pv	
••••• Route 6 •								
CM	1.6100	31.56	4.97	100	0.052625	0'-10½	1	
1589	11'-11½	31.56	5.6	31.752	Sprinkler,	5'-8½	Ре	-0.002
644	11'-11½			32.096	T(5'-81⁄2)	6'-7	Pv	
••••• Route 7 •	••••							
3L	1.0490	33.14	12.30	100	0.464044	1'-8½	Pf	2.456
1598	12'-11	33.14	5.6	35.016	Sprinkler,			0.749
662	11'-2½		-	38.221	mecT(3'-7)	5'-3½		
••••• Route 8 •					· /			
IG	5.3480	500.00	7.14	150	0.011917	1/10	Df	1.081
44	2'-6	500.00	1.14	46.571	Hydrant,			3.035
		500.00						5.055
41	-4'-6	E0.5.5.5	4.54	50.686	E(14'-0), CV(32'-0), T(30'-0)	90'-8	_	0.01
IG	6.9630	500.00	4.21	150	0.003296			0.301
41	-4'-6			50.686		18'-0		
52	-4'-6			50.988	2EE(9'-0)	91'-5		
JG	6.9630	439.21	3.70	150	0.002594			0.023
52	-4'-6			50.988		4'-0	Pe	
53	-4'-6			51.011	PIV(4'-0)	8'-11	D	

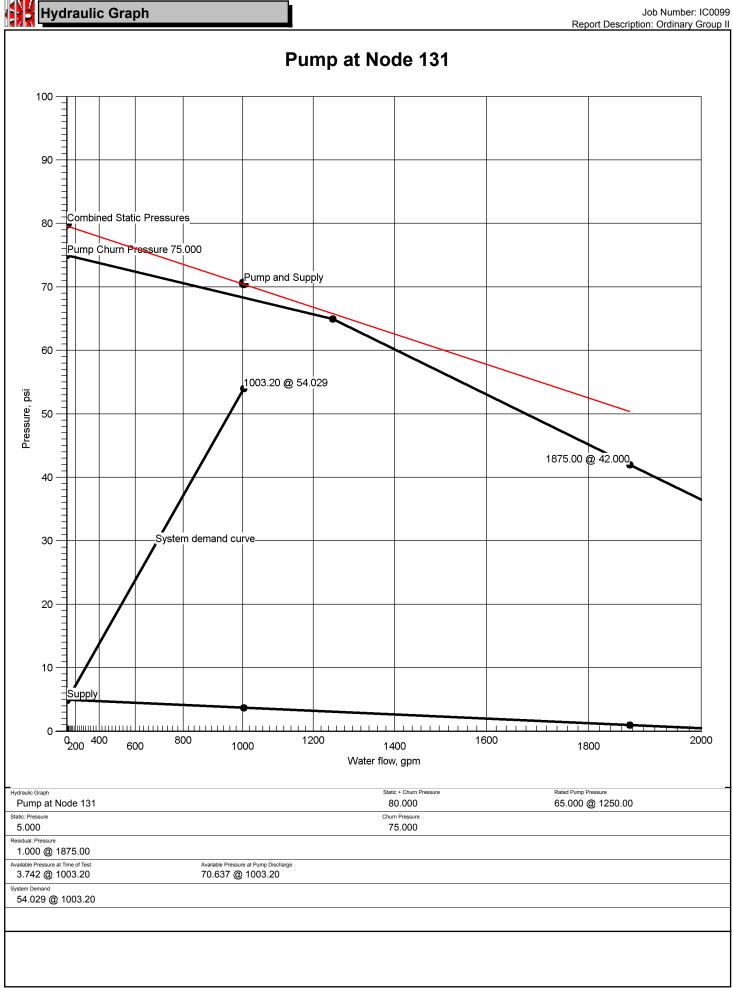
ipe Type Downstream Upstream	Diameter Elevation	Flow Discharge	Velocity K-Factor	HWC Pt	Pn	Friction Los Fittings	55		Length Eq. Length Total Length		ssure nmary
JG	6.4700	439.21	4.29	120		0.005604				Pf	0.006
53	-4'-6			51.011						Pe	
54	-4'-6			51.016					1'-0	Ρv	
JG	6.9630	439.21	3.70	150		0.002594			223'-3	Pf	0.683
54	-4'-6			51.016					40'-0	Pe	
69	-4'-6			51.699		4EE(9'-0), P	'IV(4'-0)		263'-3	Ρv	
JG	6.4700	439.21	4.29	120		0.005604			1'-0	Pf	0.006
69	-4'-6			51.699						Pe	
70	-4'-6			51.705					1'-0	Ρv	
JG	6.9630	439.21	3.70	150		0.002594			3'-11	1	0.010
70	-4'-6			51.705						Pe	
71	-4'-6			51.715					3'-11	Ρv	
• • • • • Route 9 •	••••										
JG	6.9630	60.79	0.51	150		0.000067					0.004
24	-4'-6			51.002					4'-0		
25	-4'-6			51.007		PIV(4'-0)			67'-0		
JG	6.4700	60.79	0.59	120		0.000144			1'-0		0.000
25	-4'-6			51.007						Pe	
26	-4'-6			51.007					1'-0		
JG	6.9630	60.79	0.51	150		0.000067					0.003
26	-4'-6			51.007					35'-0		
27	-4'-6			51.010		T(35'-0)			46'-0	Ρv	
••••• Route 10											
JG	6.4700	60.79	0.59	120		0.000144			1'-0		0.000
51	-4'-6			50.991						Pe	
50	-4'-6			50.991					1'-0	_	
JG	6.9630	60.79	0.51	150		0.000067			94'-5½		0.007
50	-4'-6			50.991					13'-0		
18	-4'-6			50.998		EE(9'-0), PI	V(4'-0)		107'-5½		
JG	6.4700	60.79	0.59	120		0.000144			1'-0		0.000
18	-4'-6			50.998						Pe	
19	-4'-6			50.998		0.00007			1'-0	Pv	
JG	6.9630	60.79	0.51	150		0.000067					0.004
19	-4'-6			50.998					4'-0		
22	-4'-6	00.70	0.50	51.002		PIV(4'-0)			61'-0		0.000
JG	6.4700	60.79	0.59	120		0.000144			1'-0	Pf	0.000
22	-4'-6			51.002						Pe	
24	-4'-6			51.002					1'-0	PV	
•••••• Route 11			0.54	150		0.00007					0.000
JG	6.9630	60.79	0.51	150		0.000067			4'-8		0.003
52	-4'-6			50.988		T(35'-0)			39'-0		
51	-4'-6	Filling (0, 400 s	- 1	50.991	0.)/-1	PIV(4'-0)	•		43'-8	Pv	
quivalent Pipe Le	ngths of Valves and	•	11y)			e Multiplier					
(Actual Inside		\	actor	Value		100	130	140		150
Sc	hedule 40 Steel Pip	e Inside Diameter	/ = F	aului	Multip	ying Factor	0.713	1.16	1.33		1.51



		Flow Discharge	Velocity K-Factor	HWC Pt	Pn	Friction Loss Fittings		Length Eq. Length Total Length	Pressure Summary
Pipe Type Legend			Ur	its Legend				Fittings Legen	d
Arm-Over BL Branch Line Cross Main DN Drain DR Drop DY Dynamic Feed Main Feed Riser MS Miscellaneous DR Outrigger RN Riser Nipple SP Sprig ST Stand Pipe JG Underground	Diamet Elevati Flow Discha Velocity Pressu Length Frictior HWC Pt Pn Pf Pe Pv	on Foo gpm rge gpm y fps re psi Foo I Loss psi// Haz Tota Nori Pres	t Foot en-Williams Cons al pressure at a po mal pressure at a ssure loss due to	pint in a pipe point in a pi friction betw ation differer	ipe een points nce betweer	n indicated points	ALV AngV b BalV BFP BV C cplg Cr CV DPV E EE Ee1 Ee2 f f f f DPV E EE Ee1 Ee2 f f f f CV DPV E EE Ee1 Ee2 f f f SloV GV Ho BV C V DPV E E E Str T T T V V DPV E E Str Str T Str Str Str Str Str Str Str Str Str Str	Alarm Valve Angle Valve Bushing Ball Valve Backflow Prevente Butterfly Valve Cross Flow Turn 9 Coupling Cross Run Check Valve Deluge Valve Dry Pipe Valve 90° Elbow 45° Elbow 11¼° Elbow 22½° Elbow Flow Device Flex Drop Fire Department C 90° FireLock(TM) 1 Flange Floating Node FireLock(TM) 1 Flange Floating Node FireLock(TM) 1 Flange Globe Valve Gate Valve Hose Hose Hose Hose Hose Valve Hose Hose Valve Bose Valve Hose Hose Valve Hose Hose Hose Valve Hose Hose Valve Hose Hose Hose Valve Hose Hose Hose Hose Hose Hose Hose Hos	onnection Elbow Elbow

Hydraulic Overview	Report Description: Ordinary Gr
bb bk Number	Design Engineer
IC0099 bb Name:	Phone FAX
LANL TWF	1-226-668-8168 State Certification/License Number
LOS ALAMOS NATIONAL LABS	
dress 2	AHJ LANL FPDO
dress 3	Job SterBuilding Building 151
rstem	Building 191
nsity	Area of Application
0.200gpm/ft ² Ist Demanding Sprinkler Data	1950.00ft² (Actual 1966.05ft²) Hose Streams
5.6 K-Factor 18.43 at 10.829 verage Per Sprinkler	500.00 Number Of Sprinklers Calculated
Varies	22
	System Flow Demand 1003.20
al Demand 1003.20	
pplies	Check Point Gauges
Node <u>Name Flow(gpm) Hose Flow(gpm) Static(psi)</u> Residual(ps	
62 Tank Supply 1875.00 5.000 1.000	
131 1250.00 Pump 75.000 65.000	
Pumps: Static = Chum (Pressure @ Zero Flow)	
	Tank Supply at Node 62 (1875.00, 0.00, 5.000, 1.000)
	Tank Supply at Node 62 (1875.00, 0.00, 5.000, 1.000) 10
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000
	10 7 Static Pressure 5.000 4
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 2
D0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 2
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 2
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 2
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 1875.00 @ 1.000 -2 System demand curve -3 -5 -4 -6
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 1875.00 @ 1.000 -2 System demand curve 9 -5 -1 -8 -11 -11
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 1875.00 @ 1.000 -2 System demand curve -3 -5 -4 -6
	10 7 Static Pressure 5.000 4 1 1 1875.00 @ 1.000 -2 System demand curve -3 -4 -11 1003.20 @ -12.866 -14 1003.20 @ -12.866
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1 1875.00 @ 1.000 -2 System demand curve -3 -4 -11 1003.20 @ -12.866 -14 -17
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1 1875.00 @ 1.000 -2 System demand curve -3 -4 -11 1003.20 @ -12.866 -14 1003.20 @ -12.866

Н	ydraulic Sumr	mary							Report Descripti	Job Number: IC0099 on: Ordinary Group I	
Job				_							
Job Number IC0099						Design Enginee Brad Vo					
Job Name: LANL TW	VF					State Certification	n/License Number				
Address 1	AMOS NATIONAL LA	BS				AHJ LANL F	PDO				
Address 2						Job Site/Buildin	9				
Address 3						Drawing Name	-				
System						IC0099 LANL TWF Rev 3 Remote Area(s)					
Most Demanding S	Sprinkler Data Ctor 18.43 at 10.829	2				Occupancy	y Group II	Job Suffix			
Hose Allowance At		, 				Density	-		Area of Application	1000 05#2)	
Additional Hose Su	upplies						DM/π ²		1950.00ft ² (Actual Coverage Per Sprinkler	1966.05π²)	
<u>Node</u> Hydrant A	At Node 44		(<u>gpm)</u>).00			22 AutoPeak Resul	ts: Pressure For Remote Area(s) Adjacent To Most Remote A	Varies		
Total Hose Stream 500.00 System Flow Dem		T	tal Water Required (Jochalian I-	lose Allowance)							
System Flow Dema 1003.20	ianu		tal Water Required (Including H 1003.20	use Allowance)							
Maximum Velocity 9.79 betv Volume capacity of	tween nodes 544 and ^{Under Ground} ween nodes 73 and 7	2	lume capacity of Dry Pipes	1 Gallons							
Supplies			Chatia	Desidual		Flaur	Ausilahla	Total Damand	Dequired	Cofet Mannin	
Node	Name	Hose Flow (gpm)	Static (psi)	Residual (psi)	(M)	Flow (gpm)	Available (psi) @	Total Demand (gpm)	Required (psi)	Safety Margin (psi)	
62 131	Tank Supply	Pump	5.000 75.000	1.000 65.000		875.00 250.00	3.742 70.637	1003.20 1003.20	0.000	16.608 16.608	
	tic = Churn (Pressure @ Ze										
Contractor											
	Contractor Number	er				Contact Nar BRA			Contact Title	GNER	
Name of Contractor		OTECTION				Phone	68-8168		Extension		
Address 1 5200 PAS	SADENA AVE NE, SU	JITE A				FAX 505-8	84-1863		I		
Address 2						E-mail					
Address 3						Web-Site	D.VOKES@WSFF	.03			
ALBUQU	JERQUE, NM 87113										





Summary Of Outflowing Devices

					R	eport Description: Ordinary Gro
Device		Actual Flow (gpm)	Minimum Flow (gpm)	K-Factor (K)	Pressure (psi)	Coverage (Foot)
Hydrant	44	500.00	500.00	267.26	47.003	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
Sprinkler	1558	19.72	18.43	5.6	12.403	92.15sqft
Sprinkler	1559	19.89	18.43	5.6	12.614	92.15sqft
Sprinkler	1560	20.45	18.43	5.6	13.341	92.15sqft
Sprinkler	1561	21.61	18.43	5.6	14.893	92.15sqft
Sprinkler	1562	23.51	18.43	5.6	17.622	92.15sqft
Sprinkler	1563	26.25	18.43	5.6	21.970	92.15sqft
Sprinkler	1564	31.56	18.43	5.6	31.752	92.15sqft
Sprinkler	1566	17.96	14.82	5.6	10.291	74.10sqft
Sprinkler	1567	18.07	14.82	5.6	10.414	74.10sqft
Sprinkler 🕈	1568	18.43	18.43	5.6	10.829	92.15sqft
Sprinkler	1569	19.34	18.43	5.6	11.926	92.15sqf
Sprinkler	1570	21.10	18.43	5.6	14.192	92.15sqf
Sprinkler	1571	23.62	18.43	5.6	17.789	92.15sqf
Sprinkler	1572	26.98	18.43	5.6	23.208	92.15sqft
Sprinkler	1573	33.14	14.82	5.6	35.016	74.10sqft
Sprinkler	1575	19.55	18.43	5.6	12.184	92.15sqft
Sprinkler	1576	19.71	18.43	5.6	12.393	92.15sqf
Sprinkler	1577	20.27	18.43	5.6	13.108	92.15sqf
Sprinkler	1578	21.42	18.43	5.6	14.635	92.15sqf
Sprinkler	1579	23.31	18.43	5.6	17.320	92.15sqft
Sprinkler	1580	26.03	18.43	5.6	21.598	92.15sqf
Sprinkler	1581	31.29	18.43	5.6	31.224	92.15sqft

➡ Most Demanding Sprinkler Data

Pipe Type	Diameter	Flow	Velocity	нжс	Friction Loss	Length	Pres	ssure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length		nmary
Upstream	Lievation	Discharge	N-I actor		i ittiliga	Total Length	Jun	intary
••••• Route 1 •	• • • •					Total Length		
M	1.6100	54.46	8.58	100	0.144442	7'-6	Df	1.083
1568	13'-0½	18.43	5.6	10.829	Sprinkler			0.014
1569	13'-0	10.10	0.0	11.926	op	7'-6		0.011
<u>и</u>	1.6100	73.80	11.63	100	0.253413	8'-10½		2 2/10
1569	13'-0	19.34	5.6	11.926	Sprinkler	0-10/2		0.017
1570	12'-11½	10.04	0.0	14.192	opinition	8'-10½	1	0.017
M	1.6100	94.90	14.96	100	0.403486	8'-101/2		3.581
1570	12'-11½	21.10	5.6	14.192	Sprinkler	0-10/2		0.017
1571	12'-11	21.10	5.0	17.789	Opinikei	8'-10½		0.017
N	1.6100	118.52	18.68	100	0.608692	8'-10/2		F 400
1571	12'-11	23.62	5.6	17.789	Sprinkler	0-10/2		0.017
1572	12'-10½	23.02	5.0	23.208	opinidei	8'-10½		0.017
		145 50	00.00	100	0.889550			14.31
M	1.6100	145.50	22.93	23.208	Sprinkler,			
1572	12'-10½	26.98	5.6		•			0.733
558	11'-2½			38.258	LtE(1'-5), mecT(5'-0)	16'-1		
M	4.0260	340.22	8.57	100	0.049334			0.510
558	11'-2½	194.72		38.258	Flow (q) from Route 2			0.008
544	11'-2			38.776	0.404770	10'-4		• -
M	4.0260	503.20	12.68	100	0.101772		Pf	3.722
544	11'-2	162.99		38.776	Flow (q) from Route 3	26'-9½	-	4.217
10	1'-5½			46.715	2fE(4'-10), DPV, CV(15'-8),	36'-7	Pv	
					PIV(1'-5)		-	
G	6.4000	503.20	5.02	120	0.007599			0.464
10	1'-5½			46.715				2.576
5	-4'-6			49.755	3E(18'-2½)	61'-0		
G	5.3480	503.20	7.19	150	0.012059			1.664
5	-4'-6			49.755		44'-0		
23	-4'-6			51.419	E(14'-0), PO(30'-0)	138'-0	Pv	
G	6.9630	504.10	4.25	150	0.003347	52'-0	Pf	0.187
23	-4'-6	0.90		51.419	Flow (q) from Route 9	4'-0	Pe	
25	-4'-6			51.607	PIV(4'-0)	56'-0	Pv	
G	6.4700	504.10	4.92	120	0.007231	1'-0	Pf	0.007
25	-4'-6			51.607			Pe	
26	-4'-6			51.614		1'-0	Pv	
G	6.9630	504.10	4.25	150	0.003347	119'-6	Pf	0.530
26	-4'-6			51.614		39'-0	Pe	
61	-4'-6			52.144	T(35'-0), PIV(4'-0)	158'-6	Pv	
G	6.4700	504.10	4.92	120	0.007231	1'-0	Pf	0.007
51	-4'-6			52.144			Pe	
63	-4'-6			52.151		1'-0		
G	6.9630	504.10	4.25	150	0.003347			0.189
63	-4'-6			52.151		35'-0		
71	-4'-6			52.341	T(35'-0)	56'-6		
G	6.9630	1003.20	8.45	150	0.011954			0.105
71	-4'-6	499.10	0.10	52.341	Flow (g) from Route 8		Pe	0.100
72	-4'-6			52.445	PIV(4'-0)	8'-91/2		
G	6.4700	1003.20	9.79	120	0.025830		_	0.026
72	-4'-6	1003.20	5.13	52.445	0.020000		PI	0.020
73	-4'-6			52.445		1'-0		
G	6.9630	1003.20	8.45	150	0.011954			2.722
<u> </u>	-4'-6	1003.20	0.40	52.471	0.011001			0.000
75	-4-0 -4'-6			55.193	EE(9'-0), T(35'-0), E(18'-0)	227'-8		0.000
<u>и</u>	7.9810	1003.20	6.43	120	0.009294			1.546
VI 75	-4'-6	1003.20	0.43	55.193	0.003237			-2.710
					21 tE(13' 0) 2T(25' 0) DV((13' 0)			-2.710
131	1'-9			54.029	2LtE(13'-0), 2T(35'-0), BV(12'-0),	166'-4	PV	
			Male elt		CV(45'-0)		-	
ump 131		1003.20	Velocity	54.029	Rating: 65.000 @ 1250.00	-	1	
			6 42		Churn Pressure: 75.000		1	
29	7.0040	Q=1003.20	6.43	-14.314		010	B ²	0.500
1	7.9810	1003.20	6.43	120	0.009294			0.539
29	1'-9			-14.314				-1.409
24	5'-0			-15.184	GV(4'-0), LtE(13'-0), T(35'-0)	58'-0		
M	11.9380	1003.20	2.88	120	0.001308			0.367
124	5'-0			-15.184				1.951
62	0'-6			-12.866	sCV(65'-0), GV(6'-0), 7LtE(18'-0),	280'-8	Pv	
					S			
		0.00			Hose Allowance At Source			
62		1002 20					1	
		1003.20					1	

Pipe Type	Diameter	Flow	Velocity	нжс	Friction Loss	Length	Pres	sure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length		nmary
Upstream						Total Length		
N	1.6100	19.55	3.08	100	0.021697	8'-10½	Pf	0.193
575	12'-2	19.55	5.6	12.184	Sprinkler		Pe	0.016
576	12'-2			12.393		8'-10½	Ρv	
Л	1.6100	39.26	6.19	100	0.078836	8'-10½	Pf	0.700
1576	12'-2	19.71	5.6	12.393	Sprinkler		Pe	0.016
1577	12'-1½			13.108		8'-10½	Ρv	
М	1.6100	59.54	9.38	100	0.170308	8'-10½	Pf	1.511
1577	12'-1½	20.27	5.6	13.108	Sprinkler		Pe	0.016
1578	12'-1			14.635		8'-10½	Ρv	
M	1.6100	80.96	12.76	100	0.300738	8'-10½	Pf	2.669
1578	12'-1	21.42	5.6	14.635	Sprinkler		Pe	0.016
1579	12'-0½			17.320		8'-10½	Ρv	
M	1.6100	104.26	16.43	100	0.480232	8'-10½	Pf	4.262
1579	12'-0½	23.31	5.6	17.320	Sprinkler		Pe	0.016
1580	12'-0			21.598	·	8'-10½		
M	1.6100	130.29	20.53	100	0.725238			9.951
1580	12'-0	26.03	5.6	21.598	Sprinkler,		1	0.014
573	11'-11½			31.562	T(5'-8½)	13'-8½		
M	1.6100	161.58	25.46	100	1.079996			6.217
573	11'-11½	31.29	20.70	31.562	Flow (q) from Route 5		1	0.332
572	11'-2½	0		38.111	mecT(5'-0)	5'-9		0.002
:M	4.0260	161.58	4.07	100	0.012443			0.104
572	11'-2½	101.00	T.UI	38.111	0.012110	0-4		0.104
559	11'-21/2			38.221		8'-4		0.000
559 CM	4.0260	194.72	4.91	100	0.017572			0.035
559	4.0260	<u> 194.72 </u>	4.91	38.221	Flow (g) from Route 7	Z'-U	1	0.035
	11'-2½ 11'-2½	33.14		38.221 38.258	riow (q) Itolii Roule /	2'-0		0.002
558				38.258		2-0	PV	
••••• Route 3					0.000057			
CM	1.6100	19.72	3.11	100	0.022057	8'-10½	1	
1558	12'-2	19.72	5.6	12.403	Sprinkler			0.016
1559	12'-1½			12.614		8'-10½		
M	1.6100	39.61	6.24	100	0.080141	8'-10½	1	
1559	12'-1½	19.89	5.6	12.614	Sprinkler			0.016
1560	12'-1			13.341		8'-10½		
M	1.6100	60.07	9.47	100	0.173120	8'-10½	Pf	1.536
1560	12'-1	20.45	5.6	13.341	Sprinkler		Pe	0.016
1561	12'-0½			14.893		8'-10½		
M	1.6100	81.68	12.87	100	0.305687	8'-10½	Pf	2.713
1561	12'-0½	21.61	5.6	14.893	Sprinkler			0.016
1562	12'-0½			17.622		8'-10½	Ρv	
M	1.6100	105.18	16.58	100	0.488098	8'-10½		4.332
1562	12'-0½	23.51	5.6	17.622	Sprinkler			0.016
1563	12'-0			21.970		8'-10½	Ρv	
M	1.6100	131.43	20.71	100	0.737051			10.11
1563	12'-0	26.25	5.6	21.970	Sprinkler,			0.014
541	11'-11½			32.096	T(5'-8½)	13'-8½		
M	1.6100	162.99	25.69	100	1.097452			6.339
541	11'-11½	31.56	20.00	32.096	Flow (q) from Route 6		1	0.340
544	11'-2	01.00		38.776	mecT(5'-0)	5'-9½		0.040
••••• Route 4				00.110		5-3/2	1. V	
		17.06	2.02	100	0.018560	010	Df	0.111
M 1566	<u> </u>	<u>17.96</u> 17.96	<u>2.83</u> 5.6	<u>100</u> 10.291	Sprinkler	0-0		0.111
		17.50	5.0		Ophilikier	6'-0		0.011
1567	13'-0½	26.04	E 00	10.414	0.067275			0.404
1567	1.6100	36.04	5.68	100		6'-0	1	0.404
1567	13'-0½	18.07	5.6	10.414	Sprinkler			0.011
1568	13'-0½			10.829		6'-0	PV	
••••• Route 5					0.051011			
M	1.6100	31.29	4.93	100	0.051814	0'-10½	1	
1581	11'-11½	31.29	5.6	31.224	Sprinkler,			-0.00
573	11'-11½			31.562	T(5'-8½)	6'-7	Pv	
••••• Route 6	• • • • •							
M	1.6100	31.56	4.97	100	0.052625	0'-10½	Pf	0.345
1564	11'-11½	31.56	5.6	31.752	Sprinkler,	5'-8½	Pe	-0.00
541	11'-11½			32.096	T(5'-8½)	6'-7		
••••• Route 7								
L	1.0490	33.14	12.30	100	0.464044	1'_81⁄_	Pf	2.456
1573	12'-11	33.14	5.6	35.016	Sprinkler,			0.749
559	11'-2½	00.14	0.0	38.221	mecT(3'-7)	5'-3½		0.7-3
				JU.22 I		0-3/2	F'V	
••••• Route 8		F 00.00	7 / /	450	0.011017			4.00
IG	5.3480	500.00	7.14	150	0.011917			1.081
44	2'-6	500.00		47.003	Hydrant,			3.035
41	-4'-6			51.118	E(14'-0), CV(32'-0), T(30'-0)	90'-8	Pv	

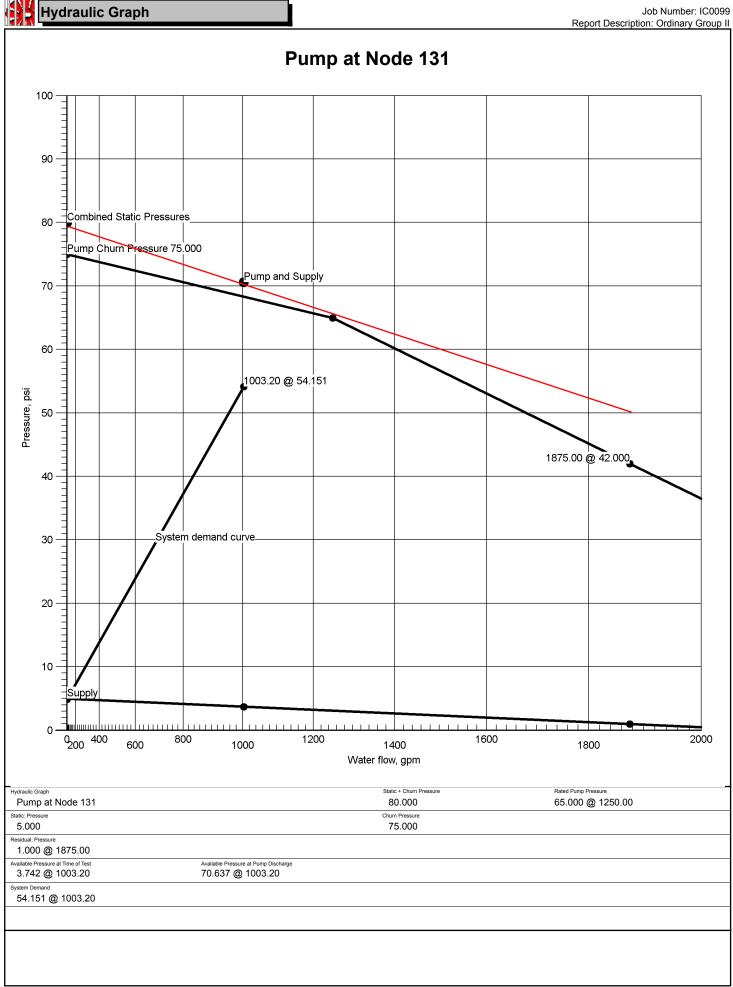
Pipe Type	Diameter	Flow	Velocity	HWC		Friction Los	S		Length	Pre	ssure
Downstream Upstream	Elevation	Discharge	K-Factor	Pt	Pn	Fittings			Eq. Length Total Length	Sun	nmary
JG	6.9630	500.00	4.21	150		0.003296			73'-5	Pf	0.301
41	-4'-6			51.118					18'-0	Pe	
52	-4'-6			51.419		2EE(9'-0)			91'-5	Ρv	
JG	6.9630	499.10	4.21	150		0.003286			4'-11	Pf	0.029
52	-4'-6			51.419					4'-0	Pe	
53	-4'-6			51.449		PIV(4'-0)			8'-11	Ρv	
JG	6.4700	499.10	4.87	120		0.007099			1'-0	Pf	0.007
53	-4'-6			51.449						Pe	
54	-4'-6			51.456					1'-0	Ρv	
UG	6.9630	499.10	4.21	150		0.003286			223'-3		0.865
54	-4'-6			51.456					40'-0	Pe	
69	-4'-6			52.321		4EE(9'-0), PI	V(4'-0)		263'-3		
JG	6.4700	499.10	4.87	120		0.007099			1'-0	Pf	0.007
69	-4'-6			52.321				1		Pe	
70	-4'-6			52.328					1'-0	Ρv	
JG	6.9630	499.10	4.21	150		0.003286			3'-11	Pf	0.013
70	-4'-6			52.328						Pe	
71	-4'-6			52.341					3'-11	Ρv	
••••• Route 9 •	••••										
JG	6.4700	0.90	0.01	120		0.000000			1'-0	Pf	0.000
51	-4'-6			51.419						Pe	
50	-4'-6			51.419					1'-0	Ρv	
JG	6.9630	0.90	0.01	150		0.000000			94'-5½	Pf	0.000
50	-4'-6			51.419					13'-0	Pe	
18	-4'-6			51.419		EE(9'-0), PIV	(4'-0)		107'-5½		
UG	6.4700	0.90	0.01	120		0.000000			1'-0	Pf	0.000
18	-4'-6			51.419						Pe	
19	-4'-6			51.419					1'-0	Ρv	
JG	6.9630	0.90	0.01	150		0.000000			57'-0	Pf	0.000
19	-4'-6			51.419					4'-0	Pe	
22	-4'-6			51.419		PIV(4'-0)			61'-0	Ρv	
JG	6.4700	0.90	0.01	120		0.000000			1'-0	Pf	0.000
22	-4'-6			51.419						Pe	
24	-4'-6			51.419					1'-0	Ρv	
JG	6.9630	0.90	0.01	150		0.000000			11'-0	Pf	0.000
24	-4'-6			51.419				Γ		Pe	
23	-4'-6			51.419					11'-0	Pv	
••••• Route 10	••••										
JG	6.9630	0.90	0.01	150		0.000000					0.00
52	-4'-6			51.419		T(35'-0)			39'-0	Pe	
51	-4'-6			51.419		PIV(4'-0)			43'-8	Pv	
quivalent Pipe Le	ngths of Valves and	l Fittings (C=120 or	nly)		C Value	Multiplier					
(Actual Inside	Diameter	۱ ^{4.87} –		Value	Of C	100	130	140		150
Sc Sc	hedule 40 Steel Pip	e Inside Diameter	—) = Fi	actor	Multipl	ying Factor	0.713	1.16	1.33		1.51



Hydraulic A					R	eport Description:	-
	iameter Flow levation Discharg	Velocity e K-Factor	HWC Pt Pn	Friction Loss Fittings		Length Eq. Length Total Length	Pressure Summary
Pipe Type Legend		l	Jnits Legend			Fittings Legen	d
O Arm-Over L Branch Line M Cross Main N Drain R Drop Y Dynamic M Feed Main R Feed Riser IS Miscellaneous 8 Outrigger N Riser Nipple P Sprig T Stand Pipe IG Underground	Diameter Elevation Flow Discharge Velocity Pressure Length Friction Loss HWC Pt Pn Pf Pe Pv	Inch Foot gpm gpm fps psi Foot psi/Foot Hazen-Williams Co Total pressure at a Normal pressure at Pressure loss due t	nstant point in a pipe a point in a pipe o friction between po evation difference be	ints ween indicated points	AngV b BalV BFP BV C cplg Cr CV DelV DPV E E E E e 1 f f f FDC f E E e 2 f f f FDC f F BV C CV DPV E E E e 2 f f f FDC f F P V DPV E E E e 2 f f f FDC f F P V DPV E E E e 2 f f f FDC F F P V DPV E E E e 2 f f FDC F F P V DPV E E E f f S N T T S S CV DPV E E E f f S N T T S S CV DPV E E E E f S N T P V V P V V P V V P V V P V V P V V P V V V V V V V V V V V V V	Alarm Valve Angle Valve Bushing Ball Valve Backflow Prevente Butterfly Valve Cross Flow Turn 9 Coupling Cross Run Check Valve Deluge Valve 90° Elbow 45° Elbow 11/2° Elbow 22/2° Elbow Flow Device Flex Drop Fire Department C 90° FireLock(TM) I Flange Floating Node FireLock(TM) Tee Gauge Globe Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Valve Hose Hose Calve Hose Nozzle Pump In Pump Out Post Indicating Val Pipe Outlet Pressure Reducing Pressure Relief Va Reducer/Adapter Supply Swing Check Valve Sprinkler Strainer Tee Flow Turn 90° Tee Run Union Wirsbo Water Meter Valve Cap	onnection Elbow Elbow

Hydraulic Overview	Report Description: Ordinary Gro
bb bb Number	Design Engineer
IC0099 b Name:	Phone FAX
LANL TWF	1-226-668-8168
dress 1 LOS ALAMOS NATIONAL LABS	State Certification/License Number
dress 2	AHJ LANL FPDO
dress 3	Job Site/Building
atom.	Building 152
rsty	Area of Application
0.200gpm/ft ² st Demanding Sprinkler Data	1950.00ft² (Actual 1966.05ft²) Hose Streams
5.6 K-Factor 18.43 at 10.829	500.00
verage Per Sprinkler Varies	Number Of Sprinklers Calculated
	System Flow Demand 1003.20
al Demand	
1003.20	Check Point Caugos
pplies Node Name Flow(gpm) <u>Hose Flow(gpm)</u> Static(psi) <u>Residual(p</u>	Check Point Gauges si) Identifier Pressure(psi) K-Factor(K) Flow(gpm)
62 Tank Supply 1875.00 5.000 1.000	
131 1250.00 Pump 75.000 65.000	
Pumps: Static = Chum (Pressure @ Zero Flow) 0099 LANL TWF Rev 3	Tank Supply at Node 62 (1875.00, 0.00, 5.000, 1.000)
	10
	Tank Supply at Node 62 (1875.00, 0.00, 5.000, 1.000) 10
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1875 00 @ 1.000
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 2
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 2
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 2
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 -2 System demand curve
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 1875.00 @ 1.000 -2 System demand curve -5 -4 -1 -8
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 -2 System demand curve -5 -11 1003.20 @ -12.744
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1875.00 @ 1.000 1 1875.00 @ 1.000 -2 System demand curve -5 -4 -1 -8
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1 1875.00 @ 1.000 -2 System demand curve -5 -11 -11 1003.20 @ -12.744 -14 -14
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1 1875.00 @ 1.000 2 System demand curve 3 -5 -11 1003.20 @ -12.744 -14 -14
0099 LANL TWF Rev 3	10 7 Static Pressure 5.000 4 1 1 1875.00 @ 1.000 -2 System demand curve -5 -11 -11 1003.20 @ -12.744 -14 -14

Н	ydraulic Sumr	mary								Job Number: IC0099 on: Ordinary Group I
Job				-						in ordinary ordup i
Job Number IC0099						Design Enginee Brad Vo				
Job Name: LANL TW	VF					State Certificatio	n/License Number			
Address 1	AMOS NATIONAL LA	BS				AHJ LANL F	PDO			
Address 2						Job Site/Buildin	g			
Address 3						Drawing Name	-			
System						Remote A	LANL TWF Rev 3	3		
Most Demanding S	Sprinkler Data Ctor 18.43 at 10.829	2				Occupancy	y Group II		Job Suffix	
Hose Allowance At		, 				Density			Area of Application	000 05#2)
Additional Hose Su	upplies						pm/ff ²		1950.00ft ² (Actual 19 Coverage Per Sprinkler	966.0511²)
<u>Node</u> Hydrant A	At Node 44		r <u>(gpm)</u> 0.00			22 AutoPeak Resu	Its: Pressure For Remote Area(s) Adjacent To Most Remote A	Varies	
Total Hose Stream 500.00										
System Flow Dema 1003.20	and	T	otal Water Required (Including I 1003.20	Hose Allowance)						
		I								
Maximum Velocity	Above Ground	1/38								
Maximum Velocity	Under Ground					-				
Volume capacity of	ween nodes 73 and 7		olume capacity of Dry Pipes	41 Gallons		-				
Supplies										
		Hose Flow	Static	Residual	@	Flow	Available @	Total Demand	Required	Safety Margin
Node 62	Name Tank Supply	(gpm)	(psi) 5.000	(psi) 1.000		(gpm) 1875.00	(psi) (psi) (psi) (psi)	(gpm) 1003.20	(psi) 0.000	(psi) 16.487
131		Pump	75.000	65.000		1250.00	70.637	1003.20	54.151	16.487
Pumps: Stat	tic = Churn (Pressure @ Ze	ro Flow)								
Contractor										
	Contractor Number	ər							Contact Title DESIG	SNER
	RN STATES FIRE PR	OTECTION					68-8168		Extension	
Address 1 5200 PAS	SADENA AVE NE, SL	JITE A				FAX 505-8	384-1863			
Address 2	,					E-mail	D.VOKES@WSFF	PUS		
Address 3						Web-Site				
ALBUQU	JERQUE, NM 87113									





Summary Of Outflowing Devices

						port Description: Ordinary Gro
Device	•	Actual Flow (gpm)	Minimum Flow (gpm)	K-Factor (K)	Pressure (psi)	Coverage (Foot)
Hydrant	44	500.00	500.00	267.26	47.018	
Sprinkler	1533	19.72	18.43	5.6	12.403	92.15sqft
Sprinkler	1534	19.89	18.43	5.6	12.614	92.15sqft
Sprinkler	1535	20.45	18.43	5.6	13.341	92.15sqft
Sprinkler	1536	21.61	18.43	5.6	14.893	92.15sqf
Sprinkler	1537	23.51	18.43	5.6	17.622	92.15sqf
Sprinkler	1538	26.25	18.43	5.6	21.970	92.15sqf
Sprinkler	1539	31.56	18.43	5.6	31.752	92.15sqf
Sprinkler	1541	17.96	14.82	5.6	10.291	74.10sqft
Sprinkler	1542	18.07	14.82	5.6	10.414	74.10sqft
🖈 Sprinkler	1543	18.43	18.43	5.6	10.829	92.15sqf
Sprinkler	1544	19.34	18.43	5.6	11.926	92.15sqf
Sprinkler	1545	21.10	18.43	5.6	14.192	92.15sqf
Sprinkler	1546	23.62	18.43	5.6	17.789	92.15sqf
Sprinkler	1547	26.98	18.43	5.6	23.208	92.15sqf
Sprinkler	1548	33.14	14.82	5.6	35.016	74.10sqft
Sprinkler	1550	19.55	18.43	5.6	12.184	92.15sqf
Sprinkler	1551	19.71	18.43	5.6	12.393	92.15sqf
Sprinkler	1552	20.27	18.43	5.6	13.108	92.15sqf
Sprinkler	1553	21.42	18.43	5.6	14.635	92.15sqf
Sprinkler	1554	23.31	18.43	5.6	17.320	92.15sqf
Sprinkler	1555	26.03	18.43	5.6	21.598	92.15sqf
Sprinkler	1556	31.29	18.43	5.6	31.224	92.15sqf

➡ Most Demanding Sprinkler Data

Pipe Type	Diameter	Flow	Velocity	нис	Friction Loss	Length	Pres	ssure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length		nmary
Upstream		2100110.90				Total Length		,
••••• Route 1 •	••••						-	
M	1.6100	54.46	8.58	100	0.144442	7'-6	Pf	1.083
1543	13'-0½	18.43	5.6	10.829	Sprinkler			0.014
1544	13'-0			11.926		7'-6		
M	1.6100	73.80	11.63	100	0.253413	8'-10½	Pf	2.249
1544	13'-0	19.34	5.6	11.926	Sprinkler			0.017
1545	12'-11½			14.192		8'-10½		
M	1.6100	94.90	14.96	100	0.403486	8'-10½		3.581
1545	12'-11½	21.10	5.6	14.192	Sprinkler			0.017
1546	12'-11			17.789		8'-10½		
M	1.6100	118.52	18.68	100	0.608692	8'-10½		5 402
1546	12'-11	23.62	5.6	17.789	Sprinkler			0.017
1547	12'-10½			23.208		8'-10½		
CM	1.6100	145.50	22.93	100	0.889550	9'-8		14.310
1547	12'-10½	26.98	5.6	23.208	Sprinkler,			0.733
455	11'-2½			38.258	LtE(1'-5), mecT(5'-0)	16'-1		
SM	4.0260	340.22	8.57	100	0.049334			0.510
455	11'-21/2	194.72	0.57	38.258	Flow (g) from Route 2	- 10-4		0.008
441	11'-2	134.72		38.776		10'-4		0.000
241 CM	4.0260	503.20	12.68	100	0.101772		_	3.722
441	4.0260	<u>503.20</u> 162.99	12.00	38.776	Flow (g) from Route 3			
		102.39			2fE(4'-10), DPV, CV(15'-8),	36'-7		4.217
107	1'-5½			46.715		36-7	PV	
10	0.4000	500.00	E 00	100	PIV(1'-5)	01 51 /		0.407
JG	6.4000	503.20	5.02	120	0.007599		1	0.464
107	1'-5½			46.715				2.576
8	-4'-6			49.755	3E(18'-2½)	61'-0	_	
JG	5.3480	503.20	7.19	150	0.012059			1.676
8	-4'-6			49.755		44'-0		
20	-4'-6			51.431	E(14'-0), PO(30'-0)	139'-0		
IG	6.9630	473.79	3.99	150	0.002984	52'-10½	Pf	0.170
20	-4'-6			51.431		4'-0	Pe	
22	-4'-6			51.601	PIV(4'-0)	56'-10½	Ρv	
IG	6.4700	473.79	4.62	120	0.006447	1'-0	Pf	0.006
22	-4'-6			51.601			Pe	
24	-4'-6			51.607		1'-0	Ρv	
JG	6.9630	473.79	3.99	150	0.002984	63'-0	Pf	0.200
24	-4'-6			51.607		4'-0		
25	-4'-6			51.807	PIV(4'-0)	67'-0		
JG	6.4700	473.79	4.62	120	0.006447			0.006
25	-4'-6			51.807			Pe	0.000
26	-4'-6			51.814		1'-0		
JG	6.9630	473.79	3.99	150	0.002984			0.473
26	-4'-6	470.75	0.00	51.814	0.002001	39'-0		0.470
61	-4'-6			52.287	T(35'-0), PIV(4'-0)	158'-6	-	
JG	6.4700	473.79	4.62	120	0.006447			0.006
61	-4'-6	475.75	4.02	52.287	0.000447		Pe	0.000
63	-4'-6			52.293		1'-0		
		470.70	2.00		0.002984			0.400
JG	6.9630	473.79	3.99	150	0.002904	21'-6		0.169
63	-4'-6			52.293	T(25' 0)			
71	-4'-6	1000.00	0.15	52.462	T(35'-0)	56'-6		0.105
IG	6.9630	1003.20	8.45	150	0.011954			0.105
71	-4'-6	529.42		52.462	Flow (q) from Route 8	4'-0		
72	-4'-6			52.567	PIV(4'-0)	8'-9½		
G	6.4700	1003.20	9.79	120	0.025830	1'-0		0.026
72	-4'-6			52.567			Pe	
73	-4'-6			52.592		1'-0	_	
IG	6.9630	1003.20	8.45	150	0.011954			2.722
73	-4'-6			52.592				0.000
75	-4'-6			55.314	EE(9'-0), T(35'-0), E(18'-0)	227'-8		
Μ	7.9810	1003.20	6.43	120	0.009294			1.546
75	-4'-6			55.314				-2.710
131	1'-9			54.151	2LtE(13'-0), 2T(35'-0), BV(12'-0),	166'-4	Ρv	
					CV(45'-0)			
ump			Velocity					
131		1003.20		54.151	Rating: 65.000 @ 1250.00			
129		Q=1003.20	6.43	-14.192	Churn Pressure: 75.000			
M	7.9810	1003.20	6.43	120	0.009294	6' 0	Pf	0.539
129	1'-9	1000.20	0.40	-14.192				-1.409
129	5'-0			-15.062	GV(4'-0), LtE(13'-0), T(35'-0)	58'-0		1.403
		1002.00	2 00		0.001308		_	0.207
M	11.9380	1003.20	2.88	120	0.001300			0.367
124	5'-0			-15.062 -12.744	sCV(65'-0), GV(6'-0), 7LtE(18'-0),	197'-0 280'-8		1.951
62	0'-6							

Job Number: IC0099	
port Description: Ordinary Group II	

Ріре Туре	Diameter	Flow	Velocity	HWC		Friction Loss	Length	Pressure
Downstream Upstream	Elevation	Discharge	K-Factor	Pt	Pn	Fittings	Eq. Length Total Length	Summary
		0.00				Hose Allowance At Source		
62		1003.20						
••••• Route 2 ••	1.6100	19.55	3.08	100		0.021697	8'-10½	Pf 0.193
CM 1550	12'-2	19.55	5.6	12.184		Sprinkler	0-10/2	Pr 0.193
1551	12'-2			12.393			8'-10½	
CM	1.6100	39.26	6.19	100		0.078836	8'-10½	
1551 1552	12'-2 12'-1½	19.71	5.6	12.393 13.108		Sprinkler	8'-10½	Pe 0.016
CM	1.6100	59.54	9.38	100		0.170308	8'-101/2	
1552	12'-1½	20.27	5.6	13.108		Sprinkler		Pe 0.016
1553	12'-1			14.635		0.000700	8'-10½	
CM 1553	<u>1.6100</u> 12'-1	80.96 21.42	<u>12.76</u> 5.6	<u>100</u> 14.635		0.300738 Sprinkler	8'-10½	Pf 2.669 Pe 0.016
1554	12'-0½	21.72	5.0	17.320		opinikoi	8'-10½	
CM	1.6100	104.26	16.43	100		0.480232	8'-10½	
1554	12'-0½	23.31	5.6	17.320		Sprinkler	01.401/	Pe 0.016
 CM	<u>12'-0</u> 1.6100	130.29	20.53	21.598 100		0.725238	8'-10½	PV Pf 9.951
1555	12'-0	26.03	5.6	21.598		Sprinkler,		Pe 0.014
470	11'-11½			31.562		T(5'-8½)	13'-8½	Pv
CM	1.6100	161.58	25.46	100		1.079996 Flow (q) from Route 5		Pf 6.217
470 469	11'-11½ 11'-2½	31.29		31.562 38.111		How (q) from Route 5 mecT(5'-0)		Pe 0.332
CM	4.0260	161.58	4.07	100		0.012443		Pf 0.104
469	11'-2½			38.111				Pe 0.006
456	11'-2½	104 70	4.04	38.221		0.017572		Pv
CM 456	4.0260 11'-2½	<u>194.72</u> 33.14	4.91	<u>100</u> 38.221		U.017572 Flow (q) from Route 7	2'-0	Pf 0.035 Pe 0.002
455	11'-21/2			38.258			2'-0	Pe 0.002
••••• Route 3 ••	•••							
CM	1.6100	19.72	3.11	100		0.022057	8'-101/2	
1533 1534	12'-2 12'-1½	19.72	5.6	12.403 12.614		Sprinkler	8'-10½	Pe 0.016
CM	1.6100	39.61	6.24	12.014		0.080141	8'-101/2	
1534	12'-1½	19.89	5.6	12.614		Sprinkler		Pe 0.016
1535	12'-1		0.47	13.341		0.470400	8'-10½	
CM 1535	<u>1.6100</u> 12'-1	<u>60.07</u> 20.45	<u>9.47</u> 5.6	<u>100</u> 13.341		0.173120 Sprinkler	8'-10½	Pf 1.536 Pe 0.016
1536	12'-0½	20.40	0.0	14.893		op	8'-10½	
СМ	1.6100	81.68	12.87	100		0.305687	8'-10½	Pf 2.713
1536	12'-0½	21.61	5.6	14.893		Sprinkler	8'-10½	Pe 0.016
1537 CM	12'-0½ 1.6100	105.18	16.58	<u>17.622</u> 100		0.488098		PV Pf 4.332
1537	12'-0½	23.51	5.6	17.622		Sprinkler		Pe 0.016
1538	12'-0			21.970		0 202054	8'-10½	
CM	1.6100	131.43	20.71	100		0.737051 Sprinkler,		Pf 10.113
1538 438	12'-0 11'-11½	26.25	5.6	21.970 32.096		Sprinkier, T(5'-8½)	5'-8½ 13'-8½	Pe 0.014
CM	1.6100	162.99	25.69	100		1.097452	0'-91/2	
438	11'-11½	31.56		32.096		Flow (q) from Route 6		Pe 0.340
441	11'-2			38.776		mecT(5'-0)	5'-91/2	Pv
Route 4 CM	1.6100	17.96	2.83	100		0.018560	<u>'a</u>	Pf 0.111
1541	13'-1	17.96	5.6	10.291		Sprinkler		Pe 0.011
1542	13'-0½			10.414				Pv
CM	1.6100	36.04	5.68	100		0.067275 Sprinkler	6'-0	Pf 0.404
1542 1543	13'-0½ 13'-0½	18.07	5.6	10.414 10.829		орника	6'-0	Pe 0.011
••••• Route 5 ••								
CM	1.6100	31.29	4.93	100		0.051814		Pf 0.340
1556	11'-11½	31.29	5.6	31.224		Sprinkler,		Pe -0.002
470	11'-11½			31.562		T(5'-8½)	6'-7	/ Pv
CM	1.6100	31.56	4.97	100		0.052625	0'-101⁄4	Pf 0.345
1539	11'-11½	31.56	5.6	31.752		Sprinkler,		Pe -0.002
	11'-11½			32.096		T(5'-8½)	6'-7	Pv
438								
🕶 • • • • • Route 7 • •		22.44	10.00	100		0.464044	41.017	Df 0.450
	1.0490 12'-11	33.14 33.14	12.30 5.6	100 35.016		0.464044 Sprinkler,		Pf 2.456

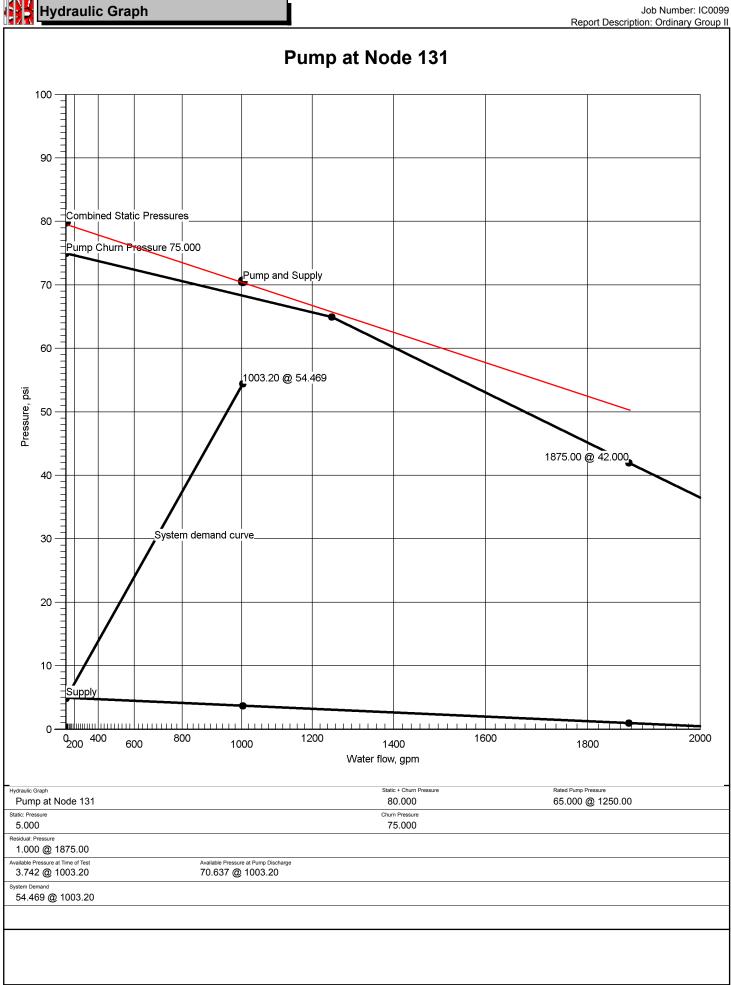
Pipe Type Downstream Upstream	Diameter Elevation	Flow Discharge	Velocity K-Factor	HWC Pt	Pn	Friction Los Fittings	S		Length Eq. Length Total Length	Press Sumi	
G	5.3480	500.00	7.14	150		0.011917			14'-8		1.081
14	2'-6	500.00		47.018		Hydrant,					3.035
41	-4'-6			51.133			(32'-0), T(30'-0)		90'-8		
G	6.9630	500.00	4.21	150		0.003296			73'-5		0.301
1	-4'-6			51.133					18'-0	-	
52	-4'-6			51.434		2EE(9'-0)			91'-5		
G	6.9630	529.42	4.46	150		0.003664			4'-11	Pf	0.033
52	-4'-6	29.42		51.434		Flow (q) from	n Route 9		4'-0		
53	-4'-6			51.467		PIV(4'-0)			8'-11		
G	6.4700	529.42	5.17	120		0.007917			1'-0	1	0.008
53	-4'-6			51.467						Ре	
54	-4'-6			51.475					1'-0		
G	6.9630	529.42	4.46	150		0.003664			223'-3		0.965
54	-4'-6			51.475					40'-0		
69	-4'-6			52.439		4EE(9'-0), PI	IV(4'-0)		263'-3		
G	6.4700	529.42	5.17	120		0.007917			1'-0		0.008
69	-4'-6			52.439						Pe	
70	-4'-6			52.447					1'-0		
IG	6.9630	529.42	4.46	150		0.003664			3'-11		0.014
70	-4'-6			52.447						Pe	
71 Davita 0	-4'-6			52.462					3'-11	Pv	
••••• Route 9 •			0.05	450		0.000047					
G	6.9630	29.42	0.25	<u>150</u> 51.431		0.000017			4'-1½		0.000
20	-4'-6								41 417	Pe	
19	-4'-6	00.40	0.00	51.431		0.000038			4'-1½	_	0.000
G 19	<u>6.4700</u> -4'-6	29.42	0.29	<u>120</u> 51.431		0.000036			1'-0 4'-0	1	0.000
18	-4-6 -4'-6			51.431		PIV(4'-0)			4 -0 5'-0		
IG	6.9630	29.42	0.25	150		0.000017			94'-5½		0.000
18	-4'-6	29.42	0.25	51.432		0.000017			94 -572 9'-0		0.002
50	-4'-6			51.433		EE(9'-0)			103'-5½		
<u>IG</u>	6.4700	29.42	0.29	120		0.000038					0.000
50	-4'-6	23.42	0.29	51.433		0.000000			4'-0		0.000
51	-4'-6			51.433		PIV(4'-0)			4-0 5'-0		
IG	6.9630	29.42	0.25	150		0.000017			4'-8	Df	0.001
51	-4'-6	20.72	0.20	51.433		0.0000.1			35'-0	Pe	0.001
52	-4'-6			51.434		T(35'-0)			39'-8		
quivalent Pipe Ler	ngths of Valves and	Fittings (C=120 or	nly)		C Valu	e Multiplier					
(Actual Inside	Diameter	۱ ^{4.87} –		Value	Of C	100	130	140	1	50
		e Inside Diameter	—) = Fi	actor		lying Factor	0.713	1.16	1.33		.51



ipe Type Diamet	er Flow	Velocity HWC		Friction Loss		Length	Pressure
Downstream Elevati Jpstream	on Discharge	K-Factor Pt	Pn	Fittings		Eq. Length Total Length	Summary
Pipe Type Legend		Units Legen	d			Fittings Legen	d
 Arm-Over Branch Line Cross Main Drop Dynamic Feed Main Feed Riser Miscellaneous Outrigger Riser Nipple Sprig Stand Pipe Underground 	Pt Total p Pn Norma Pf Pressu Pe Pressu	ot h-Williams Constant pressure at a point in a pi al pressure at a point in a ure loss due to friction be ure due to elevation differ ty pressure at a point in a	pipe tween points rence betwee		ALV AngV b b BaIV BFP BV C cplg Cr CV DPV E EE Ee1 Ee2 f fd FDC fE fEE flg FN fT g GloV GV Ho Hose HV Hyd LtE mecT Noz P1 P2 PIV PO PRV PRV PO PRV PC St T Tr U WirF WMV Z	Alarm Valve Angle Valve Bushing Ball Valve Backflow Prevente Butterfly Valve Cross Flow Turn 9 Coupling Cross Run Check Valve Deluge Valve Dry Pipe Valve 90° Elbow 45° Elbow 11¼° Elbow 22½° Elbow Flow Device Flex Drop Fire Department C 90° FireLock(TM) 1 45° FireLock(TM) 1 45° FireLock(TM) 1 Flange Floating Node FireLock(TM) 1 Elange Globe Valve Gate Valve Hose Hose Hose Hose Valve Hose Hose Valve Hose Hose Hose Valve Hose Hose Hose Valve Hose Hose Hose Valve Hose Hose Hose Hose Hose Hose Hose Hos	ornection Elbow Elbow g Valve lve

	Report Description: Ordinary Gr
s Number C0099	Design Engineer Brad Vokes
Name: 	Phone FAX 1-226-668-8168
tress 1	I-ZZO-000-0 100 State Certification/License Number
LOS ALAMOS NATIONAL LABS	AHJ
tress 3	LANL FPDO Job Site/Building
	Building 153
stem	Area of Application
D.200gpm/ft ²	1950.00ft² (Actual 1966.05ft²)
st Demanding Sprinkler Data 5.6 K-Factor 18.43 at 10.829	Hose Streams 500.00
verage Per Sprinkler Varies	Number Of Sprinklers Calculated 22
	System Flow Demand 1003.20
al Demand	1000.20
1003.20 pplies	Check Point Gauges
vode <u>Name Flow(gpm) Hose Flow(gpm)</u> Static(psi) <u>Residual(psi</u>	
62 Tank Supply 1875.00 5.000 1.000	
131 1250.00 Pump 75.000 65.000	
Pumps: Static = Churn (Pressure @ Zero Flow)	Tool: Cumply at Made 62 (4075-00-0-00-5-000-4-000)
Pumps: Static = Churn (Pressure @ Zero Flow) 0099 LANL TWF Rev 3	Tank Supply at Node 62 (1875.00, 0.00, 5.000, 1.000)

Н	ydraulic Sumr	mary								Job Number: IC0099 on: Ordinary Group I	
Job				-							
Job Number IC0099						Design Enginee Brad Vo					
Job Name: LANL TW	VF					State Certification	n/License Number				
Address 1	AMOS NATIONAL LA	BS				AHJ LANL F	PDO				
Address 2						Job Streebuilding Building 153					
Address 3						Drawing Name IC0099 LANL TWF Rev 3					
System						IC0099 Remote A		3			
Most Demanding S	Sprinkler Data Ctor 18.43 at 10.829	2				Occupancy	y Group II		Job Suffix		
Hose Allowance At		, 				Density	-		Area of Application	1000 05#2	
Additional Hose Su	upplies						DM/π ²		1950.00ft ² (Actual 1 Coverage Per Sprinkler	1966.05π²)	
<u>Node</u> Hydrant A	At Node 44		<u>(gpm)</u> 0.00			22 AutoPeak Resul	ts: Pressure For Remote Area(s) Adjacent To Most Remote A	Varies		
Total Hose Stream 500.00	ns										
System Flow Dema	nand	т	otal Water Required (Including H	Hose Allowance)							
1003.20			1003.20								
Maximum Velocity	tween nodes 338 and ^{Under Ground} ween nodes 73 and 7	2	olume capacity of Dry Pipes	1 Gallons							
Supplies											
		Hose Flow	Static	Residual	@	Flow	Available @	Total Demand	Required	Safety Margin	
Node 62	Name Tank Supply	(gpm)	(psi) 5.000	(psi) 1.000		(gpm) 875.00	(psi) (psi) () 3.742	(gpm) 1003.20	(psi) 0.000	(psi) 16.169	
131		Pump	75.000	65.000		250.00	70.637	1003.20	54.469	16.169	
Pumps: Sta	tic = Churn (Pressure @ Zei	ro Flow)									
Contractor											
Contractor	Contractor Number	er				Contact Nar			Contact Title		
Name of Contracto	IC0119 RN STATES FIRE PR					Phone	VOKES		DESI0 Extension	JNEK	
Address 1						FAX	68-8168				
5200 PAS Address 2	SADENA AVE NE, SU	JILEA				505-8 E-mail	84-1863				
Address 3							D.VOKES@WSFF	P.US			
	JERQUE, NM 87113					WED-SILE					





Summary Of Outflowing Devices

		Actual Flow	Minimum Flow	K-Factor	Pressure	Coverage
Device	9	(gpm)	(gpm)	(K)	(psi)	(Foot)
Hydrant	44	500.00	500.00	267.26	47.255	
Sprinkler	1508	19.72	18.43	5.6	12.403	92.15sqft
Sprinkler	1509	19.89	18.43	5.6	12.614	92.15sqf
Sprinkler	1510	20.45	18.43	5.6	13.341	92.15sqf
Sprinkler	1511	21.61	18.43	5.6	14.893	92.15sqf
Sprinkler	1512	23.51	18.43	5.6	17.622	92.15sq
Sprinkler	1513	26.25	18.43	5.6	21.970	92.15sq
Sprinkler	1514	31.56	18.43	5.6	31.752	92.15sq
Sprinkler	1516	17.96	14.82	5.6	10.291	74.10sqf
Sprinkler	1517	18.07	14.82	5.6	10.414	74.10sqf
Sprinkler	1518	18.43	18.43	5.6	10.829	92.15sqf
Sprinkler	1519	19.34	18.43	5.6	11.926	92.15sqf
Sprinkler	1520	21.10	18.43	5.6	14.192	92.15sqf
Sprinkler	1521	23.62	18.43	5.6	17.789	92.15sqf
Sprinkler	1522	26.98	18.43	5.6	23.208	92.15sqf
Sprinkler	1523	33.14	14.82	5.6	35.016	74.10sqf
Sprinkler	1525	19.55	18.43	5.6	12.184	92.15sqf
Sprinkler	1526	19.71	18.43	5.6	12.393	92.15sqf
Sprinkler	1527	20.27	18.43	5.6	13.108	92.15sqf
Sprinkler	1528	21.42	18.43	5.6	14.635	92.15sqf
Sprinkler	1529	23.31	18.43	5.6	17.320	92.15sqf
Sprinkler	1530	26.03	18.43	5.6	21.598	92.15sq
Sprinkler	1531	31.29	18.43	5.6	31.224	92.15sg

➡ Most Demanding Sprinkler Data

Pipe Type	Diameter	Flow	Velocity	нмс	Friction Loss	Length	Pres	ssure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length		nmary
Upstream						Total Length		,
••••• Route 1 •	••••						-	
M	1.6100	54.46	8.58	100	0.144442	7'-6	Pf	1.083
1518	13'-01⁄2	18.43	5.6	10.829	Sprinkler			0.014
1519	13'-0			11.926		7'-6		
M	1.6100	73.80	11.63	100	0.253413	8'-10½		2.249
1519	13'-0	19.34	5.6	11.926	Sprinkler			0.017
1520	12'-11½			14.192	·	8'-10½		
CM	1.6100	94.90	14.96	100	0.403486	8'-10½		3.581
1520	12'-11½	21.10	5.6	14.192	Sprinkler			0.017
1521	12'-11			17.789		8'-10½		
M	1.6100	118.52	18.68	100	0.608692	8'-101/2		5 402
1521	12'-11	23.62	5.6	17.789	Sprinkler	0 10/2		0.017
1522	12'-10½	20.02	0.0	23.208	opinition	8'-10½		0.017
CM	1.6100	145.50	22.93	100	0.889550	9'-8		14.316
1522	12'-10½	26.98	5.6	23.208	Sprinkler,			0.733
352	11'-2½	20.00	0.0	38.258	LtE(1'-5), mecT(5'-0)	16'-1		0.700
SS2	4.0260	340.22	8.57	100	0.049334			0.510
			0.07		Flow (g) from Route 2	10-4		
352	11'-2½ 11' 2	194.72		38.258		401.4		0.008
338	11'-2	500.00	40.00	38.776	0 101772	10'-4		0 700
228	4.0260	503.20	12.68	100	0.101772		Pf	
338	11'-2	162.99		38.776	Flow (q) from Route 3	26'-9½		4.217
97	1'-5½			46.715	2fE(4'-10), DPV, CV(15'-8),	36'-7	P۷	
					PIV(1'-5)			
IG	6.4000	503.20	5.02	120	0.007599	6'-5½		
97	1'-5½			46.715				2.576
13	-4'-6			49.755	3E(18'-2½)	61'-0		
IG	5.3480	503.20	7.19	150	0.012059	107'-6½	Pf	1.912
13	-4'-6			49.755				-0.000
35	-4'-6			51.667	E(14'-0), EE(7'-0), T(30'-0)	158'-6½	Ρv	
IG	6.9630	51.43	0.43	150	0.000049	51'-9	Pf	0.003
35	-4'-6			51.667			Pe	
50	-4'-6			51.669		51'-9	Ρv	
JG	6.4700	51.43	0.50	120	0.000106			0.001
50	-4'-6			51.669		4'-0		
51	-4'-6			51.670	PIV(4'-0)	5'-0		
JG	6.9630	51.43	0.43	150	0.000049			0.002
51	-4'-6	51.45	0.45	51.670	0.000010	35'-0		0.002
52	-4'-6			51.672	T(35'-0)	39'-8		
JG	6.9630	551.43	4.65	150	0.003951			0.035
52	-4'-6	500.00	4.05	51.672	Flow (q) from Route 8	4-11		0.035
53		300.00		51.707	PIV(4'-0)	8'-11		
	-4'-6	554.40	5.00		0.008537		_	0.000
IG	6.4700	551.43	5.38	120	0.008537	1-0		0.009
53	-4'-6			51.707			Pe	
54	-4'-6			51.716		1'-0		
IG	6.9630	551.43	4.65	150	0.003951			1.040
54	-4'-6			51.716		40'-0		
69	-4'-6			52.756	4EE(9'-0), PIV(4'-0)	263'-3		
IG	6.4700	551.43	5.38	120	0.008537	1'-0		0.009
69	-4'-6			52.756			Ре	
70	-4'-6			52.764		1'-0	Ρv	
IG	6.9630	551.43	4.65	150	0.003951	3'-11	Pf	0.015
70	-4'-6			52.764			Pe	
71	-4'-6			52.780		3'-11	Ρv	
IG	6.9630	1003.20	8.45	150	0.011954			0.105
71	-4'-6	451.77		52.780	Flow (q) from Route 9	4'-0		
72	-4'-6			52.885	PIV(4'-0)	8'-91/2		
IG	6.4700	1003.20	9.79	120	0.025830		_	0.026
72	-4'-6			52.885			Pe	
73	-4'-6			52.910		1'-0		
G	6.9630	1003.20	8.45	150	0.011954			2.722
73	-4'-6	1000.20	0.70	52.910				0.000
75	-4'-6			55.632	EE(9'-0), T(35'-0), E(18'-0)	227'-8		0.000
		1002.00	6 40		0.009294		_	1 = 40
M	7.9810	1003.20	6.43	120	0.003234			1.546
75	-4'-6			55.632				-2.710
131	1'-9			54.469	2LtE(13'-0), 2T(35'-0), BV(12'-0),	166'-4	Pv	
					CV(45'-0)			
ump			Velocity			_		
131		1003.20		54.469	Rating: 65.000 @ 1250.00			
129		Q=1003.20	6.43	-13.874	Churn Pressure: 75.000			
M	7.9810	1003.20	6.43	120	0.009294			0.539
129	1'-9			-13.874		52'-0	Pe	-1.409
	5'-0			-14.744	GV(4'-0), LtE(13'-0), T(35'-0)	58'-0		

Pipe Type	Diameter	Flow	Velocity	нмс		Friction Loss	Length	Pres	ssure
Downstream Upstream	Elevation	Discharge	K-Factor	Pt	Pn	Fittings	Eq. Length Total Length	Sun	nmary
M	11.9380	1003.20	2.88	120		0.001308		Pf	0.367
124	5'-0	1000.20	2.00	-14.744			197'-0		
62	0'-6			-12.426		sCV(65'-0), GV(6'-0), 7LtE(18'-0), S	280'-8	Pv	
		0.00				Hose Allowance At Source	_		
62		1003.20							
••••• Route 2 •									
M	1.6100	19.55	3.08	100		0.021697	8'-10½		
1525 1526	12'-2 12'-2	19.55	5.6	12.184 12.393		Sprinkler	8'-10½		0.016
CM	1.6100	39.26	6.19	100		0.078836	8'-101/2	_	0.700
1526	12'-2	19.71	5.6	12.393		Sprinkler			0.016
1527	12'-1½			13.108			8'-10½		
CM	1.6100	59.54	9.38	100		0.170308	8'-10½		1.511
1527 1528	12'-1½	20.27	5.6	13.108		Sprinkler	8'-10½		0.016
 CM	<u>12'-1</u> 1.6100	80.96	12.76	14.635 100		0.300738	8'-101/2		2 660
1528	12'-1	21.42	5.6	14.635		Sprinkler	- 0-10/2		0.016
1529	12'-0½	_		17.320		-	8'-10½		
M	1.6100	104.26	16.43	100		0.480232	8'-10½	Pf	
1529	12'-0½	23.31	5.6	17.320		Sprinkler			0.016
1530	12'-0	100.00	00 50	21.598		0.725228	8'-10½		0.07
CM 1530	<u>1.6100</u> 12'-0	<u>130.29</u> 26.03	<u>20.53</u> 5.6	<u>100</u> 21.598		0.725238 Sprinkler,		Pf	9.951 0.014
367	12-0 11'-11½	20.03	5.0	21.596 31.562		T(5'-8½)	13'-8½		0.014
CM	1.6100	161.58	25.46	100		1.079996		Pf	6.217
367	11'-11½	31.29	20.10	31.562		Flow (q) from Route 5			0.332
366	11'-2½			38.111		mecT(5'-0)	5'-9		
M	4.0260	161.58	4.07	100		0.012443	8'-4	1	0.104
366	11'-2½			38.111					0.006
353	11'-2½			38.221			8'-4		
CM	4.0260	194.72	4.91	100		0.017572 Flow (g) from Route 7	2'-0		0.035
353 352	11'-2½ 11'-2½	33.14		38.221 38.258		Flow (q) Iron Roule 7	2'-0		0.002
••••• Route 3 •				50.250			2-0		
CM	1.6100	19.72	3.11	100		0.022057	8'-10½	Pf	0.196
1508	12'-2	19.72	5.6	12.403		Sprinkler		Pe	0.016
1509	12'-1½			12.614			8'-10½	Ρv	
CM	1.6100	39.61	6.24	100		0.080141	8'-10½		
1509	12'-1½	19.89	5.6	12.614		Sprinkler	01.401/		0.016
<u>1510</u> CM	<u>12'-1</u> 1.6100	60.07	9.47	<u>13.341</u> 100		0.173120	8'-10½		1 5 2 6
1510	12'-1	20.45	5.6	13.341		Sprinkler	8'-10½		0.016
1511	12'-0½	20.40	0.0	14.893			8'-10½		0.010
CM	1.6100	81.68	12.87	100		0.305687	8'-10½		2.713
1511	12'-0½	21.61	5.6	14.893		Sprinkler			0.016
1512	12'-0½			17.622			8'-10½	_	
CM	1.6100	105.18	16.58	100		0.488098	8'-10½		
1512	12'-0½	23.51	5.6	17.622		Sprinkler	9' 101/		0.016
1513	12'-0	131.43	20.71	21.970 100		0.737051	8'-10½		10.11
CM 1513	<u>1.6100</u> 12'-0	26.25	<u>20.71</u> 5.6	21.970		Sprinkler,			0.014
335	11'-11½	_0.20	0.0	32.096		T(5'-8½)	13'-8½		0.014
CM	1.6100	162.99	25.69	100		1.097452	0'-9½		6.339
335	11'-11½	31.56		32.096		Flow (q) from Route 6	5'-0	Ре	0.340
338	11'-2			38.776		mecT(5'-0)	5'-9½	Ρv	
••••• Route 4 •		17.00				0.040500			
CM 1516	1.6100	17.96	2.83	100		0.018560 Sprinkler			0.111
1516 1517	13'-1 13'-0½	17.96	5.6	10.291 10.414		Opinikier	6'-0		0.011
CM	1.6100	36.04	5.68	100		0.067275			0.404
1517	13'-01/2	18.07	5.6	10.414		Sprinkler			0.011
1518	13'-0½			10.829			6'-0		
••••• Route 5 •									
CM	1.6100	31.29	4.93	100		0.051814	0'-10½		
1531	11'-11½	31.29	5.6	31.224		Sprinkler,	5'-8½		-0.00
367	11'-11½			31.562		T(5'-8½)	6'-7	PV	
•••••• Route 6• CM	1.6100	31.56	4.97	100		0.052625	0'-10½	Df	0 345
1514	11'-11½	31.56	<u>4.97</u> 5.6	31.752		Sprinkler,	5'-8½		
335	11'-11½	000	0.0	32.096		T(5'-8½)	6'-7		5.00

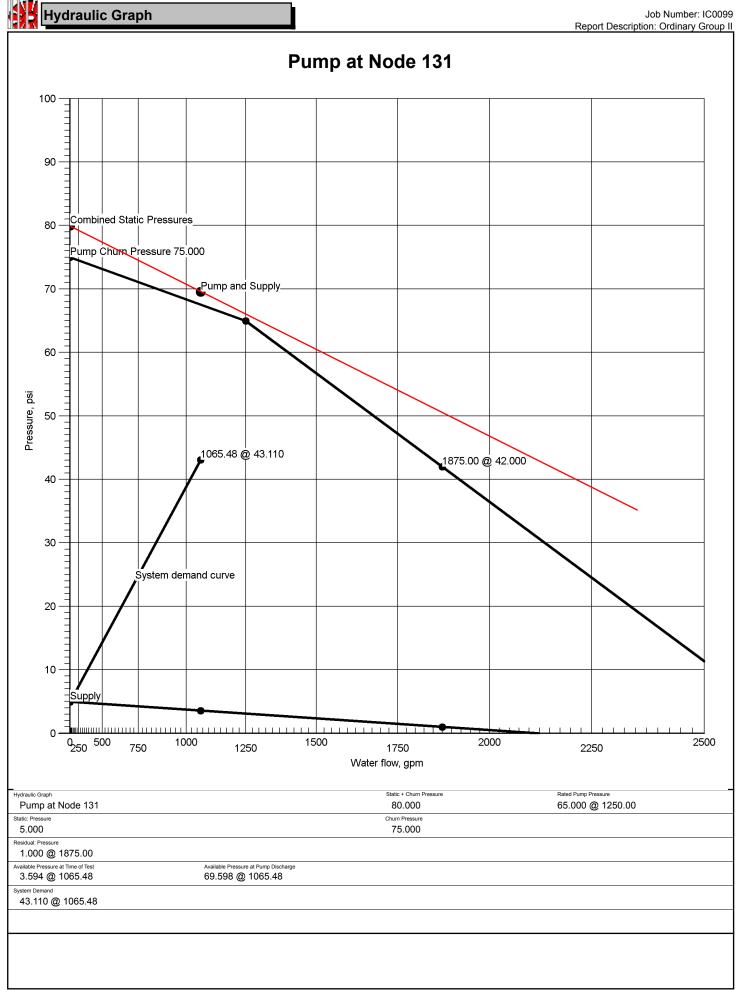
Ріре Туре	Diameter	Flow	Velocity	HWC		Friction Lo	ss		Length		ssure
Downstream Upstream	Elevation	Discharge	K-Factor	Pt	Pn	Fittings			Eq. Length Total Length	Summary	
BL	1.0490	33.14	12.30	100		0.464044			1'-8½	Pf	2.456
1523	12'-11	33.14	5.6	35.016		Sprinkler,			3'-7	Pe	0.749
353	11'-2½			38.221		mecT(3'-7)			5'-3½	Pv	
••••• Route 8	• • • • •										
IG	5.3480	500.00	7.14	150		0.011917			14'-8	Pf	1.081
44	2'-6	500.00		47.255		Hydrant,			76'-0	Pe	3.035
41	-4'-6			51.370		E(14'-0), C\	/(32'-0), T(30'-0))	90'-8	Pv	
JG	6.9630	500.00	4.21	150		0.003296		,	73'-5		0.301
41	-4'-6			51.370					18'-0		
52	-4'-6			51.672		2EE(9'-0)			91'-5		
••••• Route 9	• • • • •										
JG	6.9630	451.77	3.81	150		0.002732			63'-0	Pf	0.183
24	-4'-6			51.997					4'-0		
25	-4'-6			52.180		PIV(4'-0)			67'-0		
JG	6.4700	451.77	4.41	120		0.005904			1'-0	_	0.006
25	-4'-6			52.180						Pe	0.000
26	-4'-6			52.186					1'-0	-	
JG	6.9630	451.77	3.81	150		0.002732			119'-6		0.433
26	-4'-6		0.01	52.186					39'-0		000
61	-4'-6			52.619		T(35'-0), Pl'	V(4'-0)		158'-6		
JG	6.4700	451.77	4.41	120		0.005904	(-)		1'-0		0.006
61	-4'-6	101.11		52.619						Pe	0.000
63	-4'-6			52.625					1'-0	-	
JG	6.9630	451.77	3.81	150		0.002732			21'-6		0.154
63	-4'-6	101.11	0.01	52.625					35'-0		0.101
71	-4'-6			52.780		T(35'-0)			56'-6		
••••• Route 10	-			02.100		.(
G	6.9630	451.77	3.81	150		0.002732			42'-8½	Pf	0 152
35	-4'-6	401.11	0.01	51.667		0.002.02			13'-0		0.102
18	-4'-6			51.819		EE(9'-0), PI	V(4'-0)		55'-8½		
JG	6.4700	451.77	4.41	120		0.005904	x -7		1'-0		0.006
18	-4'-6	101.11		51.819					10	Pe	5.000
19	-4'-6			51.825					1'-0		
JG	6.9630	451.77	3.81	150		0.002732			57'-0		0.167
19	-4'-6	101.11	0.01	51.825					4'-0		5.101
22	-4'-6			51.992		PIV(4'-0)			61'-0		
IG	6.4700	451.77	4.41	120		0.005904			1'-0		0.006
22	-4'-6	101.11		51.992					10	Pe	5.000
24	-4'-6			51.997					1'-0		
		l Fittings (C=120 onl	v)		C. Valu	e Multiplier					
ganalent Fipe Le		a i naings (0=120 011	.,								
1	Actual Inside	Diameter	4.87		Value	Of C	100	130	140		150
(e Inside Diameter	—) = Fa	actor		lying Factor	0.713	1.16	1.33		1.51



Hydraulic A					R	eport Description:	-
	iameter Flow levation Discharg	Velocity e K-Factor	HWC Pt Pn	Friction Loss Fittings		Length Eq. Length Total Length	Pressure Summary
Pipe Type Legend		l	Jnits Legend			Fittings Legen	d
O Arm-Over L Branch Line M Cross Main N Drain R Drop Y Dynamic M Feed Main R Feed Riser IS Miscellaneous 8 Outrigger IN Riser Nipple P Sprig T Stand Pipe IG Underground	Diameter Elevation Flow Discharge Velocity Pressure Length Friction Loss HWC Pt Pn Pf Pe Pv	Inch Foot gpm gpm fps psi Foot psi/Foot Hazen-Williams Co Total pressure at a Normal pressure at Pressure loss due t	nstant point in a pipe a point in a pipe o friction between p evation difference be	bints tween indicated points	AngV b BaIV BFP BV C cplg Cr CV DPV E EE Ee1 Ee2 f fd FDC fE fg FN fT g GloV GV Ho Hose HV Hyd LtE mecT Noz P1 P2 PIV PO PRV PRV PRV Spr St T Tr U WirF WMV	Alarm Valve Angle Valve Bushing Ball Valve Backflow Prevente Butterfly Valve Cross Flow Turn 9 Coupling Cross Run Check Valve Deluge Valve 90° Elbow 45° Elbow 45° Elbow 11¼° Elbow 22½° Elbow Flow Device Flex Drop Fire Department C 90° FireLock(TM) 1 Flange Floating Node FireLock(TM) Tee Gauge Globe Valve Gate Valve Hose Hose Hose Valve Hose Hose Valve Hose Kozzle Pump In Pump Out Post Indicating Val Pressure Relief Va Reducer/Adapter Supply Swing Check Valve Sprinkler Strainer Tee Flow Turn 90° Tee Run Union Wirsbo Water Meter Valve Cap	onnection Elbow Elbow

Hydraulic Overview	Jo Report Description	n: Ordinary Gro
2		
Number C0099	Brad Vokes	
Name: ANL TWF	Phone FAX 1-226-668-8168	
Iress 1 LOS ALAMOS NATIONAL LABS	State Certification/License Number	
iress 2		
rress 3	Job Site/Building	
atom	Building 154	
stem	Area of Application	
).200gpm/ft² st Demanding Sprinkler Data	1950.00ft ² (Actual 1994.34ft ²) Hose Streams	
5.6 K-Factor 18.43 at 10.829	500.00	
erage Per Sprinkler Varlies	Number Of Sprinklers Calculated 27	
	System Flow Demand 1065.51	
al Demand 1065.51		
pplies	Check Point Gauges	
lode <u>Name Flow(gpm)</u> Hose Flow(gpm) Static	psi) Residual(psi) Identifier Pressure(psi) K-Factor(K)	Flow(gpm)
62 Tank Supply 1875.00 5.0		
131 1250.00 Pump 75.0	00 65.000	
Pumps: Static = Churn (Pressure @ Zero Flow) 2099 LANL TWF Rev 3	Tank Supply at Node 62 (1875.00, 0.00, 5.000, 1.000)	

Hy	ydraulic Sumi	mary							Report		ob Number: IC009 n: Ordinary Group	
Job												
Job Number IC0099						Design Enginee Brad Vo						
Job Name: LANL TV	VF					State Certification	n/License Number					
Address 1	AMOS NATIONAL LA	BS				AHJ	PDO					
Address 2		20				Job Store Building Building 154						
Address 3						Drawing Name	-					
System						IC0099 Remote A	LANL TWF Rev	3		_		
Most Demanding S					-	Occupancy			Job Suffix			
5.0 K-Fa	ictor 18.43 at 10.82	9				Density	y Group II		Area of Application			
Additional Hose S	upplies					0.200gp Number Of Sprin	om/ft ²		1950.00ft ² Coverage Per Sprink	-	94.34ft²)	
Node			<u>ow(gpm)</u>			27			Varie			
Hydrant	At Node 44	ţ	500.00			AutoPeak Resul	Its: Pressure For Remote Area	(s) Adjacent 10 Most Remote	Area			
0.000 Maximum Velocity 17.99 be Maximum Velocity	re Unbalance In Loops / Above Ground tween nodes 145 and		Total Water Required (Including 1065.51	Hose Allowance)								
Volume capacity o	of Wet Pipes		Volume capacity of Dry Pipes									
Supplies			54gal									
		Hose Flo	w Static	Residual	@	Flow	Available	Total Deman	d Re	quired	Safety Margin	
Node	Name	(gpm)	(psi) 5.000	(psi) 1.000	-	(gpm)	(psi)	(gpiii)		(psi) .000	(psi) 26.488	
62 131	Tank Supply	Pump	75.000	65.000		1875.00 1250.00	3.594 69.598	1065.48 1065.48		3.110	26.488	
Pumps: Sta	atic = Churn (Pressure @ Ze	ro Flow)										
Contractor												
	Contractor Numb	er				Contact Nan BRAD	D VOKES			Contact Title DESIG	NER	
Name of Contract	RN STATES FIRE PR	OTECTION	1			Phone 226-6	68-8168			Extension		
Address 1 5200 PA	SADENA AVE NE, SI	JITE A				FAX 505-8	84-1863			1		
Address 2						E-mail						
Address 3						BRAL Web-Site	D.VOKES@WSF	r.uð				
ALBUQU	JERQUE, NM 87113											





Summary Of Outflowing Devices

Davia		Actual Flow	Minimum Flow	K-Factor	Pressure	Coverage
Devic		(gpm)	(gpm)	(K)	(psi)	(Foot)
Hydrant	44	500.00	500.00	267.26	35.245	
Sprinkler	1201	21.03	14.82	5.6	14.109	74.10
Sprinkler	1202	22.18	14.82	5.6	15.685	74.10
Sprinkler	1203	23.66	14.82	5.6	17.853	74.10
Sprinkler	1204	25.39	14.82	5.6	20.558	74.10
Sprinkler	1205	18.78	18.43	5.6	11.244	92.15 ²
Sprinkler	1206	18.84	18.43	5.6	11.312	92.15 ²
Sprinkler	1207	19.01	18.43	5.6	11.520	92.15²
Sprinkler	1208	19.35	18.43	5.6	11.943	92.15 ²
Sprinkler	1209	19.93	18.43	5.6	12.662	92.15 ²
Sprinkler	1211	26.46	14.82	5.6	22.332	74.10
Sprinkler	1212	26.53	14.82	5.6	22.448	74.10
Sprinkler	1213	26.75	14.82	5.6	22.824	74.10
Sprinkler	1216	18.74	18.43	5.6	11.194	92.15 ²
Sprinkler	1217	19.30	18.43	5.6	11.877	92.15²
Sprinkler	1218	20.13	18.43	5.6	12.916	92.15 ²
Sprinkler	1219	20.89	18.43	5.6	13.917	92.15 ²
Sprinkler	1220	22.36	18.43	5.6	15.941	92.15 ²
Sprinkler	1223	18.58	18.43	5.6	11.004	92.15 ²
Sprinkler	1224	18.63	18.43	5.6	11.072	92.15²
Sprinkler	1225	18.80	18.43	5.6	11.275	92.15²
Sprinkler	1226	19.15	18.43	5.6	11.690	92.15²
Sprinkler	1227	19.71	18.43	5.6	12.394	92.15²
Sprinkler	1228	22.62	18.43	5.6	16.320	92.15²
Sprinkler	1229	23.70	18.43	5.6	17.910	92.15²
Sprinkler	1602	18.23	14.82	5.6	10.602	74.10
Sprinkler	1603	18.29	14.82	5.6	10.671	74.10
Sprinkler	1604	18.43	18.43	5.6	10.829	92.15 ²

➡ Most Demanding Sprinkler Data

Hydraulic Analysis

Pipe Type	Diameter	Flow	Velocity	HWC	Friction Loss	Length	Pres	sure
Downstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length		mary
Jpstream	Liovation	Dioonargo	it i dotoi		1 111190	Total Length	Cam	, nai y
••••• Route 1 •	••••							
<u>/////////////////////////////////////</u>	2.0670	54.96	5.25	100	0.043496	7'-6½	Pf	0.328
1604	13'-1	18.43	5.6	10.829	Sprinkler			0.038
216	13'-0			11.194	•	7'-6½		
Λ	2.0670	73.69	7.05	100	0.074844	8'-10½		0.664
216	13'-0	18.74	5.6	11.194	Sprinkler			0.018
217	12'-11½			11.877		8'-10½	Pv	
M	2.0670	92.99	8.89	100	0.115092	8'-10½		1.021
1217	12'-11½	19.30	5.6	11.877	Sprinkler			0.018
1218	12'-11			12.916		8'-10½	Pv	
M	2.0670	113.12	10.82	100	0.165370			0.992
1218	12'-11	20.13	5.6	12.916	Sprinkler	_		0.008
1219	12'-10½			13.917		6'-0		
М	2.0670	134.01	12.81	100	0.226267	8'-10½		2.008
219	12'-10½	20.89	5.6	13.917	Sprinkler			0.017
1220	12'-101/2			15.941		8'-10½		
M	2.0670	156.37	14.95	100	0.301021	13'-1½		7 702
220	12'-10½	22.36	5.6	15.941	Sprinkler,	12'-5½		
179	11'-2½			24.355	fT(6'-0½), mecT(6'-5)	25'-7		
M	4.0260	424.28	10.69	100	0.074227			2.081
179	11'-2½	267.91		24.355	Flow (q) from Route 3			0.019
200	11'-2			26.454	2fE(4'-10)	28'-01/2		2.010
M	4.0260	565.48	14.25	100	0.126291	7'-11½		3 780
200	11'-2	141.20	17.20	26.454	Flow (q) from Route 2	21'-11½		
84	1'-5½			34.451	fE(4'-10), DPV, CV(15'-8),	29'-11		
- ·	1 0/2			01.101	PIV(1'-5)	20-11		
G	6.4000	565.48	5.64	120	0.009430	5'-11½	Pf	0 228
84	1'-5½	303.40	5.04	34.451	0.000100	18'-2½		
16	-4'-6			37.255	E(18'-2½)	24'-1½		2.070
G	5.3480	565.48	8.08	150	0.014964	108'-11½		2 304
16	-4'-6	505.46	0.00	37.255	0.014304			-0.000
36	-4'-6			39.649	E(14'-0), EE(7'-0), T(30'-0)	159'-11½		-0.000
G	6.9630	86.26	0.73	150	0.000128			0.006
36	-4'-6	00.20	0.75	39.649	0.000120	47-9	P	0.000
50	-4'-6			39.655		47'-9		
	6.4700	86.26	0.84	120	0.000276			0.001
IG 50	-4'-6	00.20	0.04	39.655	0.000270	4'-0		0.001
	-4-0 -4'-6			39.656	PIV(4'-0)	5'-0		
51	6.9630	00.00	0.72	150	0.000128			0.005
G 51	-4'-6	86.26	0.73	39.656	0.000128	4 -8 35'-0		0.005
52	-4 -0 -4'-6			39.662	T(35'-0)	39'-8		
		500.00	4.04		0.004425			0.020
G 52	<u>6.9630</u> -4'-6	<u>586.26</u> 500.00	4.94	150	Flow (g) from Route 7	4-11		0.039
52 53		500.00		39.662		8'-11		
	-4'-6	500.00	F 70	39.701	PIV(4'-0) 0.009561			0.010
G 53	<u> </u>	586.26	5.72	<u>120</u> 39.701	0.009501	- 1-0	Pf	0.010
						1.0	Pe	
54	-4'-6	E90.00	4.04	39.711	0.004425	1'-0		1 405
IG	6.9630	586.26	4.94	150	0.004420	223'-3		1.165
54	-4'-6			39.711		40'-0		
69	-4'-6	500.00	F 70	40.876	4EE(9'-0), PIV(4'-0)	263'-3		0.040
G	6.4700	586.26	5.72	120	0.009561			0.010
69 70	-4'-6			40.876		41.0	Pe	
70	-4'-6	500.00	4.04	40.885	0.001125	1'-0		0.0
G	6.9630	586.26	4.94	150	0.004425		1	0.017
70	-4'-6			40.885			Pe	
71	-4'-6			40.902	0.010000	3'-11		
G	6.9630	1065.48	8.98	150	0.013363	4'-9½		0.117
71	-4'-6	479.21		40.902	Flow (q) from Route 10	4'-0		
72	-4'-6			41.020	PIV(4'-0)	8'-9½		
G	6.4700	1065.48	10.40	120	0.028874			0.029
72	-4'-6			41.020			Ре	
73	-4'-6			41.049		1'-0		
G	6.9630	1065.48	8.98	150	0.013363	165'-8		
73	-4'-6			41.049				0.000
75	-4'-6			44.091	EE(9'-0), T(35'-0), E(18'-0)	227'-8		
N	7.9810	1065.48	6.83	120	0.010389			1.728
75	-4'-6			44.091		153'-0	Pe	-2.710
131	1'-9			43.110	2LtE(13'-0), 2T(35'-0), BV(12'-0),	166'-4	Pv	
					CV(45'-0)			
ımp			Velocity					
131		1065.48		43.110	Rating: 65.000 @ 1250.00			
129		Q=1065.48	6.83	-24.449	Churn Pressure: 75.000		1	

Pipe Type	Diameter	Flow	Velocity	HWC	Friction Loss	Length		sure
Downstream Upstream	Elevation	Discharge	K-Factor	Pt Pn	Fittings	Eq. Length Total Length	Sum	mary
M	7.9810	1065.48	6.83	120	0.010389		Pf	0.602
129	1'-9			-24.449				-1.409
124	5'-0			-25.255	GV(4'-0), LtE(13'-0), T(35'-0)	58'-0		
M	11.9380	1065.48	3.05	120	0.001462	83'-8		0.410
124	5'-0			-25.255		197'-0 280'-8		1.951
62	0'-6			-22.894	sCV(65'-0), GV(6'-0), 7LtE(18'-0), S	280-8	PV	
		0.00			Hose Allowance At Source			
62		1065.48				_		
••••• Route 2	••••							
М	2.0670	18.58	1.78	100	0.005848	8'-10½		0.052
1223	12'-3	18.58	5.6	11.004	Sprinkler			0.016
1224	12'-2½			11.072	0.001110	8'-10½		
M	2.0670	37.21	3.56	100	0.021142	8'-10½		0.188
1224 1225	12'-2½ 12'-2	18.63	5.6	11.072 11.275	Sprinkler	8'-10½		0.016
M	2.0670	56.01	5.36	100	0.045058	8'-101/2	_	0.400
1225	12'-2	18.80	5.6	11.275	Sprinkler			0.400
1226	12'-1½		-	11.690	-	8'-10½		
M	2.0670	75.16	7.19	100	0.077626	8'-10½	Pf	0.689
1226	12'-1½	19.15	5.6	11.690	Sprinkler			0.015
1227	12'-1			12.394		8'-10½	_	
M	2.0670	94.87	9.07	100	0.119443	2'-0½		1.393
1227 212	12'-1	19.71	5.6	12.394	Sprinkler, f = (2 e) = T(7 11())	9'-7½ 11'-8		0.003
212 CM	12'-1 2.0670	55.64	5.32	13.791 100	fE(2'-6), T(7'-1½) 0.044510	0'-5½		0.449
212	12'-1	55.04	5.32	13.791	0.044310			-0.186
198	12'-6½			14.053	fE(2'-6), T(7'-1½)	10'-1		-0.100
M	2.0670	94.87	9.07	100	0.119443			1.319
198	12'-6½	39.23		14.053	Flow (q) from Route 8			0.004
199	12'-6			15.376	fE(2'-6), T(7'-1½)	11'-0½	Pv	
CM	2.0670	55.64	5.32	100	0.044510	0'-5½		0.449
199	12'-6			15.376				0.186
213	12'-1			16.011	fE(2'-6), T(7'-1½) 0.119443	10'-1		
213	<u>2.0670</u> 12'-1	<u>94.87</u> 39.23	9.07	<u>100</u> 16.011	Flow (q) from Route 9	2'-6½		0.304 0.005
1228	12-1	39.23		16.320	now (q) nom route 9	2'-6½		0.005
CM	2.0670	117.50	11.23	100	0.177412	8'-101/2		1.575
1228	12'-1	22.62	5.6	16.320	Sprinkler	0 10/2		0.016
1229	12'-0½			17.910		8'-10½		
CM	2.0670	141.20	13.50	100	0.249234	20'-3½		8.169
1229	12'-0½	23.70	5.6	17.910	Sprinkler,	12'-5½		0.375
200	11'-2			26.454	fT(6'-0½), mecT(6'-5)	32'-91/2	Pv	
••••• Route 3		10 70	1.00	100	0.005000	01.404/		0.050
CM	2.0670	18.78	1.80	100	0.005966 Sprinkler	8'-10½		
1205 1206	12'-2 12'-1½	18.78	5.6	11.244 11.312	Spinikier	8'-10½		0.016
CM	2.0670	37.61	3.60	100	0.021568	8'-101/2		0 191
1206	12'-1½	18.84	5.6	11.312	Sprinkler			0.016
1207	12'-1	-	-	11.520	-	8'-10½		
M	2.0670	56.62	5.41	100	0.045964	8'-10½	_	0.408
1207	12'-1	19.01	5.6	11.520	Sprinkler			0.016
1208	12'-0½			11.943	0.070.105	8'-10½	_	
CM	2.0670	75.97	7.26	100	0.079185	8'-10½		
1208 1209	12'-0½ 12' 01/	19.35	5.6	11.943 12.662	Sprinkler	01 401/		0.016
1209 CM	12'-0½ 2.0670	95.90	9.17	12.662 100	0.121839	8'-10½	_	1.482
1209	12'-01/2	19.93	5.6	12.662	Sprinkler,			-0.035
1201	12'-1			14.109	2fE(2'-6)	12'-2		2.000
M	2.0670	116.93	11.18	100	0.175841	8'-10½	_	1.561
1201	12'-1	21.03	5.6	14.109	Sprinkler		Ре	0.016
1202	12'-1			15.685		8'-10½		
М	2.0670	139.11	13.30	100	0.242470	8'-10½		
1202	12'-1	22.18	5.6	15.685	Sprinkler			0.016
1203	12'-0½	400 77	45.50	17.853	0 204027	8'-10½		0.005
M	2.0670	162.77	15.56	100	0.324237 Sprinkler,			2.820
1203 153	12'-0½ 12'-01∕2	23.66	5.6	17.853 20.678	Sprinkier, fT(6'-0½)	6'-0½ 8'-8½		0.005
153 M	12'-0½ 2.0670	188.17	17.99	20.678	0.423963		_	3.054
153	12'-01/2	25.39	17.33	20.678	Flow (q) from Route 5			0.341
	11'-3	20.00		24.073	mecT(6'-5)	7'-2½		0.041

Hydraulic Analysis

Pipe Type	Diameter	Flow	Velocity	HWC		Friction Loss	Length		ssure
Downstream Upstream	Elevation	Discharge	K-Factor	Pt	Pn	Fittings	Eq. Length Total Length		nmary
M	4.0260	188.17	4.74	100		0.016493	6'-0		0.099
145	11'-3			24.073					0.005
172	11'-2½			24.176		0.001710	6'-0		
M	4.0260	267.91	6.75	100		0.031710	5'-6		0.174
172 179	11'-2½ 11'-2½	79.75		24.176 24.355		Flow (q) from Route 6	EL G		0.004
••••• Route 4 •				24.355			5'-6	PV	
CM	2.0670	18.23	1.74	100		0.005650	6'-0	Df	0.034
1602	13'-3	18.23	5.6	10.602		Sprinkler			0.034
1603	13'-2	10.25	5.0	10.671		oprinder	6'-0		0.000
CM	2.0670	36.53	3.49	10.071		0.020431	6'-0		0.123
1603	13'-2	18.29	5.6	10.671		Sprinkler			0.123
1604	13'-1	10.20	0.0	10.829		opinition	6'-0		0.000
••••• Route 5 •				10.020					
	2.0670	25.39	2.43	100		0.010425	6'-6	Df	0.131
1204	12'-0	25.39	5.6	20.558		Sprinkler,			-0.011
153	12'-0½	20.00	5.0	20.678		fT(6'-0½)	12'-6½		-0.011
••••• Route 6 •				20.070			12 0/2		
CM	2.0670	26.46	2.53	100		0.011255	8'-10½	Pf	0.100
1211	11'-11½	26.46	5.6	22.332		Sprinkler	0-10/2		0.100
1212	11'-11	20.70	0.0	22.332		Spinition	8'-10½		0.010
CM	2.0670	53.00	5.07	100		0.040670	8'-101/2		0 361
1212	11'-11	26.53	5.6	22.448		Sprinkler	0-10/2		0.016
1212	11'-11	20.00	0.0	22.440			8'-10½		0.010
CM	2.0670	79.75	7.62	100		0.086622			1.058
1213	11'-11	26.75	5.6	22.824		Sprinkler,			0.294
172	11'-2½	20.10	0.0	22.024		fE(2'-6), mecT(6'-5)	12'-2½		0.204
••••• Route 7 •				24.170			12-2/2	FV	
JG	5.3480	500.00	7.14	150		0.011917	14'-8	Df	1.081
44	2'-6	500.00	7.14	35.245		Hydrant,			3.035
41	-4'-6	500.00		39.360		E(14'-0), CV(32'-0), T(30'-0)	90'-8		5.055
JG	6.9630	500.00	4.21	150		0.003296			0.301
41	-4'-6	500.00	4.21	39.360		0.003230	18'-0		0.301
52	-4'-6			39.662		2EE(9'-0)	91'-5		
••••• Route 8 •	-			00.002		222(0 0)			
DY	2.0670	39.23	3.75	100		0.023315	0'-0	Df	0.449
212	12'-1	39.23	5.75	13.791		fE(2'-6), T(7'-1½)			-0.186
198	12'-6½			14.053		fE(2'-6), T(7'-1½)	19'-3		-0.100
••••• Route 9 •				14.000			19-5	FV	
DY	2.0670	39.23	3.75	100		0.023315	0'0	Df	0.449
199	12'-6	39.23	3.75	15.376		fE(2'-6), T(7'-1½)			0.449
213	12'-1			16.011		$fE(2'-6), T(7'-1\frac{1}{2})$	19'-3		0.100
••••• Route 10				10.011			10 0		
JG	6.9630	479.21	4.04	150		0.003047	62'0	Df	0.204
24	-4'-6	475.21	4.04	40.030		0.000047	4'-0		0.204
25	-4'-6			40.234		PIV(4'-0)	67'-0	-	
JG	6.4700	479.21	4.68	120		0.006585			0.007
25	-4'-6	713.21	. .00	40.234		5.00000		PT	0.007
26	-4'-6			40.234			1'-0		
JG	6.9630	479.21	4.04	150		0.003047			0.483
26	-4'-6	710.41	7. 07	40.241			39'-0		0.703
61	-4'-6			40.724		T(35'-0), PIV(4'-0)	158'-6		
JG	6.4700	479.21	4.68	120		0.006585			0.007
61	-4'-6	710.41	+.00	40.724		2.00000		Pr	0.007
63	-4'-6			40.730			1'-0		
JG	6.9630	479.21	4.04	150		0.003047			0.172
63	-4'-6	110.21	1.0 f	40.730			35'-0		0.172
71	-4'-6			40.902		T(35'-0)	56'-6		
••••• Route 11						× /			
JG	6.9630	479.21	4.04	150		0.003047	46'-8½	Pf	0 182
36	-4'-6			39.649			13'-0		0.102
18	-4'-6			39.831		EE(9'-0), PIV(4'-0)	59'-8½		
JG	6.4700	479.21	4.68	120		0.006585		_	0.007
18	-4'-6			39.831				Pe	0.007
19	-4'-6			39.837			1'-0		
JG	6.9630	479.21	4.04	150		0.003047			0.186
19	-4'-6	710.21		39.837			4'-0		0.100
22	-4'-6			40.023		PIV(4'-0)	61'-0		
	6.4700	479.21	4.68	120		0.006585			0.007
IG	0.+/00	713.41	uu			3.00000			0.007
JG 22	-4'-6			40.023				Pe	

pe Type Downstream Jpstream	Diameter Elevation	Flow Discharge	Velocity K-Factor	HWC Pt	Pn	Friction Loss Fittings			Length Eq. Length Total Length	Pressure Summary
uivalent Pipe Ler	igths of Valves an	nd Fittings (C=120 o	nly)		C Value	Multiplier				
1	Actual Inside	e Diameter	^{4.87}		Value 0	Df C	100	130	140	150
C Sch	edule 40 Steel Pi	ipe Inside Diameter) =⊦	actor	Multiply	ing Factor	0.713	1.16	1.33	1.51
Pipe Type Le	gend		U	nits Legend					Fittings Leger	ıd
AO Arm-Over BL Branch Lind CM Cross Main DR Drop DY Dynamic Feed Main FF Feed Riser MS Miscellaned DR Outrigger RN Riser Nippl SP Sprig ST Stand Pipe JG Undergroun	e E Fi D Vi P L C Fi D Fi P P P P P	IWC Haz It Tota In Nor If Pre Pre Pre	n n	point in a pipe a point in a p o friction betw vation differe	ipe veen points nce betwee	n indicated point	S	AngV A b BaIV B BFP B C cplg C C CV D E E E E f d F F C CV D E E E E f d F F C CV D E E E f d F F C CV D E F F C CV D E F F C CV D E F F C CV D E F F C CV D E F F C CV D F F F F F C CV D F F F F F F F F F F F F F F F F F F F	Alarm Valve Angle Valve Bushing Ball Valve Backflow Prevents Backflow Prevents Backflow Prevents Backflow Prevents Backflow Prevents Coupling Cross Run Check Valve Deluge Valve Dry Pipe Valve Fice Department C Dry FireLock(TM) FireLock(TM) Tee Gauge Globe Valve Hose Hose Hose Hose Hose Hose Valve Hose Hose Valve Hose Hose Hose Hose Hose Hose Hose Hos	0° Connection Elbow Elbow g Valve alve e

Document:TA-63 TWF Construction ReportDate:January 2017

TA 63 TWF Retention Basin Sealant Information

Document:TA-63 TWF Construction ReportDate:January 2017

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Attachment A

abcont 39671	ract Number:		STR Name: Roy Maestas
-	Company Name: J.B. Henderson Constr	ruction	Date Submitted: 9/10/2014
R	Street Address: 1285 Trinity Drive, Suit	tes A&B	x Initial Submittal of a New Document
CTO	City, State, Zip code: Los Alamos, NM 8754		Re- Submittal of Previous Document
SUBCONTRACTOR	Subcontractor's Poin Taylor Cardon		
Z	Submittal Number:	5.1115 (09 920	1)
0	Submittal Title:	Retention Basin	Sealant
ă	Revision Number:	0	
			DN: cn-Grea Masterman o- IP Henderson ou
		Greg Ma	Sterman DN: cn=Greg Masterman, o=JB Henderson, ou, email=gmasterman@jbhenderson.com, c=US Date: 2014.09.10 08:06:42 -06'00'
i f	Date Received:	Greg Ma	Sterman DN: cn=Greg Masterman, o=JB Henderson, ou, email=gmasterman@jbhenderson.com, c=US Date: 2014.09.10 08:06:42 -06'00'
The second		Greg Mas	Sterman DN: cn=Greg Masterman, o=JB Henderson, ou, email=gmasterman@jbhenderson.com, c=US Date: 2014.09.10 08:06:42 -06'00'
12	Date Received:	Greg Mas Micha (*) 9/23/14	DN: cn=Greg Masterman, o=JB Henderson, ou, email=gmasterman@jbhenderson.com, c=US Date: 2014.09.10 08:06:42 -06'00'
RACTOR	Date Received: Statused By:	Greg Mas Micha (*) 9/23/14	DN: cn=Greg Masterman, o=JB Henderson, ou, email=gmasterman@jbhenderson.com, c=US Date: 2014.09.10 08:06:42 -06'00'

Subcontract No. 289671 Rev. 0, Dated 01/22/2010

Attachment A

NATIO	Alamos NAL LABORATORY EST. 1943 —		BCONTRACTOR ITAL / STATUS SHEET
u bcont 39671	ract Number:		STR Name: Roy Maestas
SUBCONTRACTOR		of Contact: 5.1134-0001 Manufacturer's Fie Xypec Retention Basin C 0 essentative's signatu and meets the requ	oncrete Sealant (09 9201/1.05.E) re below indicates that submittal has been irements of the subcontract.
CONTRACTOR		Jun 09, 2016	/Signature on File

Attachment A

• LOS	Alamos NAL LABORATORY EST. 1943		BCONTRACTOR TTAL / STATUS SHEET
Subcont 289671	ract Number:		STR Name: Roy Maestas
209071			Ruy maesias
~	Company Name: J.B. Henderson Construct Street Address:	ction	Date Submitted: 09/09/15
Ъ.	1285 Trinity Drive, Suites	s A&B	X Initial Submittal of a New Document
CT	City, State, Zip code: Los Alamos, NM 87544		Re- Submittal of Previous Document
RA.	Subcontractor's Point Taylor Cardon	of Contact:	URGENT
Ī	Submittal Number:	5.1131-0001	UNGENT
SUBCONTRACTOR	Submittal Title:	Product Data Xypex Retention Basin C	oncrete Sealant (09 9201/1.05.B)
S	Revision Number:	0	
	Subcontractor's Repre		irements of the subcontract. re:
	Date Received:		
	Statused By:		
£	Date:		
LOR	Comments:		
- U			
RA			
L N			
CONTRA	indicated comm 3 Reviewed. Rev 4 Reject. Subm 5 Permission to	se and resubmit. V nents. vise and resubmit.	Vork may proceed subject to incorporation of Work may not proceed. t requirements. Resubmit. ed.
	Submit comments to:		



Concrete Waterproofing

Description

Xypex is a unique chemical treatment for the waterproofing, protection and repair of concrete. XYPEX CONCEN-TRATE is the most chemically active product within the Xypex Crystalline Waterproofing System. When mixed with water, this light grey powder is applied as a cementitious slurry coat to above-grade or below-grade concrete, either as a single coat or as the first of a two-coat application. It is also mixed in Dry-Pac form for sealing strips at construction joints, or for the repairing of cracks, faulty construction joints and honeycombs. Xypex prevents the penetration of water and other liquids from any direction by causing a catalytic reaction that produces a non-soluble crystalline formation within the pores and capillary tracts of concrete and cement-based materials.

Recommended for:

- Reservoirs
- · Sewage and Water Treatment Plants
- Underground Vaults
- Secondary Containment Structures
- Foundations
- · Tunnels and Subway Systems
- Swimming Pools
- Parking Structures

Advantages

- · Resists extreme hydrostatic pressure
- · Becomes an integral part of the substrate
- Can seal hairline cracks up to 0.4 mm
- · Allows concrete to breathe
- Highly resistant to aggressive chemicals
- Non-toxic
- Does not require a dry surface
- · Cannot puncture, tear or come apart at the seams
- No costly surface priming or leveling prior to application
- Does not require sealing, lapping and finishing of seams at corners, edges or between membranes
- · Can be applied to the positive or the negative side of the concrete surface
- Does not require protection during backfilling or during placement of steel, wire mesh or other materials
- Less costly to apply than most other methods
- · Not subject to deterioration
- Permanent

Packaging

Xypex Concentrate is available in 20 lb. (9.1 kg) pails, 60 lb. (27.2 kg) pails and 50 lb. (22.7 kg) bags.

Storage

Xypex products must be stored dry at a minimum temperature of 45°F (7°C). Shelf life is one year when stored under proper conditions.

Coverage

For normal surface conditions, the coverage rate for each Xypex coat is 6 to 7.2 sq. ft./lb. (1.25 - 1.5 lb./sq. yd. or 0.65 - 0.8 kg/m²).

Test Data

PERMEABILITY

U.S. Army Corps of Engineers (USACE) CRD C48-73, "Permeability of Concrete", Pacific Testing Labs, Seattle, USA

Two in. (51 mm) thick, 2000 psi (13.8 MPa) Xypex-treated concrete samples were pressure tested up to a 405 ft. (124 m) water head (175 psi/1.2 MPa), the limit of the testing apparatus. While untreated samples showed marked leakage, the Xypex-treated samples (as a result of the crystallization process) became totally sealed and exhibited no measurable leakage.

DIN 1048, "Water Impermeability of Concrete", Bautest – Corporation for Research & Testing of Building Materials, Augsburg, Germany

Twenty cm thick Xypex-treated concrete samples were pressure tested up to 7 bars (230 ft./70 m water head) for 24 hours to determine water impermeability. While the reference specimens measured water penetration up to a depth of 92 mm, Xypex-treated samples measured water penetration of zero to an average of 4 mm.

ÖNORM B 3303, "Water Impermeability of Concrete", Technologisches Gerwerbemuseum, Federal Higher Technical Education & Research Institute, Vienna, Austria

Xypex-treated concrete samples were pressure tested to a maximum 7 bars (230 ft./70 m water head) for 10 days. Test revealed that while 25 ml of water had penetrated the untreated concrete samples, zero ml had penetrated the Xypex-treated samples. Test specimens were then broken and showed water penetration to a depth of 15 mm on untreated samples but no measurable water penetration on the Xypex-treated samples.

CSN 1209/1321, "Impermeability and Resistance to Pressurized Water", Institute of Civil Engineering, Technology and Testing, Bratislava, Slovak Republic

Xypex-treated and untreated concrete samples were exposed to 1.2 MPa of pressure to determine water permeability. Results showed the Xypex-treated samples provided effective protection against hydrostatic water pressure. Treated and untreated samples were also subjected to contact with silage juices and various petroleum products (e.g. diesel oil, transformer oil, gasoline) at 14 kPa for 28 days. The Xypex-treated samples significantly reduced the penetration of these solutions.

CHEMICAL RESISTANCE

ASTM C 267-77, "Chemical Resistance to Mortars", Pacific Testing Labs, Seattle, USA

Xypex-treated cylinders and untreated cylinders were exposed to hydrochloric acid, caustic soda, toluene, mineral oil, ethelyne glycol, pool chlorine and brake fluid and other chemicals. Results indicated that chemical exposure did not have any detrimental effects on the Xypex coating. Tests following chemical exposure measured an average 17% higher compressive strength in the Xypextreated specimens over the untreated control samples.

IWATE University Technical Report, "Resistance to Acid Attack", Tokyo, Japan

Xypex-treated mortar and untreated mortar were measured for acid resistance after exposure to a 5% H_2SO_4 solution for 100 days. Xypex suppressed concrete erosion to 1/8 of the reference samples.

FREEZE/THAW DURABILITY

ASTM C 672, "Standard Test Method for Scaling Resistance of Concrete Surfaces Exposed to De-Icing Chemicals", Twin City Testing Lab, St. Paul, USA

Xypex-treated samples restricted chloride ion concentration to below the level necessary to promote electrolytic corrosion of reinforcing steel. Visual examination of untreated panels after 50 freeze/thaw cycles showed a marked increase in surface deterioration compared to Xypex-treated samples.

JIS A 6204, "Concrete Freeze/Thaw", Japan Testing Center for Construction Materials, Tokyo, Japan

The resonating frequency of both untreated and Xypextreated concrete samples were measured throughout 435 freeze/thaw cycles. At 204 cycles, the Xypex-treated samples showed 96% relative durability compared to 90% in the untreated samples. At 435 cycles, the Xypextreated samples measured 91% relative durability compared to 78% in the untreated reference samples.

POTABLE WATER EXPOSURE

NSF 61, "Drinking Water System Component-Health Effects", NSF International, Ann Arbor, USA

Exposure testing of potable water in contact with Xypextreated samples indicated no harmful effects.

RADIATION RESISTANCE

U.S.A. Standard No. N69, "Protective Coatings for the Nuclear Industry", Pacific Testing Labs, Seattle, USA

After exposure to 5.76 x 10⁴ rads of gamma radiation, the Xypex treatment revealed no ill effects or damages.

Application Procedures

1. **SURFACE PREPARATION** Concrete surfaces to be treated must be clean and free of laitance, dirt, film, paint, coating or other foreign matter. Surfaces must also have an open capillary system to provide "tooth and suction" for the Xypex treatment. If surface is too smooth (e.g. where steel forms are used) or covered with excess form oil or other foreign matter, the concrete should be lightly sandblasted, waterblasted, or etched with muriatic (HCL) acid.

2. **STRUCTURAL REPAIR** Rout out cracks, faulty construction joints and other structural defects to a depth of 1.5 in. (37 mm) and a width of 1 in. (25 mm). Apply a brush coat of Xypex Concentrate as described in steps 5 & 6 and allow to dry for 10 minutes. Fill cavity by tightly compressing Dry-Pac into the groove with pneumatic packing tool or with hammer and wood block. Dry-Pac is prepared by mixing six parts Xypex Concentrate powder with one part water to a dry, lumpy consistency.

NOTE:

i. Against a direct flow of water (leakage) or where there is excess moisture due to seepage, use Xypex Patch'n Plug then Xypex Dry-Pac followed by a brush coat of Xypex Concentrate. (Refer to Xypex Specifications and Applications Manual for full details.)

ii. For expansion joints or chronic moving cracks, flexible materials such as expansion joint sealants should be used.

3. WETTING CONCRETE Xypex requires a saturated substrate and a damp surface. Concrete surfaces must be thoroughly saturated with clean water prior to the application so as to aid the proper curing of the treatment and to ensure the growth of the crystalline formation

deep within the pores of the concrete. Remove excess surface water before the application. If concrete surface dries out before application, it must be re-wetted.

4. **MIXING FOR SLURRY COAT** Mix Xypex powder with clean water to a creamy consistency in the following proportions:

For Brush Application

1.25 - 1.5 lb./sq. yd. (0.65 - 0.8 kg/m²) 5 parts powder to 2 parts water

2.0 lb./sq. yd. (1.0 kg/m²)3 parts powder to 1 part water

For Spray Application

1.25 - 1.5 lb./sq. yd. (0.65 - 0.8 kg/m²)5 parts powder to 3 parts water (ratio may vary with equipment type)

Do not mix more Xypex material than can be applied in 20 minutes. Do not add water once mix starts to harden. Protect hands with rubber gloves.

5. **APPLYING XYPEX** Apply Xypex with a semi-stiff nylon bristle brush, push broom (for large horizontal surfaces) or specialized spray equipment. The coating must be uniformly applied and should be just under 1/16 in. (1.25 mm). When a second coat (Xypex Concentrate or Xypex Modified) is required, it should be applied after the first coat has reached an initial set but while it is still "green" (less than 48 hours). Light pre-watering between coats may be required due to drying. The Xypex treatment must not be applied under rainy conditions or when ambient temperature is below 40°F (4°C). For recommended equipment, contact Xypex Chemical Corporation or your nearest Xypex distributor.

6. **CURING** A misty fog spray of clean water must be used for curing the Xypex treatment. Curing should begin as soon as the Xypex has set to the point where it will not be damaged by a fine spray of water. Under normal conditions, it is sufficient to spray Xypex-treated surfaces three times per day for two to three days. In hot or arid climates, spraying may be required more frequently. During the curing period, the coating must be protected from rainfall, frost, wind, the puddling of water and temperatures below 36°F (2°C) for a period of not less than 48 hours after application. If plastic sheeting is used as protection, it must be raised off the Xypex to allow the coating to breathe. Xypex Gamma Cure may be used in lieu of water curing for certain applications (consult with Xypex Chemical Corporation or your nearest Xypex distributor).

NOTE: For concrete structures that hold liquids (e.g. reservoirs, swimming pools, tanks, etc.), Xypex should be cured for three days and allowed to set for 12 days before filling the structure with liquid.

Technical Services

For more instructions, alternative application methods, or information concerning the compatibility of the Xypex treatment with other products or technologies, contact the Technical Services Department of Xypex Chemical Corporation or your local Xypex representative.

Safe Handling Information

Xypex is alkaline. As a cementitious powder or mixture, Xypex may cause significant skin and eye irritation. Directions for treating these problems are clearly detailed on all Xypex pails and packaging. The Manufacturer also maintains comprehensive and up-to-date Material Safety Data Sheets on all its products. Each sheet contains health and safety information for the protection of workers and customers. The Manufacturer recommends you contact Xypex Chemical Corporation or your local Xypex representative to obtain copies of Material Safety Data Sheets prior to product storage or use.

Warranty

The Manufacturer warrants that the products manufactured by it shall be free from material defects and will be consistent with its normal high quality. Should any of the products be proven defective, the liability to the Manufacturer shall be limited to replacement of the product ex factory. The Manufacturer makes no warranty as to merchantability or fitness for a particular purpose and this warranty is in lieu of all other warranties expressed or implied. The user shall determine the suitability of the product for his intended use and assume all risks and liability in connection therewith.



* 13731 Mayfield Place, Richmond, BC, Canada V6V 2G9 Toll-free: 1.800.961.4477 Tel: 604.273.5265 Fax: 604.270.0451 E-mail: info@xypex.com Web: www.xypex.com XYPEX is a registered trademark of Xypex Chemical Corporation. Copyright © 1975-2009 Xypex Chemical Corporation.





07160 CEMENTITIOUS CRYSTALLINE - CURING Concrete Waterproofing

Description

XYPEX GAMMA CURE is a curing agent designed specifically for Xypex crystalline waterproofing products. Gamma Cure may be used as an alternative to water curing for certain Xypex applications. It is also used to accelerate the Xypex crystallization process. Xypex Gamma Cure acts as an evaporation retardant by retaining the maximum amount of moisture in the Xypex coating. It also provides a catalyst for the reaction with the Xypex crystalline waterproofing treatment. It is a selfdissipating (2 - 3 days) non-film forming product.

Recommended for:

- · Applications where water-curing is not possible
- · Hot, dry, windy conditions
- Vertical surfaces

Packaging

Xypex Gamma Cure is available in 1 U.S. gallon (3.79 litre) bottles and 5 U.S. gallon (18.95 litre) pails.

Storage

Xypex products must be stored dry at a minimum temperature of 45°F (7°C). Shelf life is one year when stored under proper conditions.

Coverage

One U.S. gallon (3.79 litres) of Gamma Cure when diluted with water will cover approximately 800 sq. ft. (75 m²).

Application Procedures

1. CURING OF XYPEX COATING Dilute one part Gamma Cure with 3 parts clean water. Apply by spraying onto the crystalline waterproofing coating after the coating has reached an initial set, but before it dries (approx. 1 - 2 hours).

2. PREPARATION OF CONCRETE SUBSTRATE IN HOT, DRY OR WINDY CONDITIONS Dilute one part Gamma Cure with 3 parts clean water and apply to concrete surface before application of the Xypex crystalline coating. Gamma Cure should be applied while the concrete is still damp from pre-watering.

Technical Services

For more instructions, alternative application methods, or information concerning the compatibility of the Xypex treatment with other products or technologies, contact the Technical Services Department of Xypex Chemical Corporation or your local Xypex representative.

Safe Handling Information

Gamma Cure is an acidic solution. This product may be a mild to moderate skin and eye irritant. In addition, many of the components of the cementitious products that are used in conjunction with the Gamma Cure may also possess significant skin and eye irritation potential. Directions for treating these problems are clearly detailed on all Xypex pails and packaging. The Manufacturer also maintains comprehensive and up-to-date Material Safety Data Sheets on all its products. Each sheet contains health and safety information for the protection of workers and customers. The Manufacturer recommends you contact Xypex Chemical Corporation or your local Xypex representative to obtain copies of Material Safety Data Sheets prior to product storage or use.

Warrantv

The Manufacturer warrants that the products manufactured by it shall be free from material defects and will be consistent with its normal high quality. Should any of the products be proven defective, the liability to the Manufacturer shall be limited to replacement of the product ex factory. The Manufacturer makes no warranty as to merchantability or fitness for a particular purpose and this warranty is in lieu of all other warranties expressed or implied. The user shall determine the suitability of the product for his intended use and assume all risks and liability in connection therewith.



* 13731 Mayfield Place, Richmond, BC, Canada V6V 2G9 Toll-free: 1.800.961.4477 Tel: 604.273.5265 Fax: 604.270.0451 E-mail: info@xypex.com Web: www.xypex.com XYPEX is a registered trademark of Xypex Chemical Corporation. Copyright © 1978-2009 Xypex Chemical Corporation.





07160 CEMENTITIOUS CRYSTALLINE

Concrete Waterproofing

Description

Xypex is a unique chemical treatment for the waterproofing, protection and repair of concrete. XYPEX MODIFIED can be applied as a second coat to reinforce Xypex Concentrate, or applied by itself to damp-proof the exterior of foundation walls. Applied as a second coat, Xypex Modified chemically reinforces Xypex Concentrate where two coats are required and produces a harder finish. Where damp-proofing is required, a single coat of Modified may be used as an alternative to a spray/tar emulsion. Xypex prevents the penetration of water and other liquids from any direction by causing a catalytic reaction that produces a non-soluble crystalline formation within the pores and capillary tracts of concrete and cement-based materials.

Recommended for:

Xypex Modified is recommended as a single coat for the damp-proofing of foundations or as a second coat with Xypex Concentrate for the following applications:

- Reservoirs
- · Sewage and Water Treatment Plants
- Secondary Containment Structures
- · Tunnels and Subway Systems
- Underground Vaults
- Foundations
- · Parking Structures
- Swimming Pools

Advantages

- · Resists extreme hydrostatic pressure
- · Becomes an integral part of the substrate
- · Allows concrete to breathe
- · Resistant to aggressive chemicals
- Non-toxic
- · Does not require dry weather or a dry surface
- · Cannot puncture, tear or come apart at the seams
- No costly surface priming or leveling prior to application
- · Does not require sealing, lapping and finishing of seams at corners, edges or between membranes
- Can be applied to the positive or the negative side of the concrete surface

- · Does not require protection during backfilling or during placement of steel, wire mesh or other materials
- · Less costly to apply than most other methods
 - · Not subject to deterioration
 - Permanent

Packaging

Xypex Modified is available in 60 lb. (27.2 kg) pails and 50 lb. (22.7 kg) bags.

Storage

Xypex products must be stored dry at a minimum temperature of 45°F (7°C). Shelf life is one year when stored under proper conditions.

Coverage

For normal surface conditions, the coverage rate for each coat is 6 - 7.2 sq. ft. per lb. (1.25 - 1.5 lb. per sq. yd. or 0.65 - 0.8 kg/m²).

Test Data

When used in conjunction with Xypex Concentrate:

PERMEABILITY

U.S. Army Corps of Engineers (USACE) CRD C48-73, "Permeability of Concrete", Pacific Testing Labs, Seattle, USA

Two in. (51 mm) thick, 2000 psi (13.8 MPa) Xypex-treated concrete samples were pressure tested up to a 405 ft. (124 m) water head (175 psi/1.2 MPa), the limit of the testing apparatus. While untreated samples showed marked leakage, the Xypex-treated samples (as a result of the crystallization process) became totally sealed and exhibited no measurable leakage.

DIN 1048, "Water Impermeability of Concrete", Bautest – Corporation for Research & Testing of Building Materials, Augsburg, Germany

Twenty cm thick Xypex-treated concrete samples were pressure tested up to 7 bars (230 ft./70 m water head) for 24 hours to determine water impermeability. While the reference specimens measured water penetration up to a depth of 92 mm, Xypex-treated samples measured water penetration of zero to an average of 4 mm.

ÖNORM B 3303, "Water Permeability of Concrete", Technologisches Gerwerbemuseum, Federal Higher Technical Education & Research Institute, Vienna, Austria

Xypex-treated concrete samples were pressure tested to a maximum 7 bars (230 ft./70 m water head) for 10 days. Test revealed that while 25 ml of water had penetrated the untreated concrete samples, zero ml had penetrated the Xypex-treated samples. Test specimens were then broken and showed water penetration to a depth of 15 mm on untreated samples but no measurable water penetration on the Xypex-treated samples.

CSN 1209/1321, "Impermeability and Resistance to Pressurized Water", Institute of Civil Engineering, Technology and Testing, Bratislava, Slovak Republic

Xypex-treated and untreated concrete samples were exposed to 1.2 MPa of pressure to determine water permeability. Results showed the Xypex-treated samples provided effective protection against hydrostatic water pressure. Treated and untreated samples were also subjected to contact with silage juices and various petroleum products (e.g. diesel oil, transformer oil, gasoline) at 14 kPa for 28 days. The Xypex-treated samples significantly reduced the penetration of these solutions.

CHEMICAL RESISTANCE

ASTM C 267-77, "Chemical Resistance to Mortars", Pacific Testing Labs, Seattle, USA

Xypex-treated cylinders and untreated cylinders were exposed to hydrochloric acid, caustic soda, toluene, mineral oil, ethelyne glycol, pool chlorine and brake fluid and other chemicals. Results indicated that chemical exposure did not have any detrimental effects on the Xypex coating. Tests following chemical exposure measured an average 17% higher compressive strength in the Xypextreated specimens over the untreated control samples.

IWATE University Technical Report, "Resistance to Acid Attack", Tokyo, Japan

Xypex-treated mortar and untreated mortar were measured for acid resistance after exposure to a 5% H_2SO_4 solution for 100 days. Xypex suppressed concrete erosion to 1/8 of the reference samples.

FREEZE/THAW DURABILITY

ASTM C 672, "Standard Test Method for Scaling Resistance of Concrete Surfaces Exposed to De-Icing Chemicals", Twin City Testing Lab, St. Paul, USA

Xypex-treated samples restricted chloride ion concentration to below the level necessary to promote electrolytic corrosion of reinforcing steel. Visual examination of untreated panels after 50 freeze/thaw cycles showed a marked increase in surface deterioration compared to Xypex-treated samples.

POTABLE WATER EXPOSURE

NSF 61, "Drinking Water System Component-Health Effects", NSF International, Ann Arbor, USA

Exposure testing of potable water in contact with Xypextreated samples indicated no harmful effects.

RADIATION RESISTANCE

U.S.A. Standard No. N69 , "Protective Coatings for the Nuclear Industry", Pacific Testing Labs, Seattle, USA After exposure to 5.76×10^4 rads of gamma radiation, the Xypex treatment revealed no ill effects or damages.

Application Procedures

1. **SURFACE PREPARATION** Concrete surfaces to be treated must be clean and free of laitance, dirt, film, paint, coating or other foreign matter. Surfaces must also have an open capillary system to provide "tooth and suction" for the Xypex treatment. If surface is too smooth (e.g. where steel forms are used) or covered with excess form oil or other foreign matter, the concrete should be lightly sand-blasted, waterblasted, or etched with muriatic (HCL) acid.

2. **STRUCTURAL REPAIR** Rout out cracks, faulty construction joints and other structural defects to a depth of 1.5 in. (37 mm) and a width of 1 in. (25 mm). Apply a brush coat of Xypex Concentrate as described in steps 5 & 6 and allow to dry for 10 minutes. Fill cavity by tightly compressing Dry-Pac into the groove with pneumatic packing tool or with hammer and wood block. Dry-Pac is prepared by mixing six parts Xypex Concentrate powder with one part water to a dry, lumpy consistency.

NOTE:

i. Against a direct flow of water (leakage) or where there is excess moisture due to seepage, use Xypex Patch'n Plug then Xypex Dry-Pac followed by a brush coat of Xypex Concentrate. (Refer to Xypex Specifications and Applications Manual for full details.)

ii. For expansion joints or chronic moving cracks, flexible materials such as expansion joint sealants should be used.

3. WETTING CONCRETE Xypex requires a saturated substrate and a damp surface. Concrete surfaces must be thoroughly saturated with clean water prior to the application so as to aid the proper curing of the treatment and to ensure the growth of the crystalline formation deep within the pores of the concrete. Remove excess surface water before the application. If concrete surface dries out before application, it must be re-wetted.

4. **MIXING FOR SLURRY COAT** Mix Xypex powder with clean water to a creamy consistency in the following proportions:

For Brush Application

1.25 - 1.5 lb./sq. yd. (0.65 - 0.8 kg/m²) 5 parts powder to 2 parts water

2.0 lb./sq. yd. (1.0 kg/m²)3 parts powder to 1 part water

For Spray Application

1.25 - 1.5 lb./sq. yd. (0.65 - 0.8 kg/m²)5 parts powder to 3 parts water (ratio may vary with equipment type)

Do not mix more Xypex material than can be applied in 20 minutes. Do not add water once mix starts to harden. Protect hands with rubber gloves.

5. **APPLYING XYPEX** Apply Xypex with a semi-stiff nylon bristle brush, push broom (for large horizontal surfaces) or specialized spray equipment. The coating must be uniformly applied and should be just under 1/16 in. (1.25 mm). When a second coat (Xypex Concentrate or Xypex Modified) is required, it should be applied after the first coat has reached an initial set but while it is still "green" (less than 48 hours). Light pre-watering between coats may be required due to drying. The Xypex treatment must not be applied under rainy conditions or when ambient temperature is below 40°F (4°C). For recommended equipment, contact Xypex Chemical Corporation or your nearest Xypex distributor.

6. **CURING** A misty fog spray of clean water must be used for curing the Xypex treatment. Curing should begin as soon as the Xypex has set to the point where it will not be damaged by a fine spray of water. Under normal conditions, it is sufficient to spray Xypex-treated surfaces three times per day for two to three days. In hot or arid climates, spraying may be required more frequently. During the curing period, the coating must be protected from rainfall, frost, wind, the puddling of water and temperatures below 36°F (2°C) for a period of not less than 48 hours after application. If plastic sheeting is used as protection, it must be raised off the Xypex to allow the coating to breathe. Xypex Gamma Cure may be used in lieu of water curing for certain applications (consult with Xypex Chemical Corporation or your nearest Xypex distributor).

NOTE: For concrete structures that hold liquids (e.g. reservoirs, swimming pools, tanks, etc.), Xypex should be cured for three days and allowed to set for 12 days before filling the structure with liquid.

Technical Services

For more instructions, alternative application methods, or information concerning the compatibility of the Xypex treatment with other products or technologies, contact the Technical Services Department of Xypex Chemical Corporation or your local Xypex representative.

Safe Handling Information

Xypex is alkaline. As a cementitious powder or mixture, Xypex may cause significant skin and eye irritation. Directions for treating these problems are clearly detailed on all Xypex pails and packaging. The Manufacturer also maintains comprehensive and up-to-date Material Safety Data Sheets on all its products. Each sheet contains health and safety information for the protection of workers and customers. The Manufacturer recommends you contact Xypex Chemical Corporation or your local Xypex representative to obtain copies of Material Safety Data Sheets prior to product storage or use.

Warranty

The Manufacturer warrants that the products manufactured by it shall be free from material defects and will be consistent with its normal high quality. Should any of the products be proven defective, the liability to the Manufacturer shall be limited to replacement of the product ex factory. The Manufacturer makes no warranty as to merchantability or fitness for a particular purpose and this warranty is in lieu of all other warranties expressed or implied. The user shall determine the suitability of the product for his intended use and assume all risks and liability in connection therewith.



* 13731 Mayfield Place, Richmond, BC, Canada V6V 2G9 Toll-free: 1.800.961.4477 Tel: 604.273.5265 Fax: 604.270.0451 E-mail: info@xypex.com Web: www.xypex.com XYPEX is a registered trademark of Xypex Chemical Corporation. Copyright © 1975-2009 Xypex Chemical Corporation.



Review Cycle	End Date	Status Entered By	Status Entered	Status
SBT-289671-51134-0001 - Mfr Field Report Xype	ec Jun 8, 2016	Michael Pope	Jun 9, 2016	1 Reviewed - Work may proceed.

Reviewer	Title	Page Comment Type	Error Type	Comment Date	Final Disposition	Final Disposition Person	Final Disposition Date
Lopez, James	SBT-289671-51134-0001 - Mfr Field Report Xypec Retention Basin Concrete Sealant.pdf	3 Preference	Status Code: 1 Reviewed - Work may proceed	6/8/2016 13:3	2 Implement	Pope, Michael	6/9/2016 6:13

AE FIRM ONLY

SUBM	ISSION #	206#
1	Reviewed- Work may proceed	3 Reviewed- Revise & Resubmit.Work may NOT proceed.
12	Reviewed- Revise & Resubmit. Work may proceed subject to	4 Reject- Submittal does not meet requirements. Resubmit
<u> </u>	incorporation of indicated comments	5 Permission to proceed not required
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AE FIRM ONLY



September 2015

Dear All,

I have reviewed the application of Xypex coatings by Certified Applicators 'GWC' at the LANL TRU Waste Project and have approved its proper placement. Please don't hesitate to contact me if you have any questions, now or in the future.

Stephen Boyd Xypex Area Representative 970-946-6016 swconsult@durango.net

> Great West Xypex Region Reps. Colorado * New Mexico * Idaho * Wyoming * Montana South West Concrete Consulting, LLC – 19 Road 2720, Aztec, NM 87410 Tel: 970-946-6016 Office-505-334-7597 Web: www.xypex-it.com

Reviewer	Title	Page Comment Type Error Type Formatted Comment	Error Type	Formatted Comment	Comment Date
Sapp, Lindsay	SBT-289671-51115-0001_Retention Basin Sealantpdf	1 Preference	Scriveners Error	Lindsay Sapp commenting for Conrad Scriveners Error Ley, Lead Civil WNNNM JV. 1. Reviewed -Work may proceed	9/12/2014 9:21

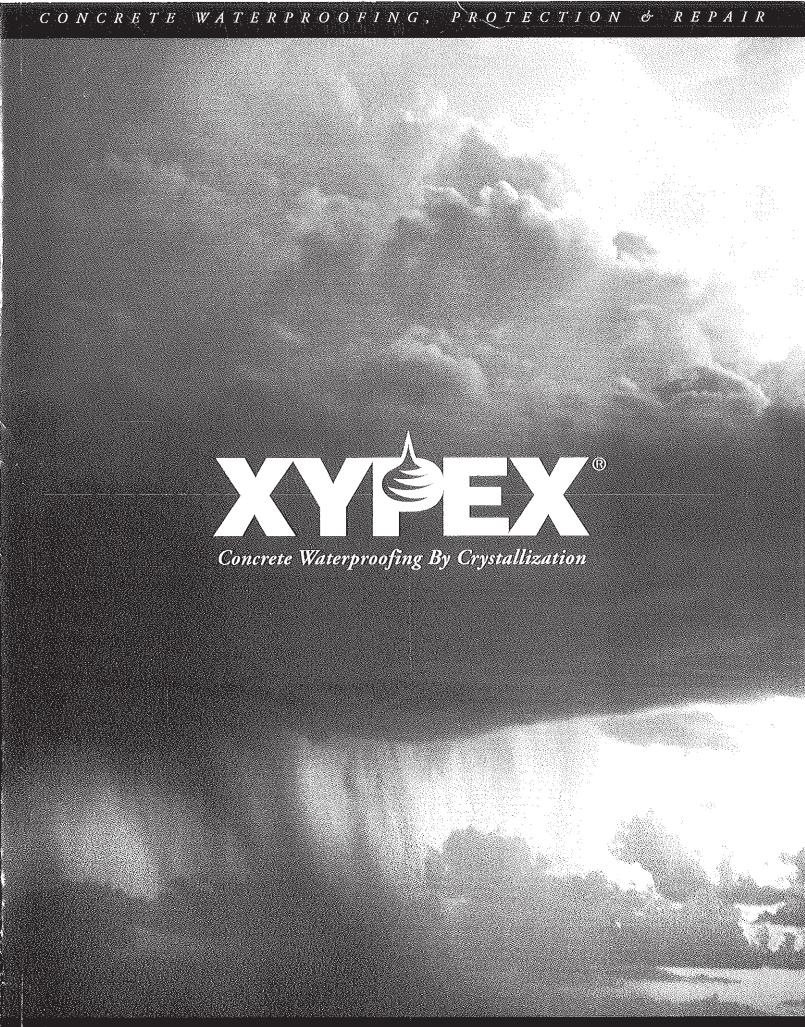
Attachment A

	Alamos NAL LABORATORY - EST. 1943		BCONTRACTOR ITAL / STATUS SHEET
Subcont 289671	ract Number:		STR Name: Roy Maestas
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AE FIRM ONLY

SUBM	ISSION #	206#
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12	Reviewed- Revise & Resubmit, Work may proceed subject to	4 Reject- Submittal does not meet requirements. Resubmit
	incorporation of indicated comments	5 Permission to proceed not required
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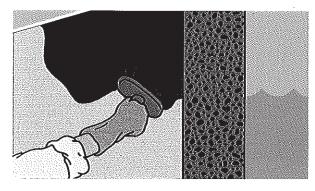
AE FIRM ONLY



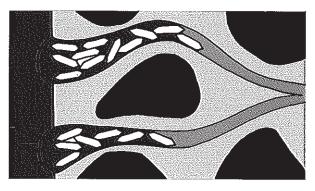
What is XYPEX Concrete Waterproofing by Crystallization[™]

XYPEX is a unique chemical treatment for the waterproofing and protection of concrete. Manufactured in the form of a dry powder compound, Xypex consists of Portland cement, very fine treated silica sand and various active proprietary chemicals.

How does **XYPEX** Waterproof Concrete?



When mixed with water and applied as a cementitious coating, the active chemicals in Xypex cause a catalytic reaction which generates a non-soluble crystalline formation of dendritic...



...fibres within the pores and capillary tracts of concrete. This process permanently seals the concrete against the penetration of water or liquids from any direction.

Electron microscope photos show the sheared face of a concrete control sample and illustrate its reaction to the Xypex crystallization process.



Concrete Before Xypex



Xypex Crystallization Begins



Xypex Crystallization Motures (26 days)

Advantages of XYPEX

Waterproofs underground structures from the inside against hydrostatic pressure.

By the process of osmosis and because the chemicals in Xypex have an affinity with water, the crystalline formation migrates throughout the pores and capillary tracts of concrete even against strong hydrostatic pressure.

Protects concrete and reinforcing steel

The Xypex treatment is highly resistant to most aggressive substances (pH 3.11 constant contact, pH 2-12 periodic contact). By preventing the intrusion of chemicals, salt water, sewage and other harmful materials, Xypex protects concrete and reinforcing steel from deterioration and oxidation. The concrete is also protected against spalling, efflorescence, popouts and other damages caused by weathering, bleeding of the salts and internal expansion and contraction during the freeze-thaw cycle.

Permits concrete to 'breathe'

The Xypex crystalline formation has 'fixed size' air spaces so small that water molecules cannot pass through. However, it does allow the passage of air, thus the concrete is able to 'breathe' and become thoroughly dry, preventing water vapour buildup.

Non-toxic

Xypex products have been approved by the U.S. Environmental Protection Agency, Agriculture Canada, Water Research Council, NSF International, Mairie de Paris and many other government health agencies throughout the world for use on concrete structures that hold potable water or foodstuffs.

Can be applied to moist or 'green' concrete

Xypex coatings require moisture to produce the crystalline formation. Therefore, concrete that is moist or 'green' is ideal for the Xypex treatment. If the concrete is dry, it must be pre-dampened prior to application.

Some other advantages

- Xypex is not just a coating. Because the crystalline formation becomes an integral part of the concrete, Xypex does not rely on its surface coating to waterproof concrete.
- Xypex will seal hairline cracks up to 0.4mm (1/41").
- Xypex does not require costly surface priming or levelling prior to application.
- Xypex cannot puncture, lear or come apart at the seams.
- Xypex does not require protection during backfilling or during placement of steel, wire mesh or other materials.
- Xypex is less costly to apply than most other methods.

Typical XYPEX Projects

- Reservoirs
- Sewage and Water Treatment Tanks
- Tunnels
- Manholes
- Underground Vaults and Cellars
- Foundations
- Parking Decks
- Bridges

Other XYPEX Products

Xypex Admix C-500, C-1000 and C-2000

With the Admix C-Series, Xypex's unique crystalline dry powder compound for the waterproofing, protection and improvement of concrete is added to the concrete mix at time of batching. Admix C-500, C-1000 and C-2000 have been specially formulated to meet varying project and temperature conditions. Xypex Admixes are available in a "no fines" grade.

Xypex DS-1 & DS-2

Xypex Concentrate DS-1 and DS-2 are special formulations which have been designed specifically for a dry-shake application on horizontal concrete prior to finishing.

Xypex Patch'n Plug

Fast setting, non-shrink, high bond strength hydraulic cement compound for concrete repairs. Stops flowing water in seconds. Patch'n Plug seals cracks, tie holes etc. and is also used for the general repair or patching of concrete. Patch'n Plug may be used in conjunction with Xycrylic Admix to increase the compressive strength and bond strength to existing concrete.

Xypex Megamix I and Megamix II

Megamix I is a thin parge coat for the waterproofing and resurfacing of vertical concrete and masonry surfaces. Megamix II is a thick repair mortar used for patching and resurfacing deteriorated concrete, whether vertical or overhead. Megamix II has been specifically formulated as a one-component mortar to produce superior bond, low shrinkage, high strength and durability. Both Megamix products contain Xypex's unique crystalline waterproofing and protection technology.

Xypex FCM 40 & FCM 60

FCM products have exceptional adhesive and elongation characteristics and are used for repairing cracks subject to movement, sealing construction joints, restoring deteriorated concrete, and waterproofing concrete structures. FCM is often used in conjunction with the Xypex Crystalline Concrete Waterproofing and Protection System.

Xypex Restora-Top

Restora-Top products have been specifically formulated for the repair and rehabilitation of horizontal concrete surfaces and provide excellent adhesive properties as well as superior durability and reduced shrinkage.

Xycrylic Admix

An acrylic polymer formulation specifically designed for use as an admix to fortily cement mixes. Xycrylic Admix increases hardness, durability, bonding capability and chemical resistance.

Xypex Gamma Cure

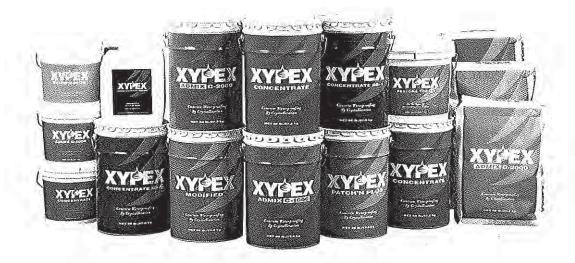
May be used as an alternative to water curing for certain Xypex applications. Consult manufacturer for further information.

Xypex Quickset

Xypex Quickset is a water-soluble liquid compound designed to harden, dustproof and seal the surfaces of fresh or newly cured concrete floors.

Technical Services

For more complete information, assistance in developing specifications, or arranging for application supervision, please contact Xypex Chemical Corporation or the nearest Xypex distributor.



Warranty The Manufacturer warrants that the products manufactured by it shall be free from material defects and will be consistent with its normal high quality. Should any of the products be proven defective, the liability to the Manufacturer shall be limited to replacement of the product ex factory. The Manufacturer makes no warranty as to merchantability or filness for a particular purpose and this warranty is in lieu of all other warrantees express or implied. The user shall determine the suitability of the product for his intended use and assume all risks and liability in connection therewith.



FM 63167

XYPEX CHEMICAL CORPORATION

Richmond, British Columbia, Canada V6V 2G9 Telephone: (604) 273-5265 Website: www.xypex.com Xypex is a registered trademark of Xypex Chemical Corporation. Printed in Canada. Distributed By:

Independent Test Results

Permeability - U.S. Army Corps of Engineers CRD-C-48-73 "Permeability of Concrete"

Two inch thick, 2000 PSI (13,790 KPa), Xypex-treated concrete samples were pressure tested up to a 123.5m water head (175 PSI-1207 KPa), which was the limit of the testing apparatus. While untreated samples showed marked leakage, the Xypextreated samples, as a result of the crystallization process, became totally sealed and exhibited no measurable leakage.

Chemical Resistance - A.S.T.M. C267-77 "Chemical Resistance of Mortars"

Xypex-treated cylinders and untreated cylinders were exposed to such chemicals as hydrochloric acid, caustic soda, toluene, mineral oil, ethelyne glycol, pool chlorine and brake fluid. Results of these studies indicated that chemical exposure did not have detrimental effect on the Xypex coating. Tests following chemical

Products

Xypex crystalline waterproofing materials are packaged in powder form and are mixed with water for application as a cementitious slurry coating on concrete surfaces, or as a Dry-Pac[™] for sealing of construction joints and repair of cracks.

XYPEX Concentrate

Used as a single coating on above or below grade concrete, or as the first of a two coat application where two coats are required (see Xypex Specification Manual). Also used as a Dry-Pac for sealing strips (fillets) at construction joints and honeycombing. Xypex Concentrate is the most chemically potent of the Xypex crystalline waterproofing material.

XYPEX Modified

Used as a second coat to reinforce Xypex Concentrate where two coats are required. Also used as an exterior damproofing.

Coverage

For normal surface applications coverage per coat is: 1.5 pounds per square yard (0.8 kilograms per square metre). For construction joint surfaces coverage is: 2.0 pounds per square yard (1.0 kilograms per square metre). See mixing instructions below.

Application Information

Surface Preparation

Concrete surfaces to be treated must be clean and free of laitance, dirt, films, paint, coatings or other foreign matter. The surfaces must also have an open capillary system so as to provide 'tooth and suction' for the Xypex treatment. It surfaces are too smooth, the concrete should be acid etched, waterblasted or lightly sandblasted.

Structural defects such as cracks, faulty construction joints and honeycombing should be routed out to sound concrete and repaired in accordance with the Xypex Repair Procedures (see Specification & Application Manual).

Horizontal surfaces should preferably have a rough wood float or broom finish. All concrete laitance must be removed either by etching with muriatic acid or by waterblasting or sandblasting.

Wetting Concrete

Prior to the application of Xypex, concrete surfaces must be thoroughly wetted with clean water to control surface suction, aid the exposure indicated average compressive strength increases of 20% for Xypex-treated specimens over untreated control samples.

Freeze-Thaw and De-icing Chemical Resistance - A.S.T.M. C672-76 "Standard Test Method for Scaling Resistance of Concrete Surfaces Exposed to De-icing Chemicals"

Xypex-treated samples restricted chloride ion concentration to below the level necessary to promote electrolytic corrosion of reinforcing steel. Visual examination of untreated panels after 50 cycles showed a marked increase in surface deterioration as compared to treated panels.

Radiation Resistance - U.S.A. Standard No. N69-1967 "Protective Coatings for the Nuclear Industry"

After exposure to 5.76x10⁴ rads of gamma radiation, the Xypex treatment revealed no ill effects or damages.

proper curing of the treatment and ensure the growth of the crystalline formation deep within the pores of the concrete. Of course, excess surface water should be removed before the application.

Mixing For Slurry Coat

Xypex powder is mixed with clean water to a creamy consistency in the following proportions by volume:

Brush application:

1.5 lbs./sq.yd (0.81 kg/sq.m) - 5 parts powder to 2 parts water

 2.0 lbs./sq.yd (1.08 kg/sq.m) – 3 parts powder to 1 part water Spray application:

1.5 lbs./sq.yd (0.81 kg/sq.m) – 5 parts powder to 3 parts water (may vary with equipment type)

Mixing for Dry-Pac

Mix 6 parts Xypex Concentrate powder with one part clean water by volume. Do not mix too wet (i.e. a putty-like consistency), otherwise mix may crack and spall as it dries.

Application

The Xypex treatment should be applied with a semi-stiff bristle brush, broom (for large horizontal applications) or with specialized spray equipment. For recommended equipment contact Xypex Chemical Corporation or your nearest distributor.

The Xypex treatment must be uniformly applied under the conditions and quantities specified. One coat should have a thickness of 1/16 inch (1.5 mm). When a second coat is required, it should be applied after the first coat has reached an initial set but is still 'green' (less than 48 hrs.). Light pre-watering between coats may be required due to drying. The Xypex treatment cannot be applied in rain or during freezing conditions.

Curing

A misty fog spray of water must be used for curing the Xypex treatment. Curing must begin as soon as the Xypex coating has hardened sufficiently so as not to be damaged by a fine spray. Under most conditions it is sufficient to spray Xypex-treated surfaces three times a day for 2-3 days. In hot climates spraying may be required more frequently. During the curing period the Xypex treatment must be protected from rainfall, frost and puddling of water.

For concrete structures that holds liquids (e.g. reservoirs, tanks, etc.), the Xypex treatment should be cured for three days and then allowed to set for 12 days before filling with liquid.



DESCRIPTION

Xypex is a unique chemical treatment for the waterproofing, protection and repair of concrete. XYPEX MODIFIED can be applied as a second coat to reinforce Xypex Concentrate, or applied by itself to dampproof the exterior of foundation walls. Applied as a second coat, Xypex Modified chemically reinforces Xypex Concentrate where two coats are required and produces a harder finish. Where dampproofing is required, a single coat of Modified may be used as an alternative to a spray/tar emulsion. Xypex prevents the penetration of water and other liquids from any direction by causing a catalytic reaction that produces a non-soluble crystalline formation within the pores and capillary tracts of concrete and cement-based materials.

RECOMMENDED FOR:

Xypex Modified is recommended as a single coat for the dampproofing of foundations or as a second coat with Xypex Concentrate for the following applications:

- Reservoirs
- · Sewage and Water Treatment Plants
- Secondary Containment Structures
- · Tunnels and Subway Systems
- · Underground Vaults
- Foundations
- Parking Structures
- Swimming Pools

ADVANTAGES

- Resists extreme hydrostatic pressure
- Becomes an integral part of the substrate
- · Allows concrete to breathe
- · Resistant to aggressive chemicals
- Non-toxic

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- Does not require dry weather or a dry surface
- Cannot puncture, tear or come apart at the seams
- · No costly surface priming or leveling prior to application
- Does not require sealing, lapping and finishing of
- seams at corners, edges or between membranes

Modified

- Can be applied to the positive or the negative side of the concrete surface
- Does not require protection during backfilling or during placement of steel, wire mesh or other materials
- · Less costly to apply than most other methods
- · Not subject to deterioration
- Permanent

PACKAGING

Xypex Modified is available in 60 lb. (27.2 kg) pails and 50 lb. (22.7 kg) bags.

STORAGE

Xypex products must be stored dry at a minimum temperature of 45°F (7°C). Shelf life is one year when stored under proper conditions.

COVERAGE

For normal surface conditions, the coverage rate for each coat is 6 - 7.2 sq. ft. per lb. $(1.25 - 1.5 \text{ lb. per sq. yd. or } 0.65 - 0.8 \text{ kg/m}^2)$.

TEST DATA

When used in conjunction with Xypex Concentrate:

PERMEABILITY

U.S. Army Corps of Engineers (USACE) CRD C48-73 "Permeability of Concrete" Pacific Testing Labs, Seattle, USA Two inch (51 mm) thick, 2000 psi (13.8 MPa) Xypextreated concrete samples were pressure tested up to a 405 ft. (124 m) water head (175 psi/1.2 MPa), the limit of the testing apparatus. While untreated samples showed marked leakage, the Xypex-treated samples (as a result of the crystallization process) became totally sealed and exhibited no measurable leakage.

DIN 1048 "Water Impermeability of Concrete" Bautest – Corporation for Research & Testing of Building Materials, Augsburg, Germany

Twenty cm thick Xypex-treated concrete samples were pressure tested up to 7 bars (230 ft./70 m water head) for

24 hours to determine water impermeability. While the reference specimens measured water penetration up to a depth of 92 mm, Xypex-treated samples measured water penetration of zero to an average of 4 mm.

ÖNORM B 3303 "Water Permeability of Concrete" Technologisches Gerwerbemuseum, Federal Higher Technical Education & Research Institute, Vienna, Austria

Xypex-treated concrete samples were pressure tested to a maximum 7 bars (230 ft./70 m water head) for 10 days. Test revealed that while 25 ml of water had penetrated the untreated concrete samples, zero ml had penetrated the Xypex-treated samples. Test specimens were then broken and showed water penetration to a depth of 15 mm on untreated samples but no measurable water penetration on the Xypex-treated samples.

CSN 1209/1321 "Impermeability and Resistance to Pressurized Water" Institute of Civil Engineering, Technology and Testing, Bratislava, Slovak Republic

Xypex-treated and untreated concrete samples were exposed to 1.2 MPa of pressure to determine water permeability. Results showed the Xypex-treated samples provided effective protection against hydrostatic water pressure. Treated and untreated samples were also subjected to contact with silage juices and various petroleum products (e.g. diesel oil, transformer oil, gasoline) at 14 kPa for 28 days. The Xypex-treated samples significantly reduced the penetration of these solutions.

CHEMICAL RESISTANCE

ASTM C 267-77 "Chemical Resistance to Mortars" Pacific Testing Labs, Seattle, USA

Xypex-treated cylinders and untreated cylinders were exposed to hydrochloric acid, caustic soda, toluene, mineral oil, ethelyne glycol, pool chlorine and brake fluid and other chemicals. Results indicated that chemical exposure did not have any detrimental effects on the Xypex coating. Tests following chemical exposure measured an average 17% higher compressive strength in the Xypextreated specimens over the untreated control samples.

IWATE University Technical Report "Resistance to Acid Attack" Tokyo, Japan

Xypex-treated mortar and untreated mortar were measured for acid resistance after exposure to a 5% H₂SO₄ solution for 100 days. Xypex suppressed concrete erosion to 1/8 of the reference samples.

FREEZE/THAW DURABILITY

ASTM C 672 "Standard Test Method for Scaling Resistance of Concrete Surfaces Exposed to De-icing Chemicals" Twin City Testing Lab, St. Paul, USA

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Xypex-treated samples restricted chloride ion concentration to below the level necessary to promote electrolytic corrosion of reinforcing steel. Visual examination of untreated panels after 50 freeze/thaw cycles showed a marked increase in surface deterioration compared to Xypex-treated samples.

POTABLE WATER EXPOSURE

NSF 61 "Drinking Water System Component-Health Effects" NSF International, Ann Arbor, USA

Exposure testing of potable water in contact with Xypextreated samples indicated no harmful effects.

RADIATION RESISTANCE

U.S.A. Standard No. N69 "Protective Coatings for the Nuclear Industry" Pacific Testing Labs, Seattle, USA

After exposure to 5.76 x 10⁺ rads of gamma radiation, the Xypex treatment revealed no ill effects or damages.

APPLICATION PROCEDURES

1. SURFACE PREPARATION Concrete surfaces to be treated must be clean and free of laitance, dirt, film, paint, coating or other foreign matter. Surfaces must also have an open capillary system to provide "tooth and suction" for the Xypex treatment. If surface is too smooth (e.g. where steel forms are used) or covered with excess form oil or other foreign matter, the concrete should be lightly sandblasted, waterblasted, or etched with muriatic (HCL) acid.

2. STRUCTURAL REPAIR Rout out cracks, faulty construction joints and other structural defects to a depth of 1.5 inches (37 mm) and a width of one inch (25 mm). Apply a brush coat of Xypex Concentrate as described in steps 5 & 6 and allow to dry for 10 minutes. Fill cavity by tightly compressing Dry-Pac into the groove with pneumatic packing tool or with hammer and wood block. Dry-Pac is prepared by mixing six parts Xypex Concentrate powder with one part water to a dry, lumpy consistency.

Note:

1. Against a direct flow of water (leakage) or where there is excess moisture due to seepage, use Xypex Patch'n Plug then Xypex Dry-Pac followed by a brush coat of Xypex Concentrate. (Refer to Xypex Specifications and Applications Manual for full details.)

AVERY CHEMICAL CORPORATION 000 **Cementitious Orystalline** Concrete Waterproofing 07160

2. For expansion joints or chronic moving cracks, flexible materials such as expansion joint sealants should be used.

3. WETTING CONCRETE Xypex requires a saturated substrate and a damp surface. Concrete surfaces must be thoroughly saturated with clean water prior to the application so as to aid the proper curing of the treatment and to ensure the growth of the crystalline formation deep within the pores of the concrete. Remove excess surface water before the application. If concrete surface dries out before application, it must be re-wetted.

4. MIXING FOR SLURRY COAT Mix Xypex powder with clean water to a creamy consistency in the following proportions:

For Brush Application

1.25 - 1.5 lb./sq. yd. (0.65 - 0.8 kg/m²) 5 parts powder to 2 parts water

2.0 lb./sq. yd. (1.0 kg/m²) 3 parts powder to 1 part water

For Spray Application
1.25 - 1.5 lb./sq. yd. (0.65 - 0.8 kg/m²)
5 parts powder to 3 parts water (ratio may vary with equipment type)

Do not mix more Xypex material than can be applied in 20 minutes. Do not add water once mix starts to harden. Protect hands with rubber gloves.

5. APPLYING XYPEX Apply Xypex with a semi-stiff nylon bristle brush, push broom (for large horizontal surfaces) or specialized spray equipment. The coating must be uniformly applied and should be just under 1/16 in. (1.25 mm). When a second coat (Xypex Concentrate or Xypex Modified) is required, it should be applied after the first coat has reached an initial set but while it is still "green" (less than 48 hours). Light pre-watering between coats may be required due to drying. The Xypex treatment must not be applied under rainy conditions or when ambient temperature is below 40°F (4°C). For recommended equipment, contact Xypex Chemical Corporation or your nearest Xypex distributor.

6. CURING A misty fog spray of clean water must be used for curing the Xypex treatment. Curing should begin as soon as the Xypex has set to the point where it will not be damaged by a fine spray of water. Under normal conditions, it is sufficient to spray Xypex treated surfaces three times per day for two to three days. In hot or arid climates, spraying may be required more frequently. During the curing period, the coating must be protected from rainfall, frost, wind, the puddling of water and temperatures below 36°F (2°C) for a period of not less than 48 hours after application. If plastic sheeting is used as protection, it must be raised off the Xypex to allow the coating to breathe. Xypex Gamma Cure may be used in lieu of water curing for certain applications (consult with Xypex Chemical Corporation or your nearest Xypex distributor).

Note: For concrete structures that hold liquids (e.g. reservoirs, swimming pools, tanks, etc.), Xypex should be cured for three days and allowed to set for 12 days before filling the structure with liquid.

TECHNICAL SERVICES

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SAFE HANDLING INFORMATION

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WARRANTY

The Manufacturer warrants that the products manufactured by it shall be free from material defects and will be consistent with its normal high quality. Should any of the products be proven defective, the liability to the Manufacturer shall be limited to replacement of the product ex factory. The Manufacturer makes no warranty as to merchantability or fitness for a particular purpose and this warranty is in lieu of all other warranties expressed or implied. The user shall determine the suitability of the product for his intended use and assume all risks and liability in connection therewith.





13731 Mayfield Place, Richmond, British Columbia, Canada V6V 2G9 Tel: (604) 273-5265 Tel: (800) 961-4477 Fax: (604) 270-0451 E-mail: info@xypex.com Website: www.xypex.com XYPEX is a registered trademark of Xypex Chemical Corporation. (

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DESCRIPTION

Xypex is a unique chemical treatment for the waterproofing, protection and repair of concrete. XYPEX CONCENTRATE is the most chemically active product within the Xypex Crystalline Waterproofing System. When mixed with water, this light grey powder is applied as a cementitious slurry coat to above-grade or belowgrade concrete, either as a single coat or as the first of a two-coat application. It is also mixed in Dry-Pac form for sealing strips at construction joints, or for the repairing of cracks, faulty construction joints and honeycombs. Xypex prevents the penetration of water and other liquids from any direction by causing a catalytic reaction that produces a non-soluble crystalline formation within the pores and capillary tracts of concrete and cement-based materials.

RECOMMENDED FOR:

Reservoirs

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- · Sewage and Water Treatment Plants
- Underground Vaults
- Secondary Containment Structures
- Foundations
- · Tunnels and Subway Systems
- Swimming Pools
- Parking Structures

ADVANTAGES

- Resists extreme hydrostatic pressure
- · Becomes an integral part of the substrate
- · Can seal hairline cracks up to 0.4 mm
- · Allows concrete to breathe
- · Highly resistant to aggressive chemicals
- Non-toxic
- Does not require a dry surface
- Cannot puncture, tear or come apart at the seams
- No costly surface prinning or leveling prior to application
- Does not require sealing, lapping and finishing of seams at corners, edges or between membranes
- Can be applied to the positive or the negative side of the concrete surface

Concentrate

- Does not require protection during backfilling or during placement of steel, wire mesh or other materials
- Less costly to apply than most other methods
- · Not subject to deterioration
- Permanent

PACKAGING

Xypex Concentrate is available in 20 lb. (9.1 kg) pails, 60 lb. (27.2 kg) pails and 50 lb. (22.7 kg) bags.

STORAGE

Xypex products must be stored dry at a minimum temperature of 45°F (7°C). Shelf life is one year when stored under proper conditions.

COVERAGE

For normal surface conditions, the coverage rate for each Xypex coat is 6 to 7.2 sq. ft./lb. $(1.25 - 1.5 \text{ lb./sq. yd. or } 0.65 - 0.8 \text{ kg/m}^2)$.

TEST DATA

PERMEABILITY

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Two inch (51 mm) thick, 2000 psi (13.8 MPa) Xypextreated concrete samples were pressure tested up to a 405 ft. (124 m) water head (175 psi/1.2 MPa), the limit of the testing apparatus. While untreated samples showed marked leakage, the Xypex-treated samples (as a result of the crystallization process) became totally sealed and exhibited no measurable leakage.

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CSN 1209/1321 "Impermeability and Resistance to

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Xypex-treated and untreated concrete samples were exposed to 1.2 MPa of pressure to determine water permeability. Results showed the Xypex-treated samples provided effective protection against hydrostatic water pressure. Treated and untreated samples were also subjected to contact with silage juices and various petroleum products (e.g. diesel oil, transformer oil, gasoline) at 14 kPa for 28 days. The Xypex-treated samples significantly reduced the penetration of these solutions.

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Xypex-treated cylinders and untreated cylinders were exposed to hydrochloric acid, caustic soda, toluene, mineral oil, ethelyne glycol, pool chlorine and brake fluid and other chemicals. Results indicated that chemical exposure did not have any detrimental effects on the Xypex coating. Tests following chemical exposure measured an average 17% higher compressive strength in the Xypextreated specimens over the untreated control samples.

IWATE University Technical Report "Resistance to Acid Attack" Tokyo, Japan

Xypex-treated mortar and untreated mortar were measured for acid resistance after exposure to a 5% H₂SO₄ solution for 100 days. Xypex suppressed concrete erosion to 1/8 of the reference samples.

FREEZE/THAW DURABILITY

ASTM C 672 "Standard Test Method for Scaling Resistance of Concrete Surfaces Exposed to De-icing Chemicals" Twin City Testing Lab, St. Paul, USA

Xypex-treated samples restricted chloride ion concentration to below the level necessary to promote electrolytic corrosion of reinforcing steel. Visual examination of untreated panels after 50 freeze/thaw cycles showed a marked increase in surface deterioration compared to Xypex-treated samples.

JIS A 6204 "Concrete Freeze/Thaw" Japan Testing Center For Construction Materials, Tokyo, Japan

The resonating frequency of both untreated and Xypextreated concrete samples were measured throughout 435 freeze/thaw cycles. At 204 cycles, the Xypex-treated samples showed 96% relative durability compared to 90% in the untreated samples. At 435 cycles, the Xypex-treated samples measured 91% relative durability compared to 78% in the untreated reference samples.

POTABLE WATER EXPOSURE

NSF 61 "Drinking Water System Component-Health Effects" NSF International, Ann Arbor, USA

Exposure testing of potable water in contact with Xypextreated samples indicated no harmful effects.

RADIATION RESISTANCE

U.S.A. Standard No. N69 "Protective Coatings for the Nuclear Industry" Pacific Testing Labs, Seattle, USA

After exposure to 5.76 x 10⁺rads of gamma radiation, the Xypex treatment revealed no ill effects or damages.

APPLICATION PROCEDURES

1. SURFACE PREPARATION Concrete surfaces to be treated must be clean and free of laitance, dirt, film, paint, coating or other foreign matter. Surfaces must also have an open capillary system to provide "tooth and suction" for the Xypex treatment. If surface is too smooth (e.g. where steel forms are used) or covered with excess form oil or other foreign matter, the concrete should be lightly sandblasted, waterblasted, or etched with muriatic (HCL) acid.

2. STRUCTURAL REPAIR Rout out cracks, faulty construction joints and other structural defects to a depth of 1.5 inches (37 mm) and a width of one inch (25 mm). Apply a brush coat of Xypex Concentrate as described in steps 5 & 6 and allow to dry for 10 minutes. Fill cavity by tightly compressing Dry-Pac into the groove with pneumatic packing tool or with hammer and wood block. Dry-Pac is prepared by mixing six parts Xypex Concentrate powder with one part water to a dry, lumpy consistency.

Note:

1. Against a direct flow of water (leakage) or where there is excess moisture due to seepage, use Xypex Patch'n Plug then Xypex Dry-Pac followed by a brush coat of Xypex

XYPEX CHEMICAL CORPORATION

Concentrate. (Refer to Xypex Specifications and Applications Manual for full details.)

2. For expansion joints or chronic moving cracks, flexible materials such as expansion joint sealants should be used.

3. WETTING CONCRETE Xypex requires a saturated substrate and a damp surface. Concrete surfaces must be thoroughly saturated with clean water prior to the application so as to aid the proper curing of the treatment and to ensure the growth of the crystalline formation deep within the pores of the concrete. Remove excess surface water before the application. If concrete surface dries out before application, it must be re-wetted.

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For Brush Application 1.25 - 1.5 lb./sq. yd. (0.65 - 0.8 kg/m²)

5 parts powder to 2 parts water

2.0 lb./sq. yd. (1.0 kg/m²)3 parts powder to 1 part water

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1.25 - 1.5 lb./sq. yd. (0.65 - 0.8 kg/m²)
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Do not mix more Xypex material than can be applied in 20 minutes. Do not add water once mix starts to harden. Protect hands with rubber gloves.

5. APPLYING XYPEX Apply Xypex with a semi-stiff nylon bristle brush, push broom (for large horizontal surfaces) or specialized spray equipment. The coating must be uniformly applied and should be just under 1/16 in. (1.25 mm). When a second coat (Xypex Concentrate or Xypex Modified) is required, it should be applied after the first coat has reached an initial set but while it is still "green" (less than 48 hours). Light pre-watering between coats may be required due to drying. The Xypex treatment must not be applied under rainy conditions or when ambient temperature is below 40°F (4°C). For recommended equipment, contact Xypex Chemical Corporation or your nearest Xypex distributor.

6. CURING A misty fog spray of clean water must be used for curing the Xypex treatment. Curing should begin as soon as the Xypex has set to the point where it will not be damaged by a fine spray of water. Under normal conditions, it is sufficient to spray Xypex-treated surfaces three times per day for two to three days. In hot or arid climates, spraying may be required more frequently. During the curing period, the coating must be protected from rainfall, frost, wind, the puddling of water and temperatures below 36°F (2°C) for a period of not less than 48 hours after application. If plastic sheeting is used as protection, it must be raised off the Xypex to allow the coating to breathe. Xypex Gamma Cure may be used in lieu of water curing for certain applications (consult with Xypex Chemical Corporation or your nearest Xypex distributor).

Note: For concrete structures that hold liquids (e.g. reservoirs, swimming pools, tanks, etc.), Xypex should be cured for three days and allowed to set for 12 days before filling the structure with liquid.

TECHNICAL SERVICES

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SAFE HANDLING INFORMATION

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WARRANTY

The Manufacturer warrants that the products manufactured by it shall be free from material defects and will be consistent with its normal high quality. Should any of the products be proven defective, the liability to the Manufacturer shall be limited to replacement of the product ex factory. The Manufacturer makes no warranty as to merchantability or fitness for a particular purpose and this warranty is in lieu of all other warranties expressed or implied. The user shall determine the suitability of the product for his intended use and assume all risks and liability in connection therewith.





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DESCRIPTION

XYPEX PATCH'N PLUG is a specially designed, fastsetting, non-shrink, high-bond-strength, hydraulic cement compound for concrete patching and repair. Patch'n Plug stops flowing water in seconds and is used to seal cracks, tie holes, and other defects in concrete. The high performance characteristics of Patch'n Plug are enhanced by Xypex's unique crystalline waterproofing technology.

RECOMMENDED FOR:

- · Stopping an active flow of water through cracks
- Repair of concrete substrates before the application of Xypex coating materials

ADVANTAGES

- Single component (simply add water)
- Fast setting: two to three minutes at 70°F (21°C)
- Excellent structural strength
- As durable as the masonry and concrete to which it is applied
- Non-metallic (won't rust or deteriorate)
- Non-toxic

PACKAGING

Xypex Patch'n Plug is available in 20 lb. (9.1 kg) pails and 60 lb. (27.2 kg) pails.

STORAGE

Xypex products must be stored dry at a minimum temperature of 45°F (7°C). Shelf life is one year when stored under proper conditions.

COVERAGE

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One 60 lb. (27.2 kg) pail of Xypex Patch'n Plug will produce 0.64 cubic feet (0.02 cu. metres) of mortar.

Patch'	N.	N	(fend)	1	IJ	Ca
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test data

PHYSICAL PROPERTY	TEST METHOD	TYPICA	L RESULT
Compressive Strength	ASTM C109	psi	(MPa)
at 24 hours		2100	(14.3)
at 7 days		3100	(21.3)
at 28 days		4500	(31.0)
C	40734 0366		1
Setting Time	ASTM C266	minutes	seconds
Initial Set	ASIM C200	minutes 3	seconds
	ASIM C200		
Initial Set	CSA A23.2-6B	3	50

Note: Samples prepared with 1 part water to 3.25 parts dry powder by volume (1 part water to 4 parts dry powder by mass). Setting time was determined using Gilmore needles.

PLUGGING INSTRUCTIONS

1. PREPARATION Rout out crack or hole by chiseling or chipping to a minimum depth of one inch (25 mm). Form a square or dovetail shaped space (do not use a "V" cut). Flush away all loose materials and dirt from the cavity with water and a stiff brush.

2. MIXING Add 1 part water to 3.5 parts Patch'n Plug by volume and mix to the consistency of a stiff putty. Do not mix more than can be used in 3 minutes. For best results, water temperature should be approximately 60°F - 70°F (15°C - 20°C).

3. PLUGGING Form plug with gloved hand. Place plug into cavity pressing firmly until plug is hard. When sealing cracks, begin at the highest point and work down.

Note: Where there is a high volume of water flow due to extreme hydrostatic pressure, a bleeder hose may be necessary to relieve the water pressure while sealing the repair area. (See procedures on reverse side.) Follow these steps:

a. With a concrete chisel and hammer (or chipping gun), cut open a cavity at the point of greatest water flow.

b. Place a stiff section of hose or pipe into the cavity and secure in place with Patch'n Plug to force water through the hose. This relieves the pressure so that the area can be patched. Allow a minimum of 24 hours for hardening.

c. Remove bleeder hose and plug remaining hole. If necessary, reduce water flow by inserting steel wool or wooden plug in the remaining hole before patching.

PATCHING INSTRUCTIONS

1. SURFACE PREPARATION Rout out faulty concrete until sound substrate is reached. Remove all loose materials from area and saturate with clean water. Allow water to be absorbed into the concrete, then remove excess water.

2. MIXING For fast repairs to concrete or masonry, add water to Patch'n Plug powder (1.5 parts water to 4 parts powder by volume). Mix to a workable mortar consistency and trowel on as required. For large repairs, mix 1 part Patch'n Plug with 2 parts mason sand or small aggregate (3/8 in. or 10 mm minus crushed stone). Maximum ratio is 40 lb. (18.2 kg) stone to one 60 lb. pail (27.2 kg) of Patch'n Plug.

ABNORMAL TEMPERATURES

During above normal ambient temperatures, mixing water should not exceed 90°F (32°C) and Xypex Patch'n Plug material should not exceed 70°F (21°C). Below normal ambient temperatures will retard the setting time of Patch'n Plug. In this situation, Xypex materials should be stored at normal temperatures (see Storage) and mixing water should be heated to increase setting speed.

TECHNICAL SERVICES

For more instructions, alternative application methods, or information concerning the compatibility of the Xypex treatment with other products or technologies, contact the Technical Department of Xypex Chemical Corporation or your local Xypex representative.

SAFE HANDLING INFORMATION

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Document:TA-63 TWF Construction ReportDate:January 2017

TA63 TWF Storage Building Floor Coating

Document:TA-63 TWF Construction ReportDate:January 2017

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Exhibit I

Attachment A

ubcont 39671	tract Number:		STR Name: Roy Maestas
SUBCONTRACTOR	Company Name: J.B. Henderson Constr Street Address: 1285 Trinity Drive, Suit City, State, Zip code: Los Alamos, NM 8754 Subcontractor's Poin Taylor Cardon	es A&B 4	Date Submitted: 11/12/14 Initial Submittal of a New Document Re- Submittal of Previous Document
Z	Submittal Number:	5.0579 (09 960	10/1.3.A.3)
CO	Submittal Title:	Testing Agency Coatings)	Certification of Nuclear Decontaminability (Special
8	Revision Number:	0	
2.3.7		resentative's signa	ature:
	Date Received:		ature:
	Date Received: Statused By:	Michael	ature:
			ature:
SR	Statused By:		Ature:
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Exhibit I Attachment A

	Alamos NAL LABORATORY - EST, 1943		BCONTRACTOR TTAL / STATUS SHEET
Subcont 289671	ract Number:		STR Name: Roy Maestas
SUBCONTRACTOR		of Contact: 5.0578-0001 Paint Schedule Special Coatings 6 esentative's signatu and meets the requ	re below indicates that submittal has been irements of the subcontract.
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Project	LANL TruWaste Facility TA63 - J.B. Henderson Construction						
09 9600	5.0578-1 09 9600	/1.3.A.2 - PAINT SCH	EDULE Spec	ial Coatings			
Building	Location	Surface Preparation	Coat/DFT	Name Color/Sheen	Application Method		
Storage 0149,	Storage, Electrical,	Diamond Grind as per	1 st 1.5 -2 Mils 2 nd 6-8	PPGAmerlock Sealer/Gloss	Brush/Roller		
0150, 0151, 0152,	Riser -Room Floors	ASTM D4259	Mils	PPGAmerlock2 Pearl Grey Gloss	Brush/Squeegee/Roller		
0153			3 rd 5-7 Mils	PPGPSX700 Pearl Grey Gloss	Brush/Roller		
Storage 0149, 0150, 0151, 0152, 0153	Storage, Electrical- Walls & Ceiling HM Doors/ Frames	N/A Gyp Board Light Sand HM Doors/ Frames	1 st , 2 nd ,3 rd 2-3 Mils per coat	PPGPitt-Tech 90-374 PC835 Porcelain White/Gloss	Brush/Roller/Spray		
	Fire Riser Steel	Light Sand	1 st ,2 nd 2-3 Mils Per Coat	PPGPitt-Tech 90-374 ½ PC842 Cooling Tower	Brush/Roller		
Storage & Character-	Rooms 1001, 1001A,	Diamond Grind as per	1 st 1.5-2 Mils	PPGAmerlock Sealer/Gloss	Brush/Roller		
ization Building	1002, 1003, 1003A,	ASTM D4259	2 nd 6-8 Mils	PPGAmerlock2 Pearl Grey Gloss	Brush/Squeegee/Roller		
	1021, 1022- Floors		3 rd 5-7 Mils	PPGPSX700 Pearl Grey Gloss	Brush/Roller		
Storage & Character- ization Building	Rooms 1001, 1001A, 1002, 1003, 1003A, 1021, 1022- Walls/Ceilings HM Doors/Frames	N/A Gyp Board Light Sand HM Doors/Frames	1 st , 2 nd ,3 rd 2-3 Mils Per Coat	PPGPitt-Tech 90-374 PC835 Porcelain White Gloss	Brush/Roller/Spray		

					PG. 2/2
Building	Location	Surface Preparation	Coat/DFT	Name Color/Sheen	Application Method
Storage & Character- ization Building	Fire Riser Steel	Light Sand	1 st , 2 nd 2-3 Mils Per coat	PPGPitt-Tech 90-374 ½ PC842 Cooling Tower	Brush/Roller
Operations Building	Rooms 1111, 1113- Floors	Diamond Grind as per ASTM D4259	1 st 1.5-2 Mils 2 nd	PPGAmerlock Sealer/Gloss PPGAmerlock2	Brush/Roller Brush/Squeegee/Roller
			6-8 Mils	Pearl Grey Gloss	
			3 rd 5-7 Mils	PPGPSX700 Pearl Grey Gloss	Brush/Roller
Operations Building	Rooms 111, 1113 Walls, Ceilings HMDoors/Frames	N/A Gyp Board Light Sand HMDoors/Frames	1 st ,2 nd ,3 rd 2-3 Mils per coat	PPGPitt-Tech 90-374 PC835 Porcelain White	Brush/Roller/Spray

Reviewer	Title	Page	Comment Type	Error Type	Formatted Comment	Standard/Spec Reference	Comment Date
Tarin, Manuel	SBT-289671-50579-0001_Testing Agency Cert Nuclear Decontaminability.pdf	2	Preference	Other	Reviewed by Sam Chlebana. Reviewed. Work may proceed.		11/21/2014 13:18

Exhibit I

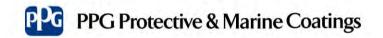
Attachment A

LOS	Alamos NAL LABORATORY EST. 1943		BCONTRACTOR ITAL / STATUS SHEET
Subcont 289671	ract Number:		STR Name: Roy Maestas
	Company Name:		Date Submitted:
	J.B. Henderson Constru	iction	11/12/14
OR.	Street Address: 1285 Trinity Drive, Suite	es A&B	Initial Submittal of a New Document
-C	City, State, Zip code: Los Alamos, NM 87544	L	Re- Submittal of Previous Document
SUBCONTRACTOR	Subcontractor's Point Taylor Cardon		
Z	Submittal Number:	5.0579 (09 9600/1	.3.A.3)
0 C	Submittal Title:	Testing Agency Cer Coatings)	rtification of Nuclear Decontaminability (Special
<u> </u>	Revision Number:	0	
	Date Received:		
	Statused By:		
	Date:		
OR	Comments:		
ACTOR			
CONTR	indicated com 3 Reviewed. Re 4 Reject. Sub	ise and resubmit. W ments. vise and resubmit. N	/ork may proceed subject to incorporation of Work may not proceed. t requirements. Resubmit. ed.
	Submit comments to:		

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SUBM	ISSION #	206#
1	Reviewed- Work may proceed	3 Reviewed- Revise & Resubmit.Work may NOT proceed.
12	Reviewed- Revise & Resubmit. Work may proceed subject to	4 Reject- Submittal does not meet requirements. Resubmit
<u> </u>	incorporation of indicated comments	5 Permission to proceed not required
consi not n omis	stency with the projec elieve the Contractor f sions in designs for wh	rom responsibility for errors or ich the contractor is responsible,
consi not n omis for co Docu work techr safet the s Date	stency with the project elieve the Contractor f sions in designs for who impliance with all requirements, and for the safe . This review does not hiques, sequences, and y precautions or progri	t design concept. This review does from responsibility for errors or lich the contractor is responsible, uirements of the Contract e and successful construction of the consider the means, methods, d operations of construction, or ams incidental thereto, which are

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79 Ronzo Road, Bristol, CT 06010 Tel: 203-232-3896

November 6, 2014

Mr. Michael Hunter Vice President Red Head Painting

Re: PSX 700 Level II Certification

Dear :

Please be advised that PPG PMC product PSX 700 has been fully tested and is an acceptable coating for use in Nuclear Facilities Coating Service Level II applications. This testing includes:

Radiation Tolerance (1E+09) Decontamination (>95% removal) Chemical Resistance (ASTM D3912) Fire Resistance (ASTM E84) Class B <25

I trust this information satisfies your needs at this time. If you have any questions, or require additional information, please feel free to call me at 203-232-3896.

Sincerely,

John 7. De Barba

John F. De Barba Technical Service Manager

cc: R. Knapp g/files/letters/Red Head_MH

 Document:
 TA-63 TWF Construction Report

 Date:
 January 2017

ENCLOSURE 3

Technical Area 63 Transuranic Waste Facility Container Storage Unit Permit Equipment and Operational Requirements

EPC-DO-16-361

LA-UR-16-29607

Date: _____ JAN 1 3 2017

 Document:
 TA-63 TWF Construction Report

 Date:
 January 2017

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.

Technical Area 63 Transuranic Waste Facility (TWF) Operations Equipment and Project Requirements from LANL Hazardous Waste Facility Permit for NMED Approval

No.	Item	Description	LANL Hazardous Waste Facility
			Permit Citation
1	Spill kits	Typically sorbents, neutralizers, personnel protection equipment (PPE)	A.6.8, Table D-5
2	Cleanup equipment	Shovels, bags, drums, over-pack drums	A.6.8, Table D-5
3	Safety data sheets	Available for cleaners, solvents used on site	A.6.8, Table D-5
4	First aid kits	Sufficient for minor injuries	Table D-5
5	Hearing protection	Sufficient to mitigate noise impacts	Table D-5
6	Secondary containment pallets	For free liquid waste containers	A.6.9
7	Fire extinguishers	ABC or BC rated portable fire extinguishers available	A.6.8, Table D-5
8	Communication equipment	All personnel have access to internal alarm or emergency communication device. Personnel working alone have access to two way radio, cell phone, or landline telephone without having to enter	2.10.3, Table D-5
		another building.	
9	Ignitable or reactive waste boundary restriction	Demarcation or knowledge of storage restriction for ignitable or reactive waste within 15 meters of the TWF fence line	2.8, 3.14.1(2)
10	Training	Hazardous waste management workers and supervisor training	2.7
11	Inspection plan	Plan for daily/weekly RCRA inspections	2.6
12	Records repository	Location for copies of Operating Record, Contingency Plan, Inspection Record Forms, training records	2.12.2 (as applicable), 2.11.3(1), 2.6.3
13	Program for soil vapor monitoring	In place for quarterly sampling, analysis, and reports after operations commence	3.14.3
14	Program for equipment and structure repair	In place to resolve repairs for any actions required (ARs) forthcoming from inspection program after operations commence	2.6.2
15	Evacuation plans/areas	Evacuation plan with routes and signals. Signs posted.	2.11.2, 2.11.3

No.	Item	Description	LANL Hazardous Waste Facility
			Permit Citation
16	Arrangements with local authorities	Los Alamos Fire Department notification of waste	2.10.5
		types, constituents, quantities, and location.	
17	Pallets	Pallets and drum binding for stacking as necessary	3.5.1(2)
18	Waste container labels	Hazardous, radioactive and free liquids labels	3.6
19	Warning signs	Bilingual warning signs stating posted on the perimeter fences and gates in accordance with Permit Section 2.5.2, Warning Signs.	A.6.7
20	Badge readers	Personnel security access	A.6.7

 Document:
 TA-63 TWF Construction Report

 Date:
 January 2017

ENCLOSURE 4

Facility Certification

EPC-DO-16-0361

LA-UR-16-29607

Date: _____ JAN 1 3 2017

 Document:
 TA-63 TWF Construction Report

 Date:
 January 2017

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Document: TA-63 TWF Construction Report
Date: January 2017

CERTIFICATION

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

John C. Bretzke Division Leader Environmental Protection and Compliance Division Los Alamos National Security, LLC Los Alamos National Laboratory Operator

Date Signed

Karen E. Armijo Permitting and Compliance Program Manager National Nuclear Security Administration Los Alamos Field Office U.S. Department of Energy Owner/Operator

01

Date Signed

Document: TA-63 TWF Construction Report Date: December 2016

CERTIFICATION

This certification was prepared in accordance with generally accepted professional engineering principles and practice pursuant to the requirements of 20.4.1 NMAC, incorporating 40 CFR §270.30(1)(2)(i), for a registered professional engineer's certification. These services have been performed with the care and skill ordinarily exercised by members of the profession practicing under similar conditions at this time. No other warranty is either expressed or implied. The finding and certification are based on 1) review of the project construction drawings associated with the construction of the Technical Area 63 Transuranic Waste Facility (TA-63 TWF); 2) review of the relevant materials specifications associated with the project; 3) review of the permit conditions for the TA-63 TWF contained in the LANL Hazardous Waste Facility Permit (the Permit); 4) observation of the construction procedures and activities for the project; and 5) discussion with project and environmental personnel responsible for the production of this report.

With the signature and seal below, I certify that the construction of the TA-63 TWF Container Storage Unit was conducted in accordance with the conditions of the Permit. The information presented in this report is, to the best of my knowledge and belief, true, accurate, and complete.

Respectfully, Los Alamos National Security, LLC

Michael D. Pope New Mexico Registered Professional Engineer No. $\frac{942}{128}$ Expires: $\frac{12-3}{-2016}$ Date: $\frac{12-18}{-2016}$

